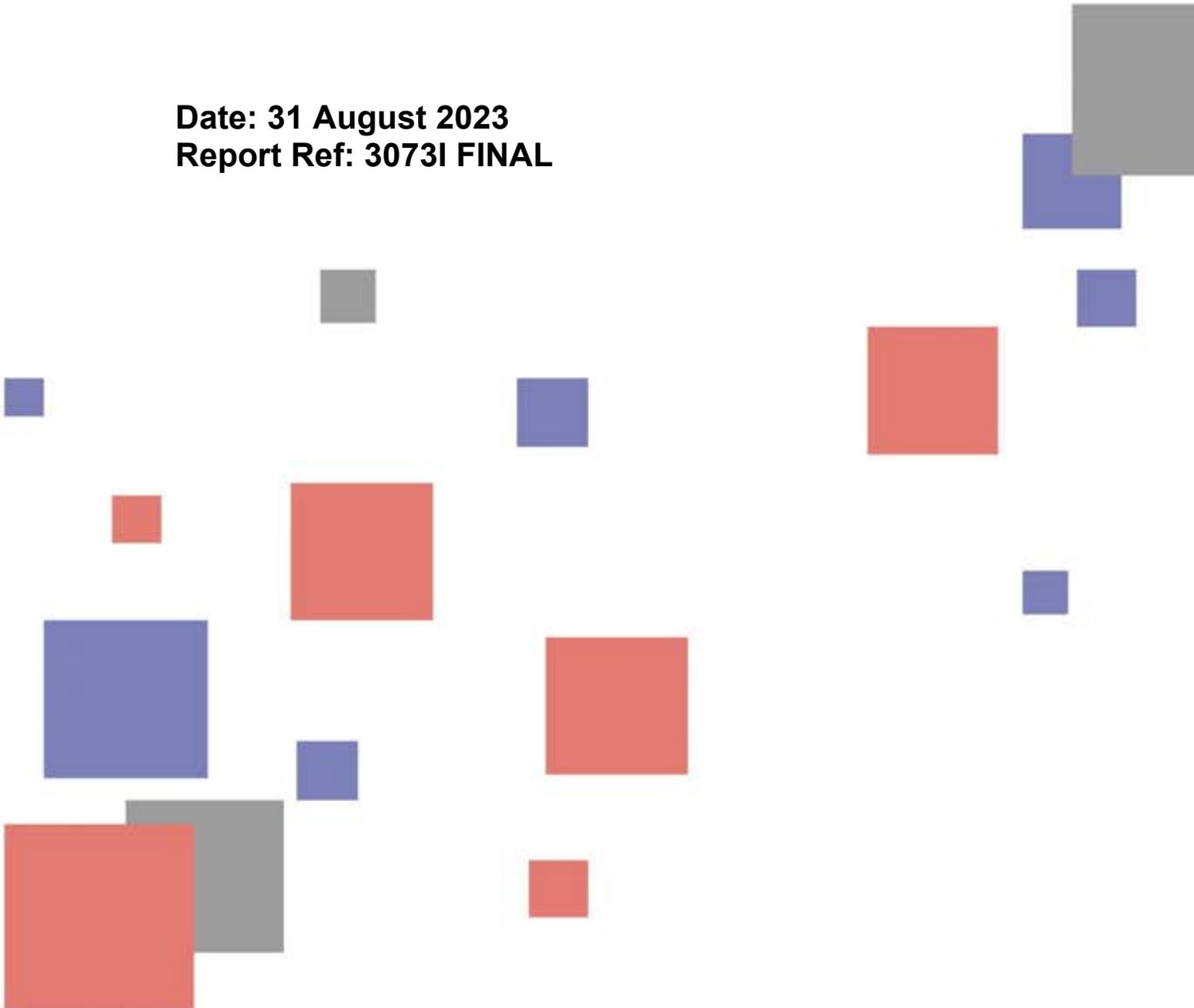


Report

Geotechnical Investigation for Coastal Erosion Vulnerability Assessment.

Ledge Point, Shire of Gingin WA.

**Date: 31 August 2023
Report Ref: 3073I FINAL**



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EXECUTIVE SUMMARY

A geotechnical investigation has been carried out as part of a coastal erosion assessment at Ledge Point in the Shire of Gingin, Western Australia. During the investigation ground geophysical and intrusive geotechnical testing was conducted within a 1500m corridor of coastal beach and dune formation adjacent to the Ledge Point settlement which has been identified as an at-risk site as part of Coastal Hotspot #19.

The investigation scope consisted of acquiring multi-channel analysis of surface waves data as a series of specified transects either along-shore (parallel to the coast) or cross-shore (perpendicular to the coast) and cone penetration testing at spot locations along these transects. This was supplemented with geological mapping of surface rock outcrops and topographic survey using GNSS receiver along the transects.

The acquired MASW dataset was processed for the generation of seismic velocity sections along the transects showing variations in the seismic shear wave velocity of the subsurface material to a target depth of 10-15m below ground level. The seismic velocity sections were calibrated with the CPT plots and demarcated into velocity ranges representing different material types and conditions for the generation of interpreted geological sections consisting of loose to compacted sediment and variably weathered to fresh rock.

The interpreted geological sections have been compiled to develop subsurface models of the level to rock substrate (relative to AHD) and overlying sand thickness within the region between the foreshore and the settlement. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the settlement.

The following observations have been made:

- Interpreted rock substrate was observed along the majority of the transects and within the maximum target investigation depth of 10-15m below ground level.
- Interpreted top of rock substrate on the along-shore transects on the beach ranged from -8.5m AHD to -2.5m AHD and averaged -5.5m AHD, overlain with an average 7.5m thick layer of variably compacted sediment.
- Interpreted top of rock substrate on the along-shore transects located adjacent to the existing settlement and along De Burgh Street ranged from -10m AHD to 3.5m AHD and averaged -4.5m AHD, overlain with an average 11m thick layer of variably compacted sediment.
- Interpreted top of rock substrate for the cross-shore transects extending over the dune formation ranged from -9m AHD to -1.5m AHD and averaged -5.5m AHD, overlain with an average 9.25m thick layer of variably compacted sediment.

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1 INTRODUCTION

At the request of The Government of Western Australia Department of Transport (DoT), GBG Group carried out a geotechnical investigation at Ledge Point, Shire of Gingin in May 2023. During the investigation, seismic geophysical testing and intrusive geotechnical testing was conducted within a 1500m corridor of coastal beach and dune formation which has been identified as an at risk site as part of Coastal Hotspot #19.

The objective of the investigation was to provide detailed mapping of the extent, elevation and consistency/strength of the rock underlying the coastal beach and dune formation. In particular, the key outcome of the investigation was to develop a subsurface model of the level to competent rock substrate (relative to AHD) within the region between the foreshore and the settlement. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the settlement.

To achieve the project objectives, data from the following investigation methods was acquired, processed and analysed so as to obtain the required subsurface information within the anticipated geological conditions:

1. **Geophysical testing** by way of Multi-channel Analysis of Surface Waves (MASW) to obtain seismic shear wave velocity models related to variations in subsurface material stiffness.
2. **Intrusive geotechnical testing** by way of Cone Penetration Testing (CPT) to measure sediment strength and compressibility, and for calibration and ground truthing of the geophysical dataset.
3. **Topographic survey** using Differential GNSS receiver. Note photogrammetry was not carried out, as the site was within a no-fly-zone restricting the use of survey drones within a controlled aerodrome space.

2 INVESTIGATION SITE

The investigation was carried out over an approximate 1500m corridor of coastal beach and dune formation extending from the foreshore in the west, to Roberts Road and De Burgh Street to the east, and from Wood Way in the south to Hill Place in the north. The extent of the investigation site is shown as a yellow dashed area in Figure 1.

Data was acquired as a series of transects for the seismic geophysical testing and point locations for the intrusive geotechnical testing. These were positioned so as to best utilise existing roads, tracks, and beach whilst not impacting native vegetation and in order to ensure the most optimal, efficient and economical acquisition methodology. Data was not acquired where surface obstructions were present such as thick vegetation, steep topography or where the beach was inundated with seawater. Photographs showing the typical site conditions are provided in Figure 2.



Figure 1: The extent of the geophysical investigation (yellow polygon) at Ledge Point. Aerial imagery from Landgate (main image) and Google Maps (inset image).



Figure 2: Site conditions at Ledge Point including along De Burgh Street (left image) and the beach access track (right image).

3 INVESTIGATION METHODOLOGY

3.1 FIELD SURVEY LOGISTICS

Geophysical data acquisition was carried out on the 29 to 31 June 2023 by a two-person crew from GBG Group consisting of qualified geophysicists. CPT data acquisition was carried out by a technician from Probedrill on the 10 and 11 July 2023. Where required, the site work was carried out under appropriate traffic and pedestrian management commissioned by the Shire of Gingin.

Prior to the commencement of data acquisition, a site assessment was carried out with representatives from the Shire of Gingin. Potential concerns and issues including the placement of and access to the MASW transects and CPT points were addressed and the initial indicative survey plan was adjusted, where necessary.

The site work for the investigation consisted of a total of 2912m of MASW profiling acquired as 5 along-shore transects (parallel to the coast) and 4 cross-shore transects (perpendicular to the coast), and a total of 7 CPT points along the transects. Details of the acquired MASW transects and CPT points are provided in Tables 1 and 2 respectively. The extents of the MASW transects and locations of the CPT points overlaid onto aerial imagery are shown in Appendix A drawing 3073I-01.

Table 1 – Acquired MASW Transects (Coordinates in GDA94, MGA Zone 50).

Transect ID	Orientation	Start Coordinate		End Coordinate		Length (m)
		East	North	East	North	
MASW01	Along-shore	344615.9	6557916.9	344693.9	6557110.8	792
MASW02	Along-shore	344693.8	6557090.2	345167.7	6556659.4	616
MASW03	Along-shore	344695.7	6557695.8	344746.5	6557389.2	304
MASW04	Along-shore	344715.5	6557359.5	344726.8	6557172.8	192
MASW05	Along-shore	344717.8	6557153.9	345163.1	6556803.1	592
MASW06	Cross-shore	344633.5	6557680.4	344700.1	6557653.7	72
MASW07	Cross-shore	344650.8	6557356.8	344765.2	6557380.3	120
MASW08	Cross-shore	344677.5	6557095.4	344737.8	6557193.4	112
MASW09	Cross-shore	344952.8	6556796.6	344998.5	6556894.5	112

Table 2 – Acquired CPT Points (Coordinates in GDA94, MGA Zone 50).

CPT ID	Coordinate		Surface Level (mAHD)	Probing Depth (m)
	East	North		
CPT01	345158	6556801	9.98	10.20
CPT02	344952	6556808	2.08	9.28
CPT03	344844	6556939	9.00	10.22
CPT04	344685	6557104	1.68	8.36
CPT05	344721	6557311	4.79	10.20
CPT06	344692	6557662	3.56	5.82
CPT07	344714	6557492	6.79	10.22

3.2 MULTI-CHANNEL ANALYSIS OF SURFACE WAVES

MASW is a seismic geophysical method that utilises phase and frequency information to calculate Shear wave (S-wave) velocities in vertical layer models averaged over an array of linearly spaced geophones. These 1D models can be laterally stacked to provide 2D cross-sections of S-wave velocity in layers. Under most circumstances it is an indicator of material stiffness and as such the method can be used to provide quantitative results on the compaction of the subsurface material.

MASW data was acquired using a Geode (Geometrics) seismograph connected to a receiver array of 24 geophones set at 1m intervals for a total array length of 23m. The receiver array was mobilised on a land streamer whereby the geophones are mounted on base plates attached to webbing, and either towed behind a 4WD light vehicle or manually pulled by the field team. Seismic energy was generated using summed impacts from a PEG-40 (R.T. Clark) vehicle mounted accelerated weight drop or softened steel sledgehammer with source points made at a constant offset from receiver array. MASW acquisition parameters are provided in Table 3. Photographs of MASW data acquisition are shown in Figure 3.

Table 3 – MASW Acquisition Parameters

Parameter	Value
Number of geophones	24
Geophone spacing	1 m
Array length	23 m
Geophone frequency	4.5 Hz
Record length	1 s
Sample interval	0.25 ms
Source	40kg AWD or 6.35kg sledgehammer
Source offset	4 m
Sounding interval	8m
Source stacks	3



Figure 3: MASW data acquisition using a seismic streamer.

The MASW data was observed to be of high quality with the seismic records having high signal to noise ratio. The generated overtone images plotting phase velocity against frequency showed a prominent dispersion curve of the surface wave component. The MASW data was processed using SurfSeis version 6++ (Kansas Geological Survey, 2017) with the following processing routine:

1. Import acquired seismic data files and apply geometry including geophone spacing, source offset and sounding interval.
2. Generate overtone images giving the percentage intensity of phase velocity versus frequency for each seismic record (Figure 4, left image).
3. Pick the maximum intensity across the useful range of frequencies for each overtone image resulting in a dispersion curve.
4. Run the dispersion curves through a 10-layer inversion algorithm to produce 1D soundings plotting seismic S-wave velocity with depth (Figure 4, right image).

The S-wave velocity soundings were compiled with reference to distance along the transects and gridded with Surfer version 25 (Golden Software, 2023). The resulting contoured cross-sections show the variation in the modelled S-wave velocity of the subsurface material in metres per second laterally along each of the transects and with elevation.

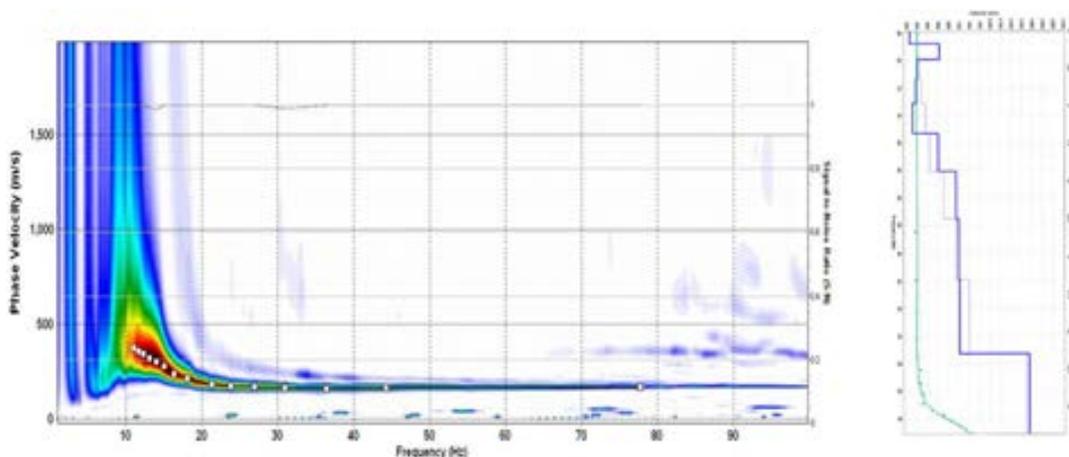


Figure 4: MASW overtone image with high signal to noise ratio and picked dispersion curve.

3.3 CONE PENETRATION TESTING

CPT is a geotechnical test method for evaluating the properties of soils and assessing subsurface stratigraphy including the sediment/rock interface at spot locations. The method involves pushing a calibrated cone and rod into the ground with a measured force with the resulting friction resistance plotted against depth to provide sediment compaction rates as well as the refusal depth indicating the depth to competent rock.

Testing was carried out using a M2 (Morooka) 11 tonne track mounted CPT Rig, specifications of which are provided in Appendix D. The test points were initially marked out at suitable locations within 2m of the intersecting geophysical transects. Dial Before You Dig enquiries and if necessary, utility locating was carried out prior to testing commencing.

CPT readings were made with sufficient ground bearing pressure to obtain a target depth of 10m or prior refusal. Where shallow refusal depths of less than 2m was encountered, when deemed necessary, an additional offset test was made to ascertain whether shallow refusal was due to a rock floater or other shallow obstruction. A photograph of CPT data acquisition is shown in Figure 5.



Figure 5: CPT data acquisition during a previous coastal investigation.

3.4 SPATIAL POSITIONING AND PHOTOGRAMMETRY

Spatial positioning of the acquired geophysical transects was achieved using an S631 (Hemisphere) GNSS receiver with a coordinate recorded for each MASW sounding location and CPT point. Coordinates of the geophysical transects have been provided in GDA94, MGA zone 50 for horizontal component and Australian Height Datum (mAHD) for vertical component. An accuracy of +/-0.2m is expected for both vertical and horizontal components.

To achieve precise reduced levels referenced to AHD, a local base correction with an Atlas Satellite-Based Differential Correction Service (L-Band) was used.

A reduced level of 0.0mAHD is considered to be the Mean Sea Level (MSL) for the purpose of this investigation. This relationship for Mean Sea Level was established by the Geoscience Australia Survey

in 1971 (<http://www.ga.gov.au/scientific-topics/positioning-navigation/geodesy/datums-projections/australian-height-datum-ahd>).

4 RESULTS AND INTERPRETATION

4.1 PRESENTATION OF RESULTS

The results of the geotechnical investigation at Ledge Point, Shire of Gingin are presented in Appendices B and C of this report as follows:

Appendix B – Geophysical and Interpreted Sections

- **3073I-02, 3073I-03 and 3073I-04.** Transect 1 seismic S-wave velocity model and interpreted geological section.
- **3073I-05 and 3073I-06.** Transect 2 seismic S-wave velocity model and interpreted geological section.
- **3073I-07.** Transect 3 seismic S-wave velocity model and interpreted geological section.
- **3073I-08.** Transect 4 seismic S-wave velocity model and interpreted geological section.
- **3073I-09 and 3073I-10.** Transect 5 seismic S-wave velocity model and interpreted geological section.
- **3073I-11.** Transects 6 and 7 seismic S-wave velocity model and interpreted geological section.
- **3073I-12.** Transects 8 and 9 seismic S-wave velocity model and interpreted geological section.

Appendix C – Modelled Level to Top of Rock and Sand Thickness

- **3073I-13 and 3073I -14.** Contoured level to modelled top of rock.
- **3073I-15.** Class post map level to modelled top of rock.
- **3073I-16 and 3073I -17.** Contoured modelled sand thickness over rock.
- **3073I-18.** Class post map modelled sand thickness over rock.

4.2 SEISMIC SHEAR WAVE VELOCITY SECTIONS

The seismic S-wave velocity (V_s) sections modelled from the MASW data acquired along the along-shore and cross-shore transects are presented at the top of each drawing in Appendix B. These sections show variations in the modelled V_s as per the colour scale with velocity ranging from 150m/s to 1000m/s representing a wide range of material types and conditions.

Seismic S-wave velocity is governed by the elastic properties of the medium that the wave propagates through as shown in the equation below. In particular, it is primarily a function of soil density, void ratio

and effective stress. As such calculated values can provide a useful guide to the subsurface material condition with increasing velocity an indication of increasing material stiffness.

Seismic S-wave velocity

$$V_s = \sqrt{\frac{G}{\rho}}$$

where; G = Shear modulus,
 ρ = In-situ material density

4.3 INTERPRETED GEOLOGICAL SECTIONS

Below the seismic S-wave velocity sections are the interpreted geological sections based on detectable seismic velocity contrasts correlated with the CPT. Four classes have been defined representing different subsurface material conditions as follows:

1. **Very low seismic S-wave velocity** ($V_s < 250\text{m/s}$). Representing the lowest seismic velocities modelled during the investigation, this class is interpreted as sediment consisting of SAND of low compaction from either the beach or dune formation.
2. **Low seismic S-wave velocity** ($V_s 250\text{-}350\text{m/s}$). This class is interpreted as sediment consisting of SAND of moderate compaction due to increased depth of cover particularly in the beach and dune formation, or due to development adjacent to the settlement.
3. **Moderate seismic S-wave velocity** ($V_s 350\text{-}475\text{m/s}$). This class is interpreted as low strength rock consisting of variably weathered CALCARENITE. Where continuous and at base of the sections it likely represents a transitional zone to stronger, more competent underlying CALCARENITE. Where present as isolated anomalies within the interpreted SAND it is likely to represent partially lithified SAND and/or CALCARENITE lenses.
4. **Moderate to high seismic wave velocity** ($V_s > 475\text{m/s}$). This class is interpreted as moderate strength rock consisting of slightly weathered to fresh CALCARENITE. It is typically observed at the base of the sections as competent rock underlying the variably weathered CALCARENITE.

4.4 CALIBRATION WITH GEOTECHNICAL TESTING AND ROCK MAPPING

The results of the CPTs are presented in Appendix D showing the plots of cone tip resistance in megapascals against depth in metres. The CPT plots are also shown in Appendix B and overlaid onto the interpreted geological sections with the following observations being made:

- **CPT-01 on Transect 5** – reached a target depth of 10m Below Ground Level (BGL) without refusal. An increase in CPT tip resistance was observed at the top of interpreted low strength rock.

- **CPT-02 on Transects 2 and 9** – refusal of 65MPa plus rod friction was at a depth of 9.28mBGL which corresponds to the top of interpreted low strength rock on Transect 9 and approximately 1.5m into the interpreted low strength rock on Transect 2.
- **CPT-03 on Transect 5** – reached a target depth of 10mBGL without refusal corresponding to sand of variable compaction and with no evidence of rock.
- **CPT-04 on Transects 1 and 8** – refusal of 50MPa plus rod friction was at 8.36mBGL which corresponds to the top of interpreted low strength rock on both intersecting transects.
- **CPT-05 on Transect 4** – reached a target depth of 10mBGL without refusal corresponding to sand of variable compaction and with no evidence of rock.
- **CPT-06 on Transects 3 and 6** – refusal of 55MPa plus rod friction was at 5.82m BGL within interpreted sand. This is potentially due to a rock floater or partially lithified lens within the dune formation.
- **CPT-07 on Transect 3** – reached a target depth of 10mBGL without refusal corresponding to sand of variable compaction and with no evidence of rock.

The differences in the modelled level to low strength and moderate strength rock as interpreted from the MASW transects and from the CPT data can be attributed to the fact that the geophysical methods used are broad scale whilst the CPT is a point method. Geophysical methods sample a volume of subsurface material with the calculated depths at any particular point representing an average value over this volume. The CPT method samples the subsurface directly below the probe and is influenced by local variations in the subsurface such as rock floaters, highly weathered zones or lenses of partially lithified sediment. The differences in the type of subsurface sampling of the methods will not adversely affect the results as the CPT results have been used to constrain the geophysics interpretation and as such the results represent the best modelled fit between the datasets.

No surface outcropping rock was observed onsite along the acquired MASW transects. Furthermore, analysis of available aerial photogrammetry indicates no evidence of outcropping rock within the area between the coastal foreshore and settlement.

4.5 MODELLED LEVEL TO TOP OF ROCK AND SAND THICKNESS

Subsurface models for the level to top of rock substrate and overlying sand thickness within the region between the coastal foreshore and settlement are presented in Appendix C. These have been generated by digitising the interface between the interpreted sediment and underlying rock profile from the interpreted geological sections along the acquired along-shore and cross-shore transects and calibrated with the CPT plots. The modelled sand thickness was then generated by subtracting this from the surface elevation. The following subsurface models have been provided:

- **Contoured Level to Top of Rock Substrate** (drawing 3073I-13 and 3073I-14) – this presents the level to the top of rock substrate ranging from -9mAHD to 0mAHD.

- **Classed Post Map Level to Top of Rock Substrate** (drawing 3073I-15) – this presents the level to the top of rock substrate along the acquired transects at 1m level increments from -8mAHD to -2mAHD.
- **Contoured Sand Thickness Over Rock** (drawing 3073I-16 and 3073I-17) – this presents the thickness of sand overlying the rock substrate ranging from 4mBGL to 14mBGL.
- **Classed Post Map Sand Thickness Over Rock** (drawing 3073I-18) – this presents the thickness of sand overlying the rock substrate along the acquired transects at 2m depth increments from 4mBGL to 14mBGL.

The following limitations should be considered when assessing the subsurface models for the level to top of rock substrate and overlying sand thickness:

The expected accuracy of the top of rock substrate modelled from this investigation is +/-0.5mAHD. Similarly, an accuracy of +/-0.5m is expected for the modelled sand thickness over rock. The quoted accuracies have been based on consideration to the accuracy of the GNSS receivers used during the site work, 1D inversion of the MASW dataset using a 10-layer model, and expected undulations in the sand/rock interface. Note the quoted accuracies are only valid along the geophysical transects. Values given between transects have been interpolated in the contour maps and as such the accuracy in this case is indeterminable.

The generated contours will give the general trend of the top of rock profile however will not image local variations when the extent of these is less than transect spacing. Spatially small features such as karst sinkholes or pinnacle features may not be imaged. The significance of this limitation is considered minor for this investigation since although local geological features such as pinnacles may not be represented in the data, the generated surface of the top of rock will show the broad trends in the geology over the site which is suitable for a coastal erosion assessment.

Transition zones including between fresh and weathered rock and between sediment and lithified/partially lithified sediment may be gradational and as such the interface between these layers are not well defined.

The calculated levels to the top of rock will only be valid along the geophysical transects. Values shown on the contour maps not on the transects have been interpolated using the krigging algorithm and as such the accuracy of these levels is indeterminable. The contour surface will give the general trend of the interface however may not image local variations, it is recommended that the interpreted geological sections presented in Appendix B be used to obtain more accurate top of rock levels and overlying sand thickness.

5 PROJECT SUMMARY

A geotechnical investigation has been carried out as part of a coastal erosion assessment at Ledge Point in the Shire of Gingin, Western Australia. During the investigation ground geophysical and intrusive geotechnical testing was conducted within a 1500m corridor of coastal beach and dune formation adjacent to the Ledge Point settlement which has been identified as an at risk site as part of Coastal Hotspot #19.

The investigation scope consisted of acquiring multi-channel analysis of surface waves data as a series of specified transects either along-shore (parallel to the coast) or cross-shore (perpendicular to the coast) and cone penetration testing at spot locations along these transects. This was supplemented with geological mapping of surface rock outcrops and topographic survey using GNSS receiver along the transects.

The acquired MASW dataset was processed for the generation of seismic velocity sections along the transects showing variations in the seismic shear wave velocity of the subsurface material to a target depth of 10-15m below ground level. The seismic velocity sections were calibrated with the CPT plots and demarcated into velocity ranges representing different material types and conditions for the generation of interpreted geological sections consisting of loose to compacted sediment and variably weathered to fresh rock.

The interpreted geological sections have been compiled to develop subsurface models of the level to rock substrate (relative to AHD) and overlying sand thickness within the region between the foreshore and the settlement. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the settlement.

The methods used during the investigation are geophysical and as such the results are based on indirect measurements and the processing and interpretation of seismic wave signals calibrated with limited intrusive geotechnical testing. The findings in this report represent the professional opinions of the authors, based on experience gained during previous similar investigations.

We trust that this report and the attached drawings provide you with the information required. If you require clarification on any points arising from this geophysical investigation, please do not hesitate to contact the undersigned on 08 9354 6300.

For and on behalf of

GBG GEOTECHNICS (AUSTRALIA)

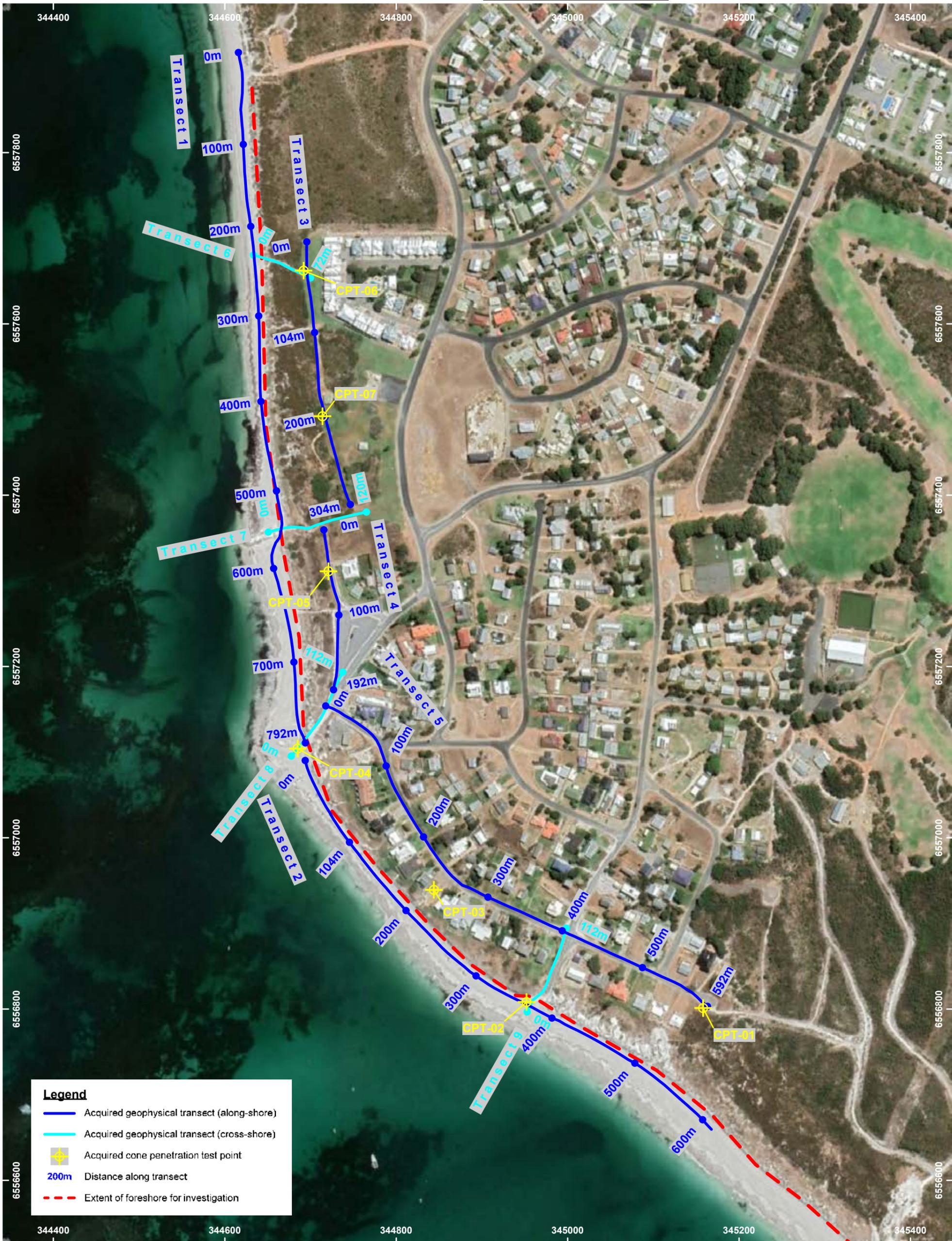


ANDREW SPYROU

Operations Manager, Western Australia / Senior Geophysicist

APPENDIX A – INVESTIGATION SITE MAP

INVESTIGATION SITE MAP



Legend

- Acquired geophysical transect (along-shore)
- Acquired geophysical transect (cross-shore)
- ★ Acquired cone penetration test point
- 200m Distance along transect
- - - Extent of foreshore for investigation

NOTES
 Drawing to be used in conjunction with GBG report 30731
 Map Projection GDA94 MGA Zone 50.
 Aerial image from Google Earth Pro



Date	23 August 2023	Paper Size	A3
Scale	1:4000	Drawn	AHWS
Drawing	30731-01	Revised	C

DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA
 GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.
 LEDGE POINT, SHIRE OF GINGIN WA

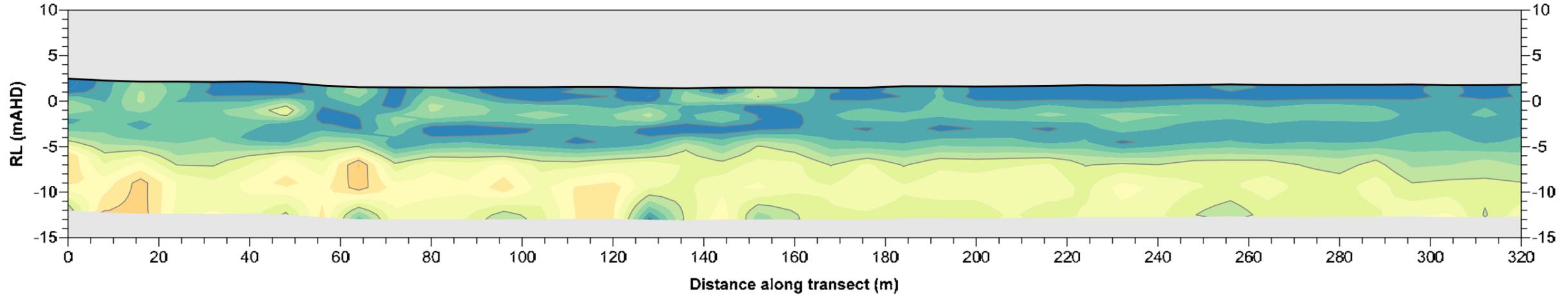
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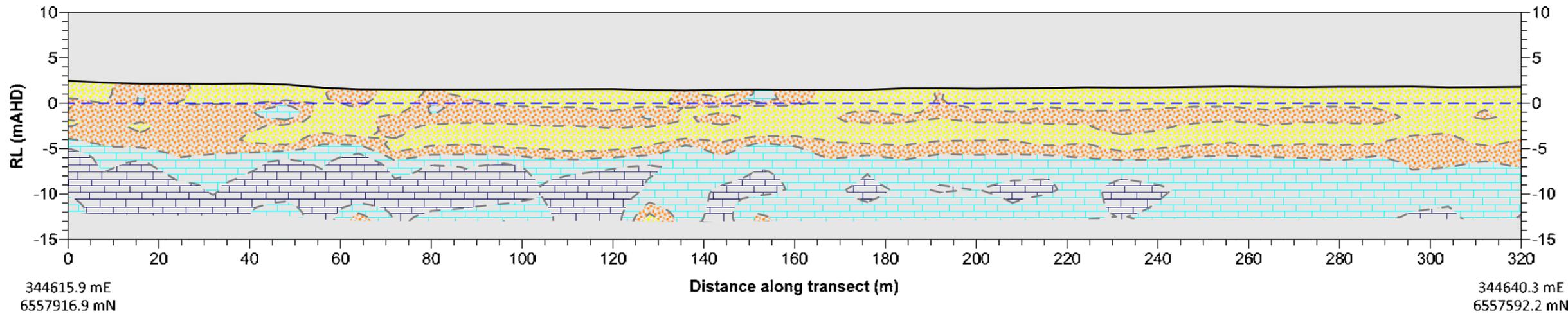
APPENDIX B – GEOPHYSICAL AND INTERPRETED SECTIONS

**GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT
LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA**

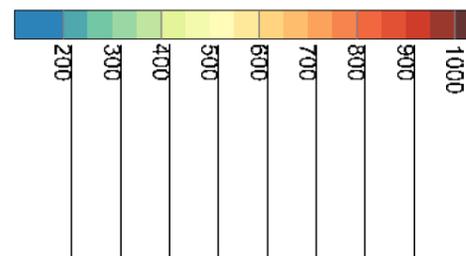
TRANSECT 1 (0-320m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 1 (0-320m) - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

- Tip Resistance (MPa)
- 0 to <5
 - 5 to <10
 - 10 to <15
 - 15 to <20
 - 20 to <25
 - 25 to <30
 - 30 to <35
 - 35 to <40
 - 40 to <45
 - 45 to <50
 - Equal to or >50

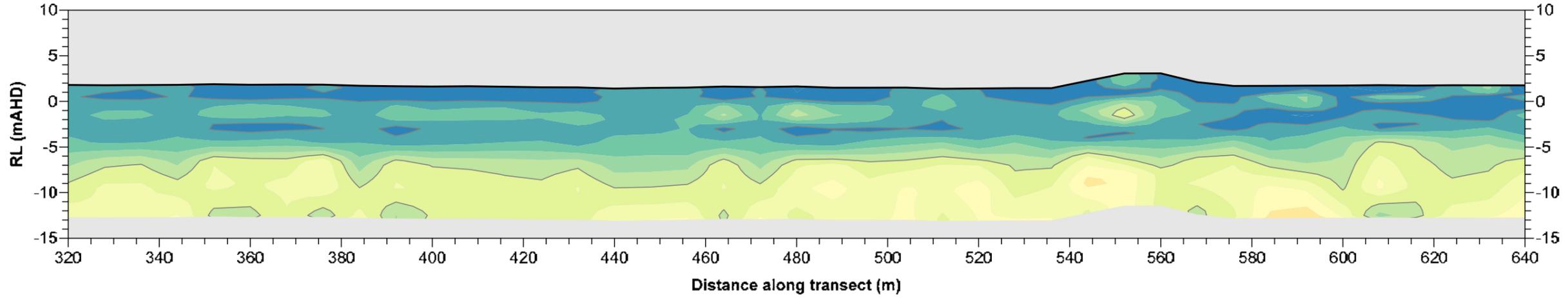
NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

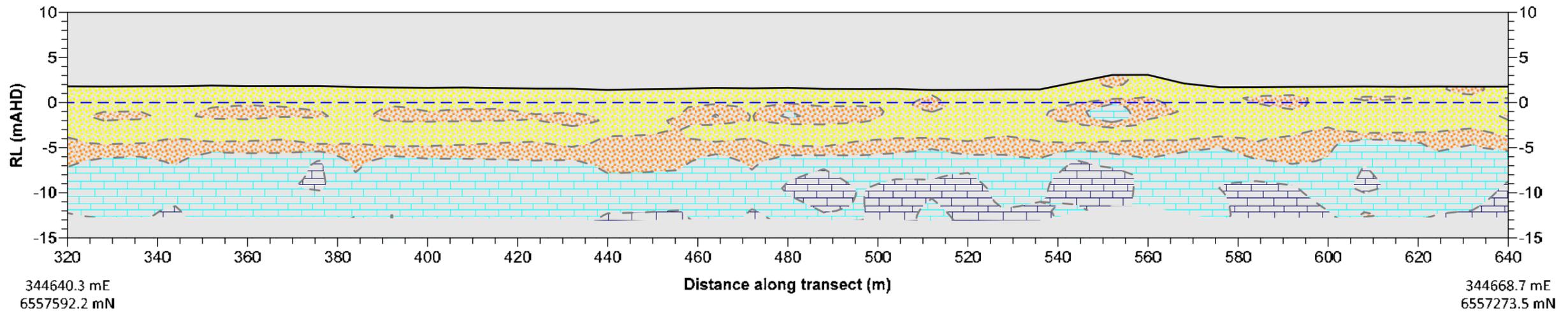
CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
	GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WA	Scale	1:1000H, 1:500V	Drawn	PJE
		Drawing	30731-02	Revised	C

**GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT
LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA**

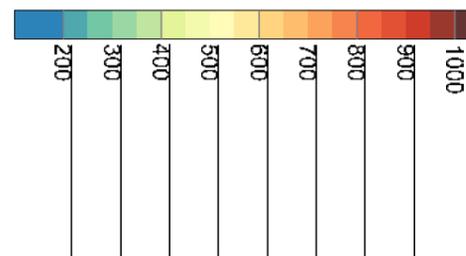
TRANSECT 1 (320-640m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 1 (320-640m) - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

- Tip Resistance (MPa)
- 0 to <5
 - 5 to <10
 - 10 to <15
 - 15 to <20
 - 20 to <25
 - 25 to <30
 - 30 to <35
 - 35 to <40
 - 40 to <45
 - 45 to <50
 - Equal to or >50

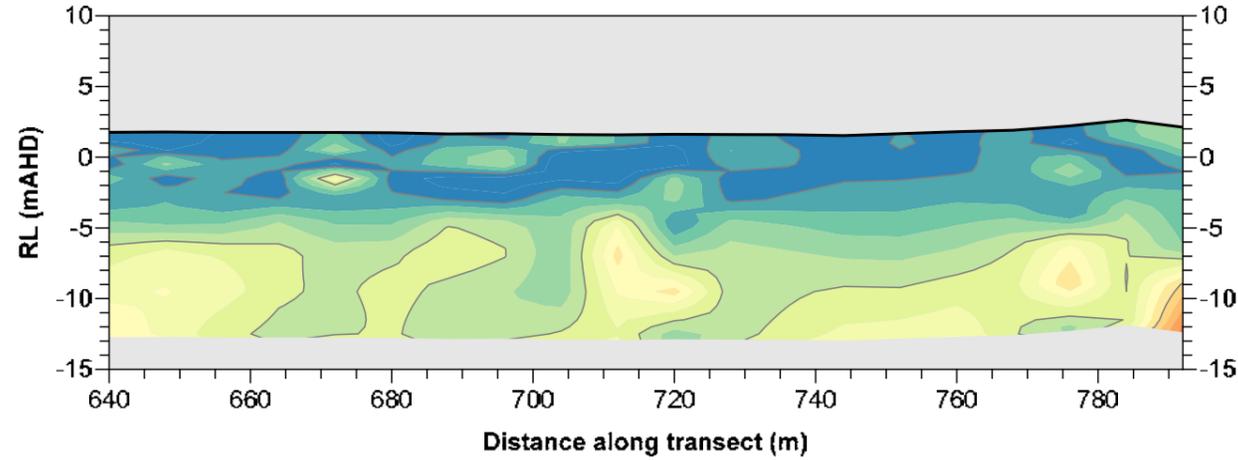
NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

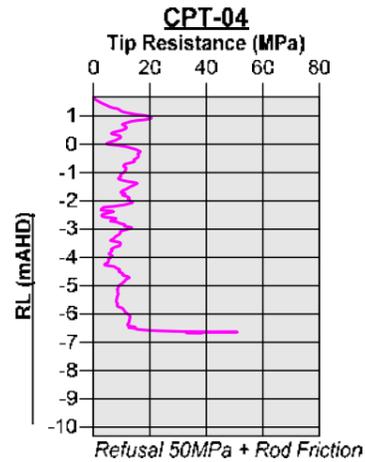
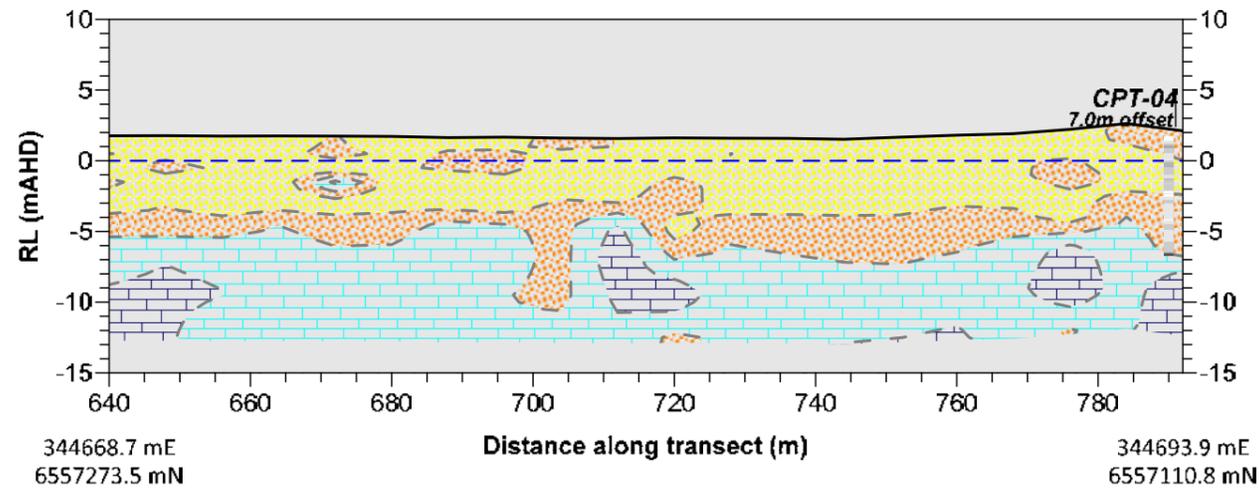
CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
	GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WA	Scale	1:1000H, 1:500V	Drawn	PJE
		Drawing	30731-03	Revised	C

**GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT
LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA**

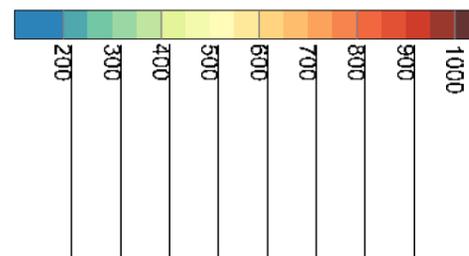
TRANSECT 1 (320-640m) - SEISMIC SHEAR WAVE VELOCITY MODEL



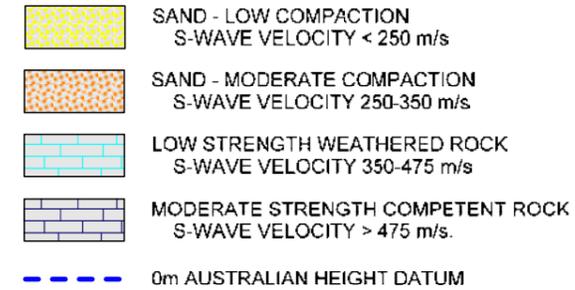
TRANSECT 1 (320-640m) - INTERPRETED GEOLOGICAL SECTION



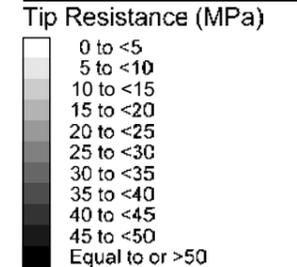
SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE



CONE PENETRATION TEST

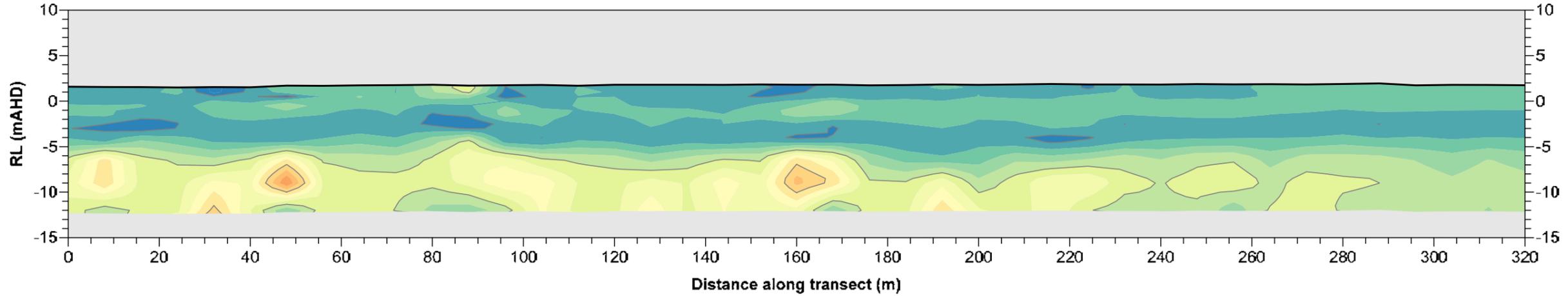


NOTES

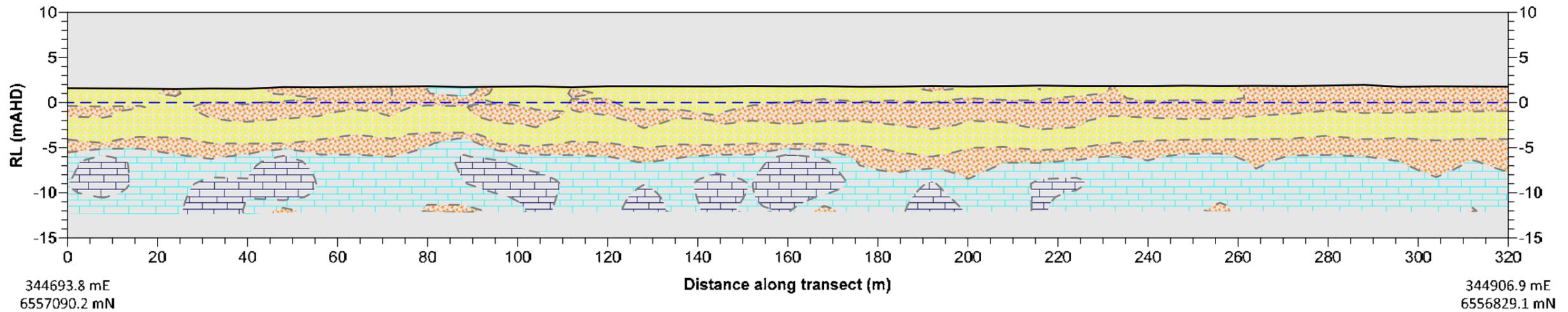
Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
	GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WA	Scale	1:1000H, 1:500V	Drawn	PJE
		Drawing	30731-04	Revisior	C

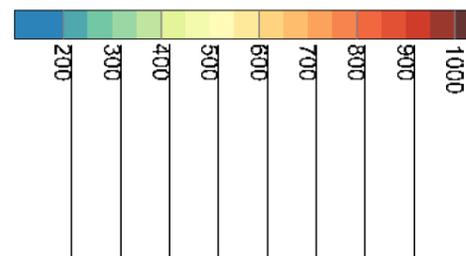
TRANSECT 2 (0-320m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 2 (0-320m) - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

- Tip Resistance (MPa)
- 0 to <5
 - 5 to <10
 - 10 to <15
 - 15 to <20
 - 20 to <25
 - 25 to <30
 - 30 to <35
 - 35 to <40
 - 40 to <45
 - 45 to <50
 - Equal to or >50

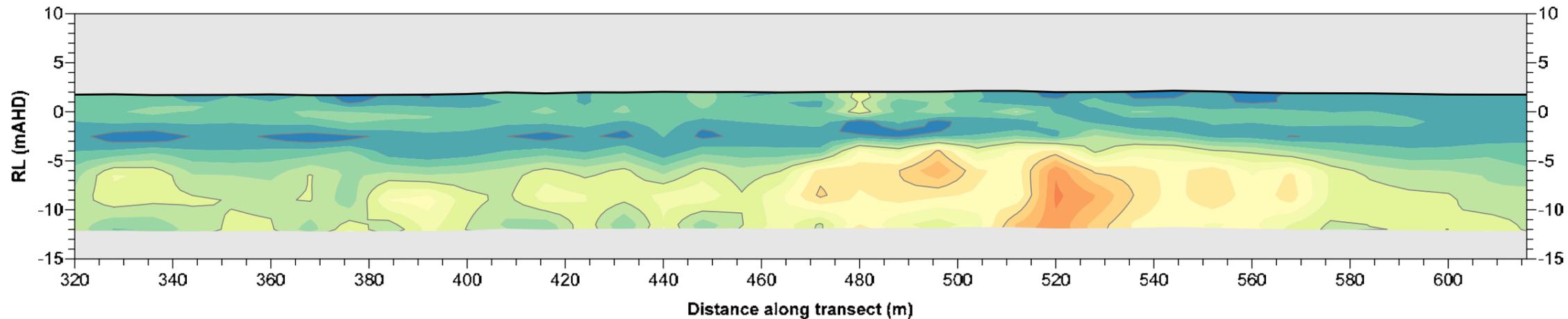
NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

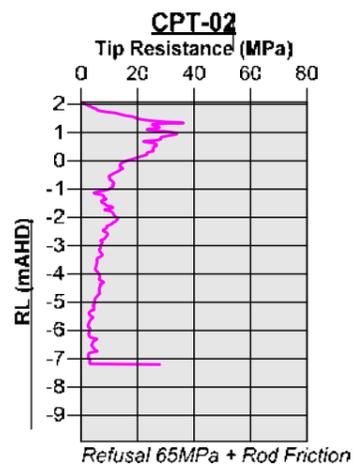
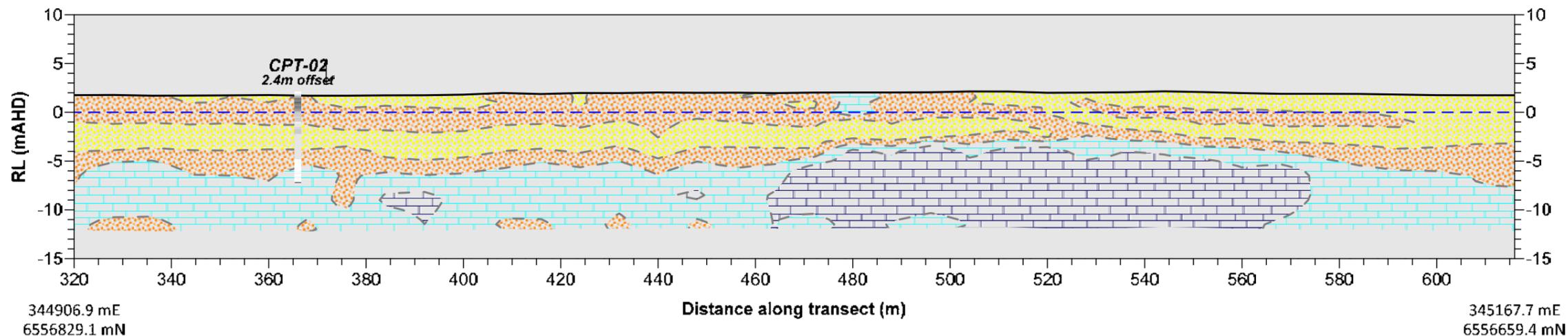
CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
	GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WA	Scale	1:1000H, 1:500V	Drawn	PJE
		Drawing	30731-05	Revisior	C

GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA

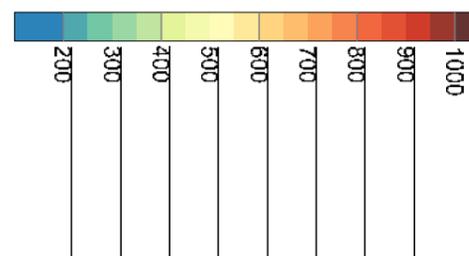
TRANSECT 2 (320-616m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 2 (320-616m) - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

CLIENT **DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA**

**GEOPHYSICAL INVESTIGATION FOR COASTAL
EROSION VULNERABILITY ASSESSMENT
LEDGE POINT, SHIRE OF GINGIN WA**

Date **14 August 2023**

Scale **1:1000H, 1:500V**

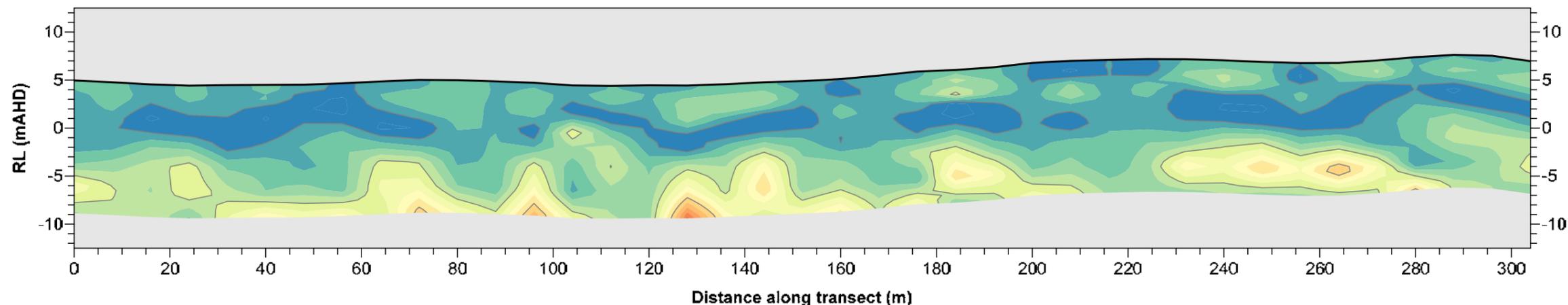
Drawing **30731-06**

Paper Size **A3**

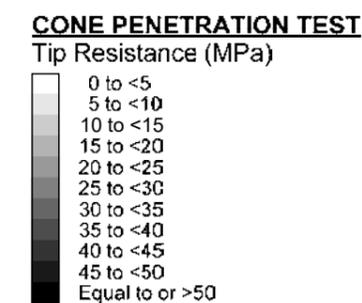
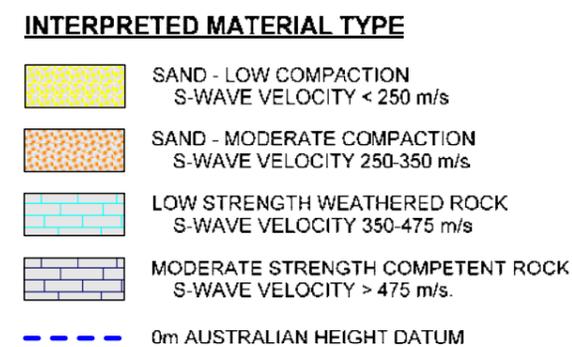
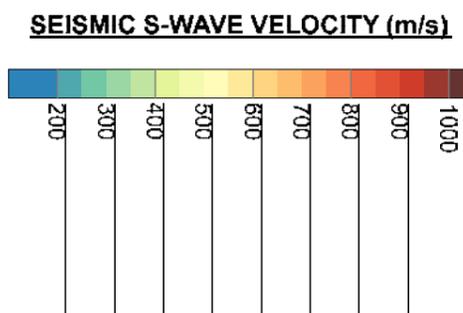
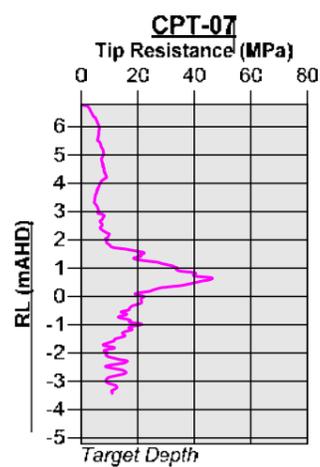
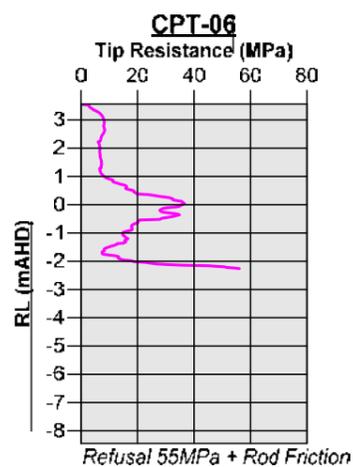
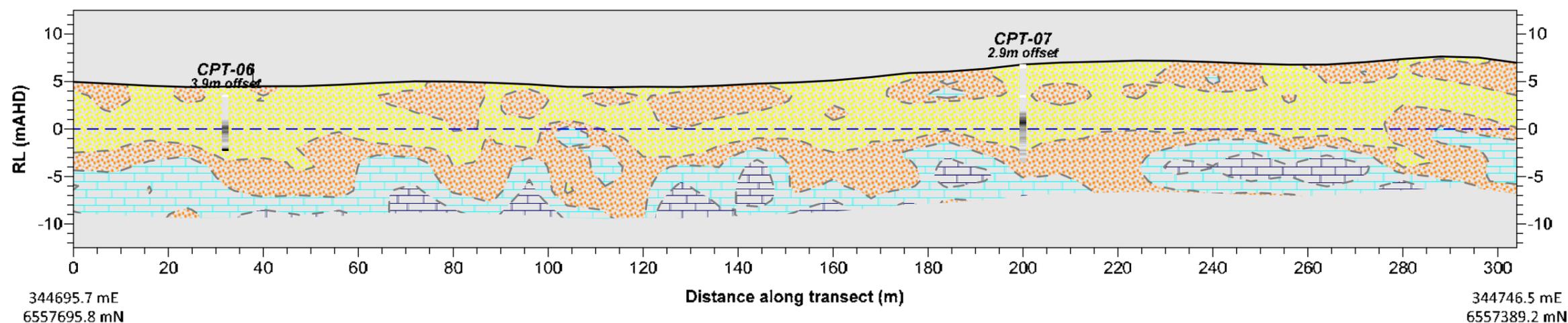
Drawn **PJE**

Revised **C**

TRANSECT 3 - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 3 - INTERPRETED GEOLOGICAL SECTION

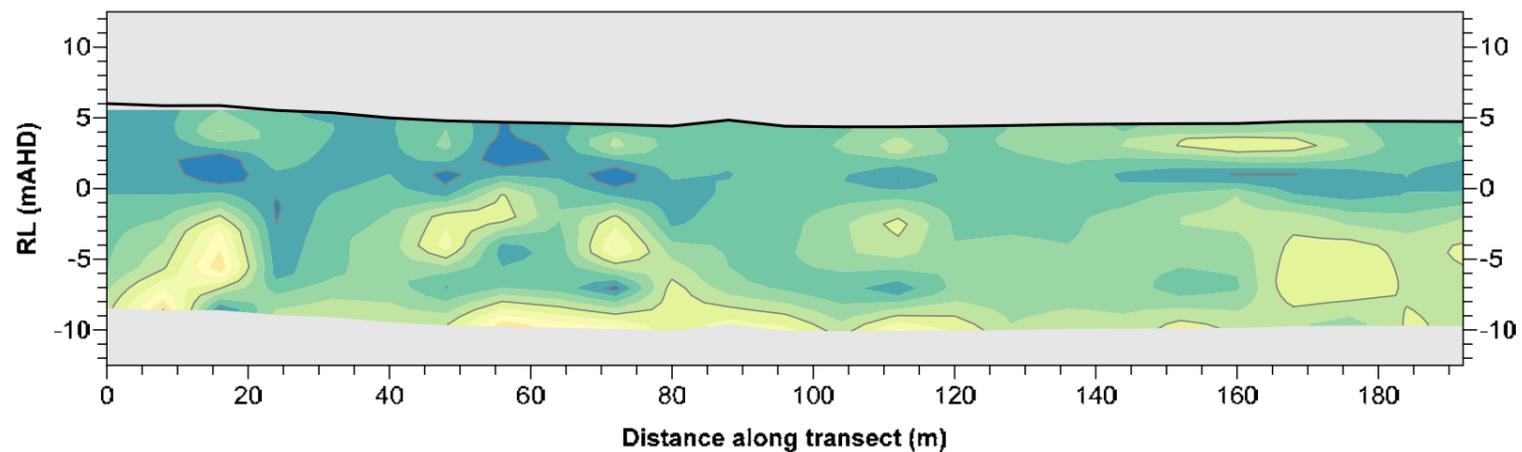


NOTES
Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

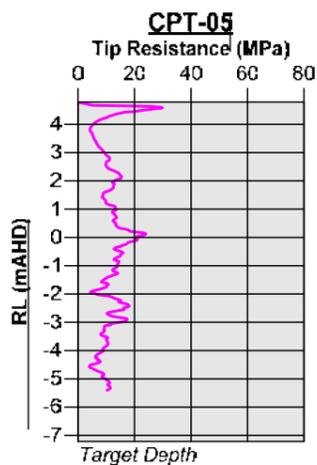
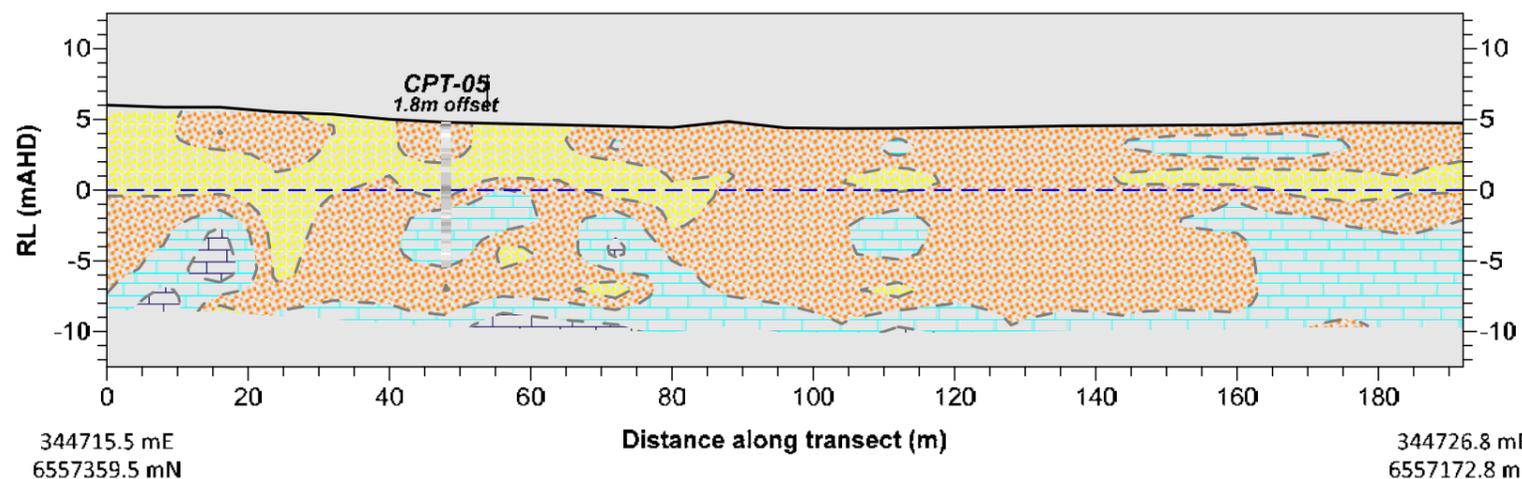
CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
	GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WA	Scale	1:1000H, 1:500V	Drawn	PJE
		Drawing	30731-07	Revisior	C

GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA

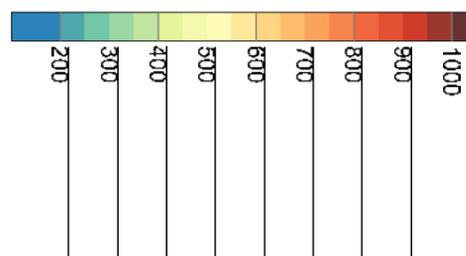
TRANSECT 4 - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 4 - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

- Tip Resistance (MPa)
- 0 to <5
 - 5 to <10
 - 10 to <15
 - 15 to <20
 - 20 to <25
 - 25 to <30
 - 30 to <35
 - 35 to <40
 - 40 to <45
 - 45 to <50
 - Equal to or >50

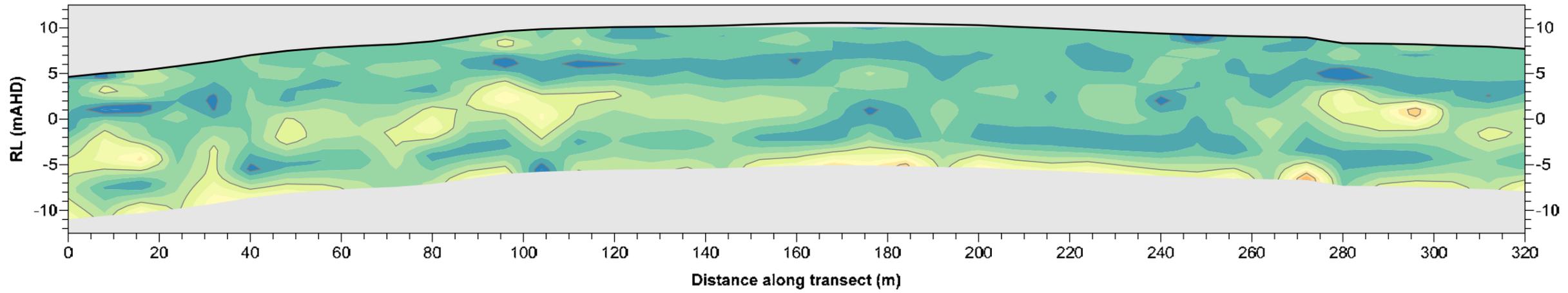
NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

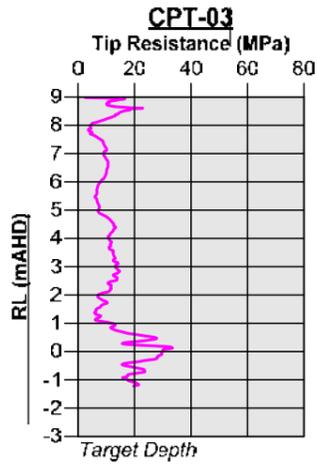
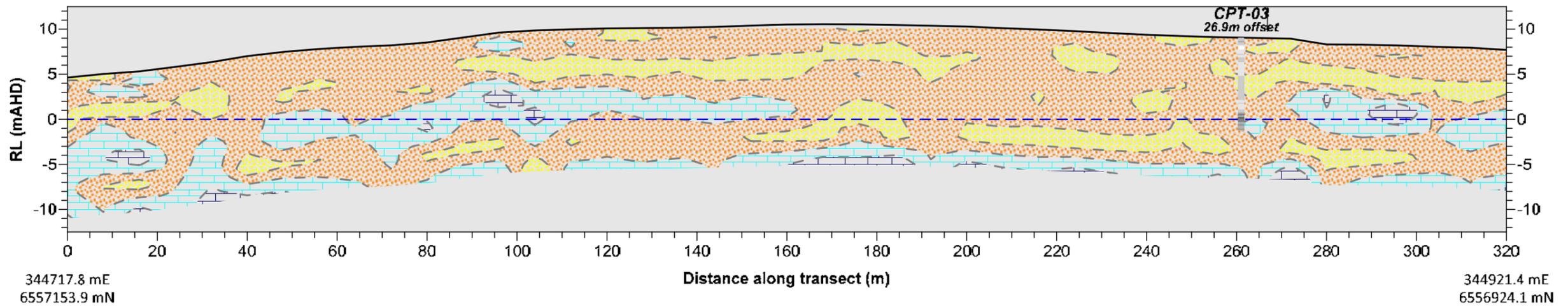
CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
	GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WA	Scale	1:1000H, 1:500V	Drawn	PJE
		Drawing	30731-08	Revised	C

**GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT
LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA**

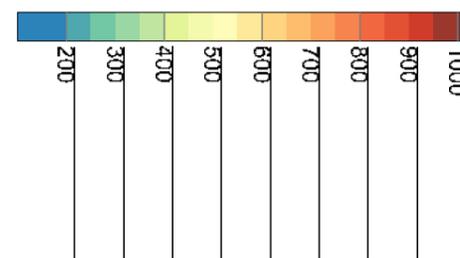
TRANSECT 5 (0-320m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 5 (0-320m) - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

- Tip Resistance (MPa)
- 0 to <5
 - 5 to <10
 - 10 to <15
 - 15 to <20
 - 20 to <25
 - 25 to <30
 - 30 to <35
 - 35 to <40
 - 40 to <45
 - 45 to <50
 - Equal to or >50

NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

CLIENT **DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA**

Date **14 August 2023**

Paper Size **A3**

**GEOPHYSICAL INVESTIGATION FOR COASTAL
EROSION VULNERABILITY ASSESSMENT
LEDGE POINT, SHIRE OF GINGIN WA**

Scale **1:1000H, 1:500V**

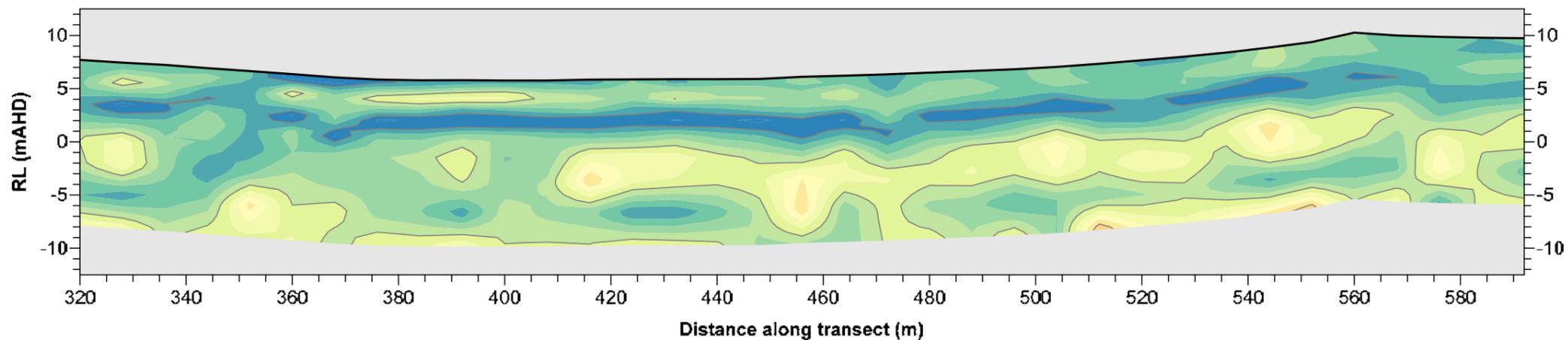
Drawn **PJE**

Drawing **30731-09**

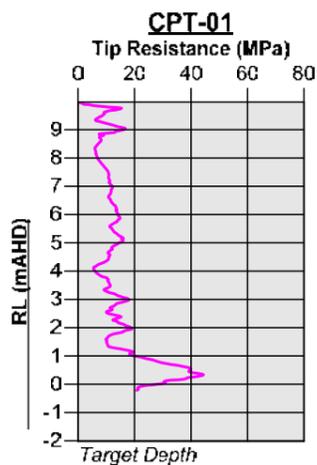
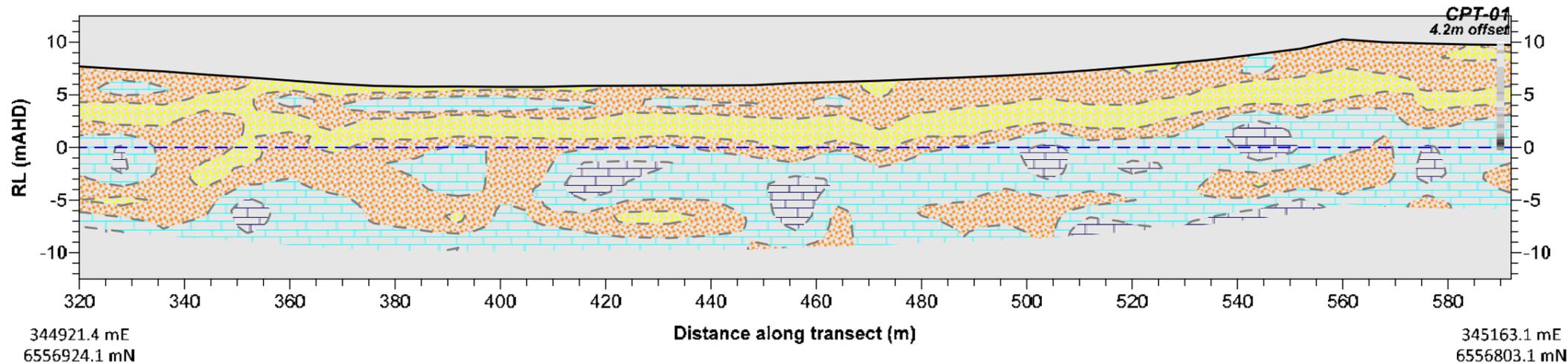
Revised **C**

GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA

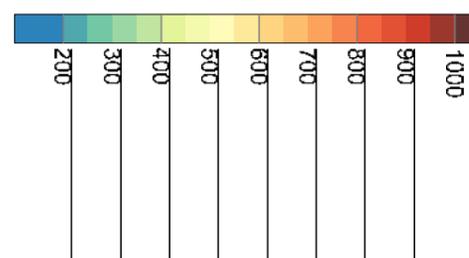
TRANSECT 5 (320-592m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 5 (320-592m) - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

- Tip Resistance (MPa)
- 0 to <5
 - 5 to <10
 - 10 to <15
 - 15 to <20
 - 20 to <25
 - 25 to <30
 - 30 to <35
 - 35 to <40
 - 40 to <45
 - 45 to <50
 - Equal to or >50

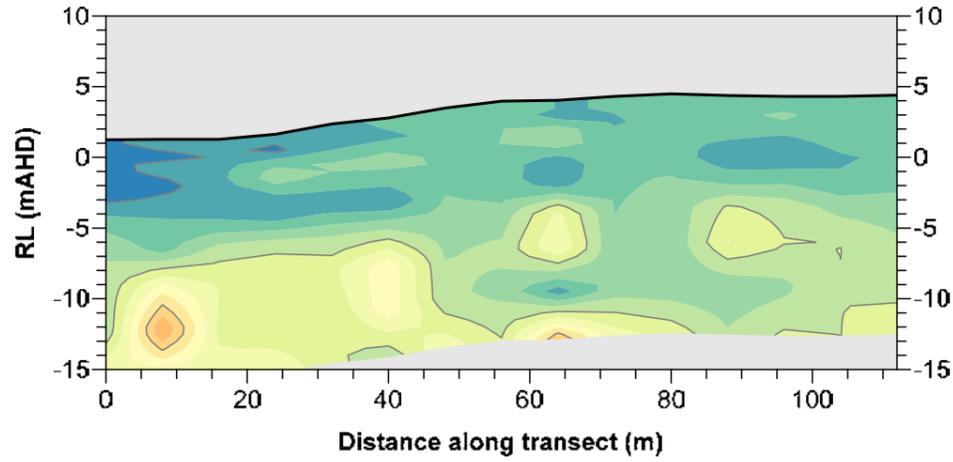
NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

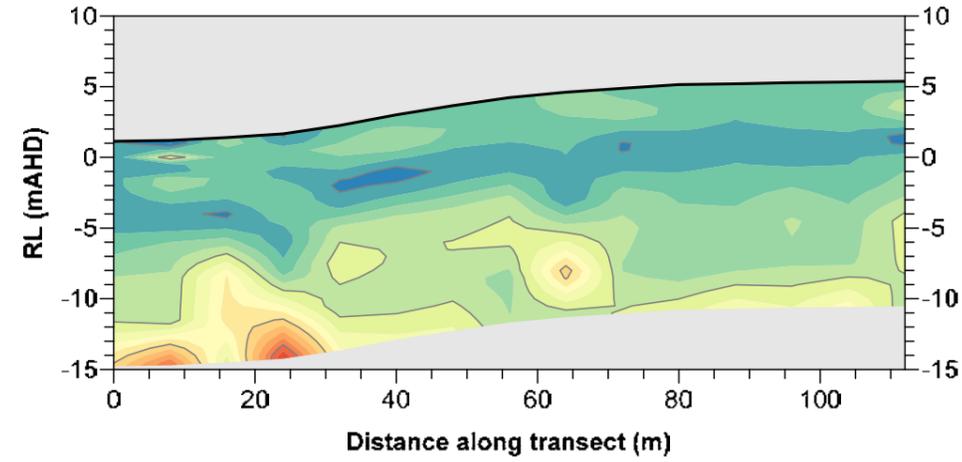
CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
	GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WA	Scale	1:1000H, 1:500V	Drawn	PJE
		Drawing	30731-10	Revised	C

GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT LEDGE POINT, SHIRE OF GINGIN WESTERN AUSTRALIA

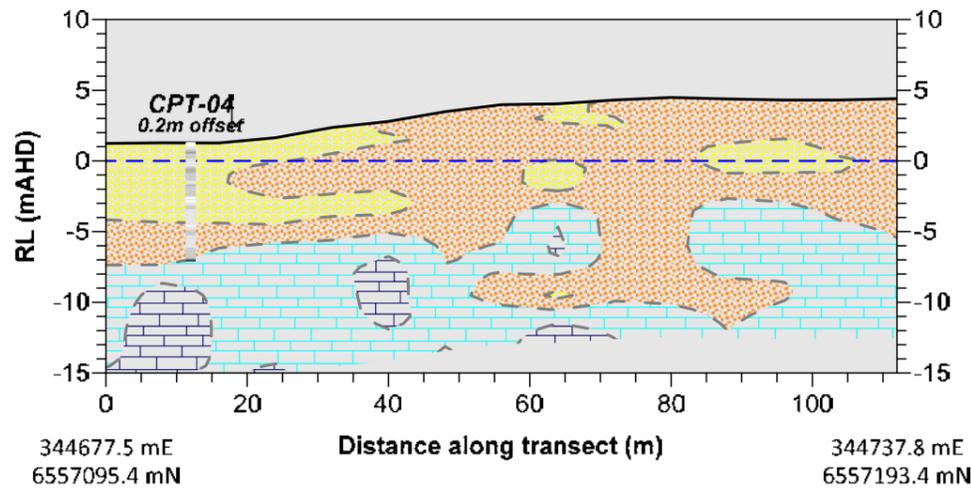
TRANSECT 8 - SEISMIC SHEAR WAVE VELOCITY MODEL



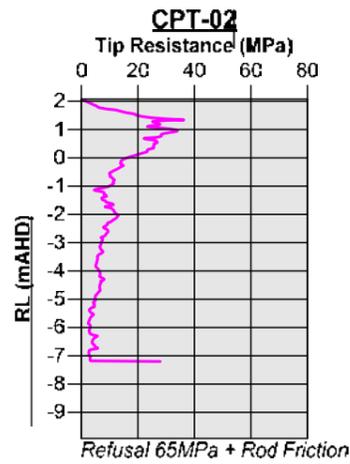
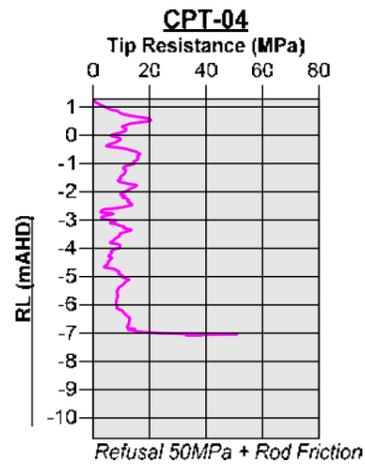
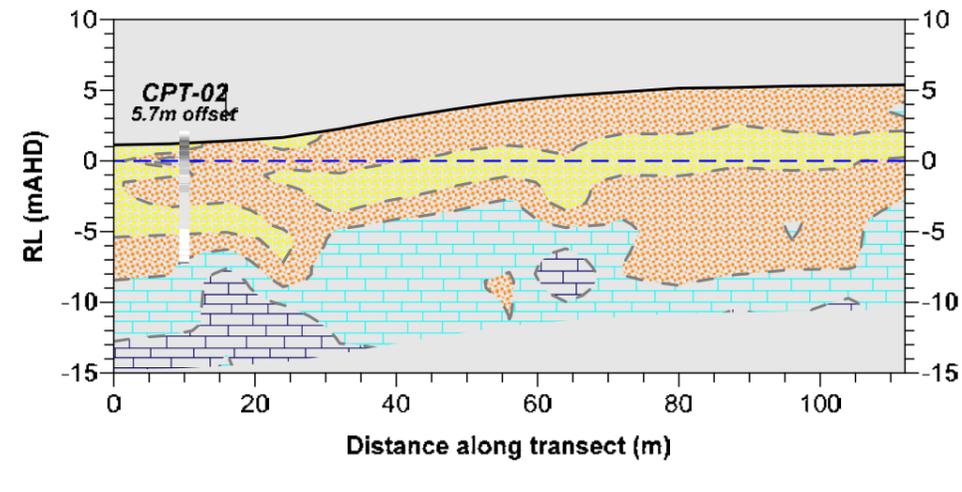
TRANSECT 9 - SEISMIC SHEAR WAVE VELOCITY MODEL



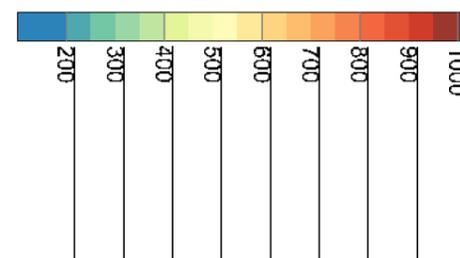
TRANSECT 8 - INTERPRETED GEOLOGICAL SECTION



TRANSECT 9 - INTERPRETED GEOLOGICAL SECTION



SEISMIC S-WAVE VELOCITY (m/s)



INTERPRETED MATERIAL TYPE

- SAND - LOW COMPACTION
S-WAVE VELOCITY < 250 m/s
- SAND - MODERATE COMPACTION
S-WAVE VELOCITY 250-350 m/s
- LOW STRENGTH WEATHERED ROCK
S-WAVE VELOCITY 350-475 m/s
- MODERATE STRENGTH COMPETENT ROCK
S-WAVE VELOCITY > 475 m/s.
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

- Tip Resistance (MPa)
- 0 to <5
 - 5 to <10
 - 10 to <15
 - 15 to <20
 - 20 to <25
 - 25 to <30
 - 30 to <35
 - 35 to <40
 - 40 to <45
 - 45 to <50
 - Equal to or >50

NOTES

Drawing to be used in conjunction with Report 30731.
Positioning is given in GDA 94 zone 50.
Levels are given in Australian Height Datum (AHD).

CLIENT **DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA**

**GEOPHYSICAL INVESTIGATION FOR COASTAL
EROSION VULNERABILITY ASSESSMENT
LEDGE POINT, SHIRE OF GINGIN WA**

Date **14 August 2023**

Scale **1:1000H, 1:500V**

Drawing **30731-12**

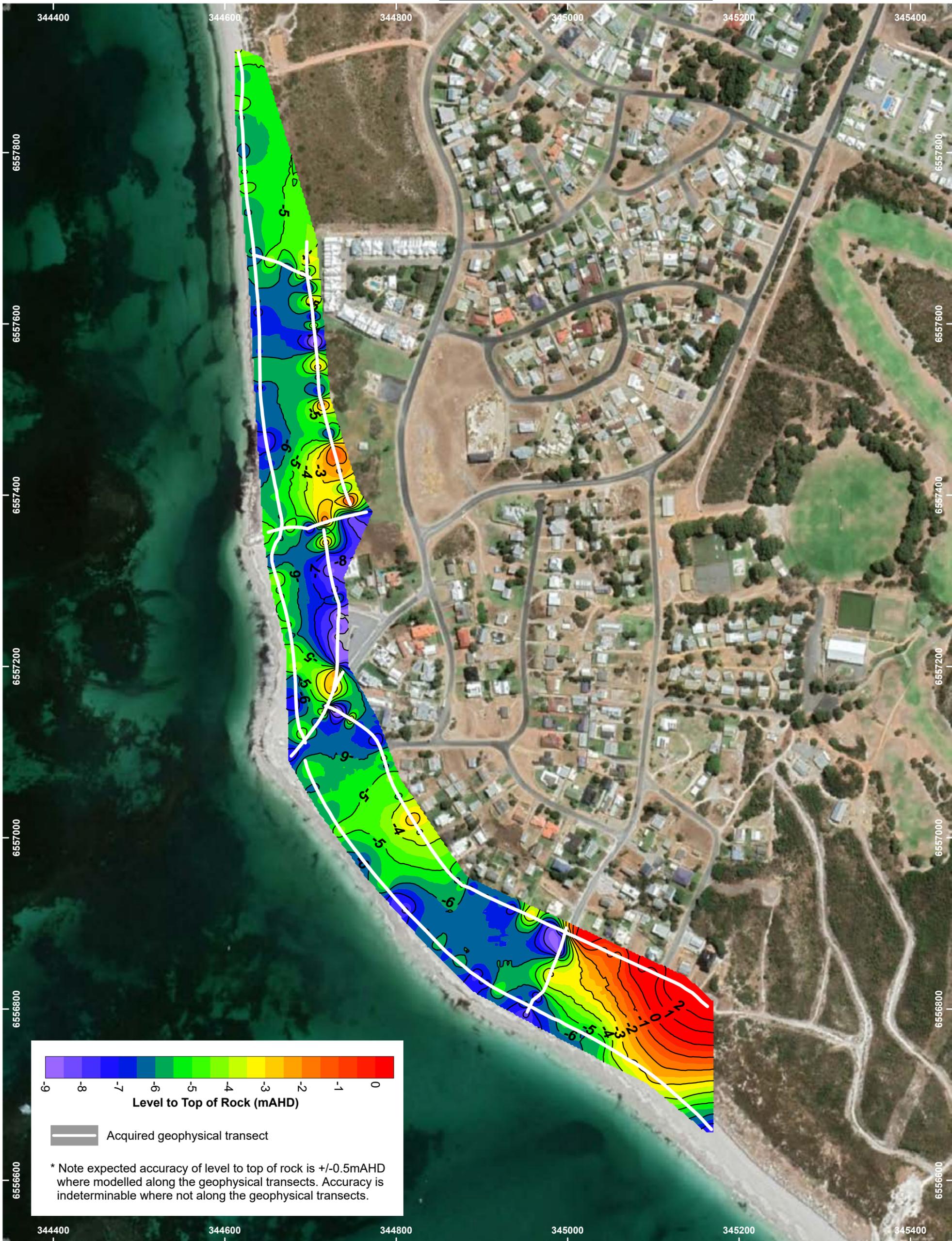
Paper Size **A3**

Drawn **PJE**

Revised **C**

APPENDIX C – MODELLED TOP OF ROCK AND SAND THICKNESS

CONTOURED LEVEL TO TOP OF ROCK



Level to Top of Rock (mAHD)

Acquired geophysical transect

* Note expected accuracy of level to top of rock is +/-0.5mAHD where modelled along the geophysical transects. Accuracy is indeterminable where not along the geophysical transects.

NOTES

Drawing to be used in conjunction with GBG report 30731
 Map Projection GDA94 MGA Zone 50.
 Aerial image from Google Earth Pro

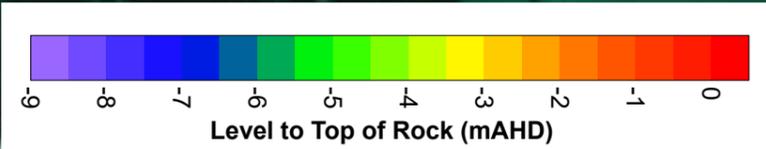
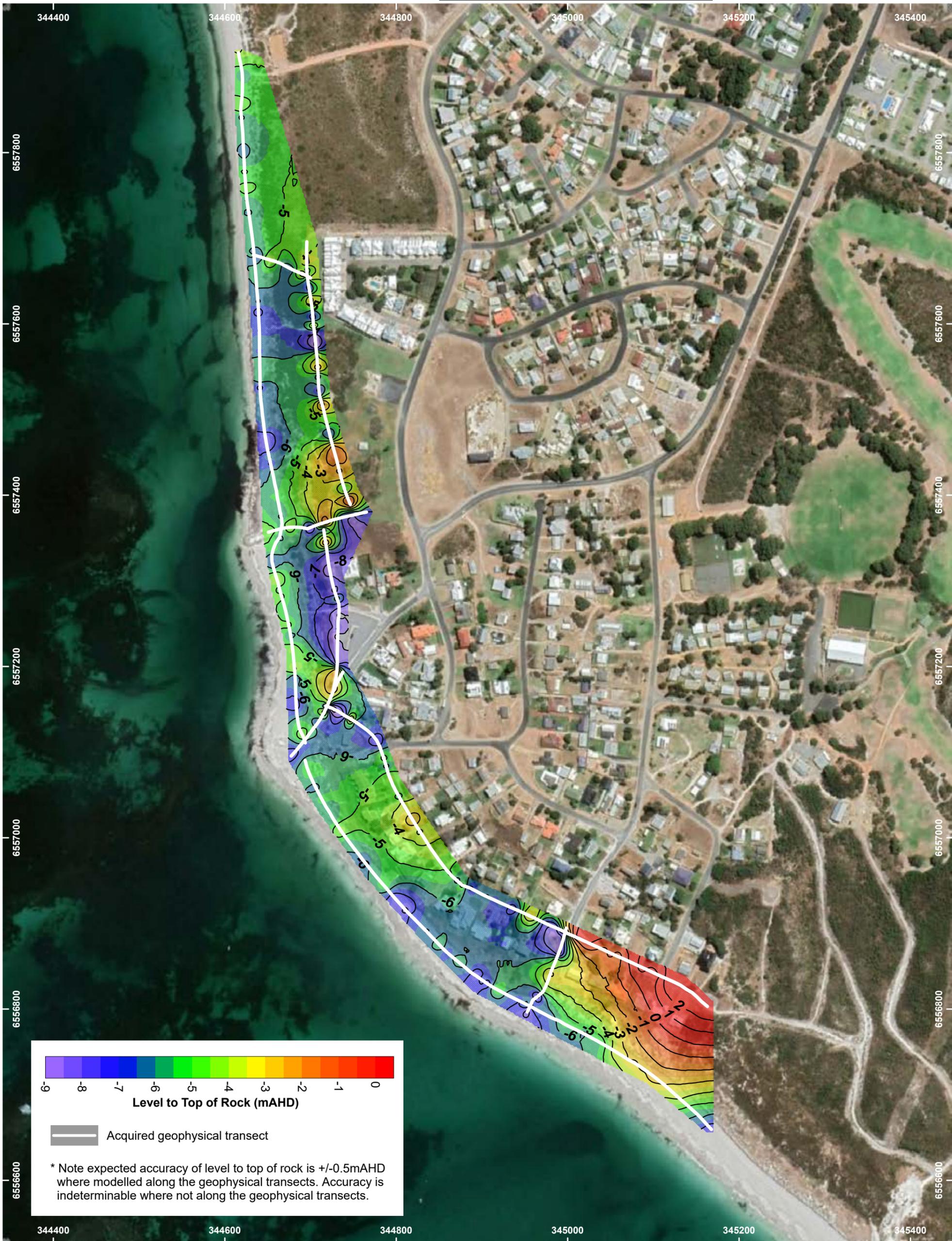


Date	23 August 2023	Paper Size	A3
Scale	1:4000	Drawn	AHWS
Drawing	30731-13	Revised	C

DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

**GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.
LEDGE POINT, SHIRE OF GINGIN WA**

CONTOURED LEVEL TO TOP OF ROCK



— Acquired geophysical transect

* Note expected accuracy of level to top of rock is +/-0.5mAHD where modelled along the geophysical transects. Accuracy is indeterminable where not along the geophysical transects.

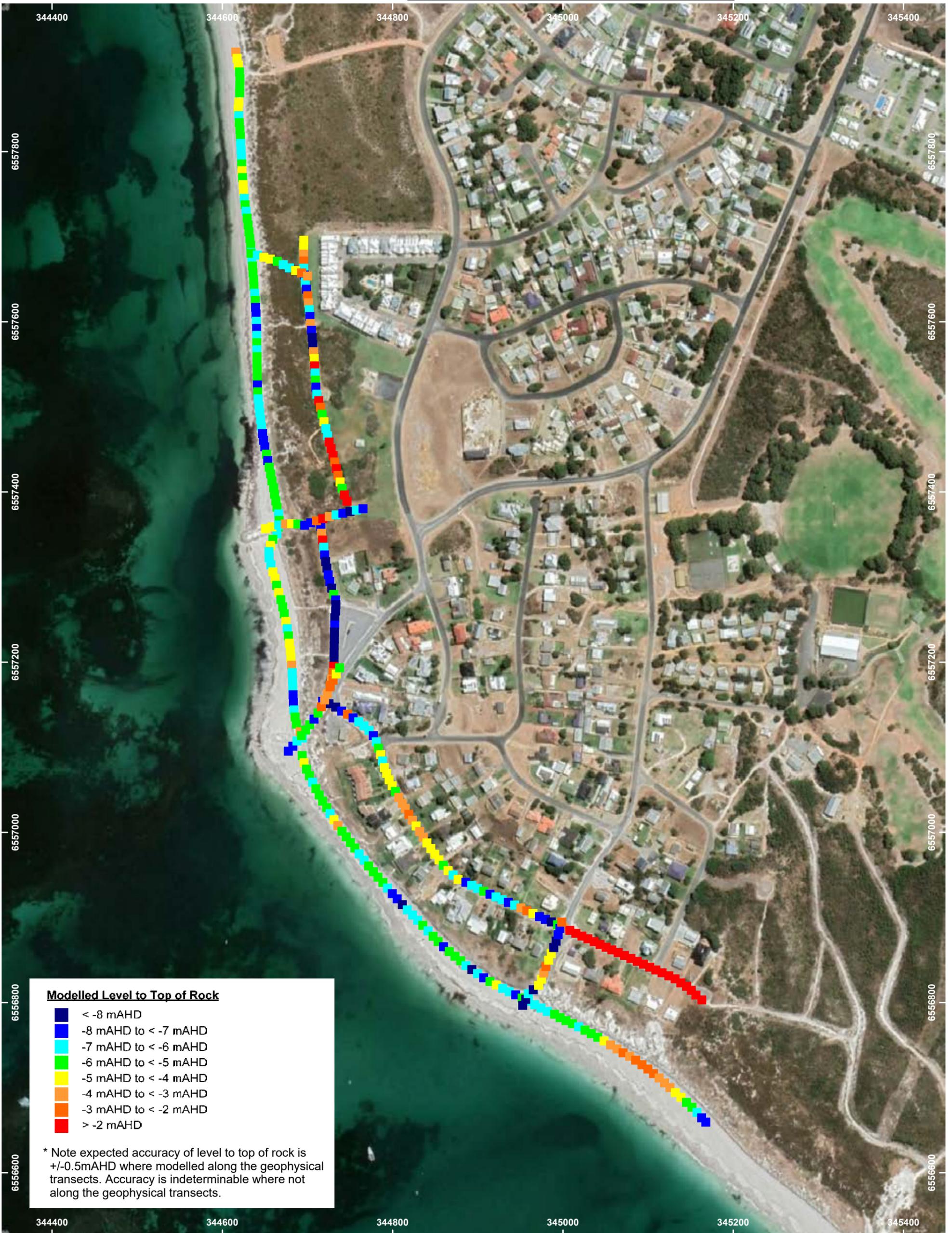
NOTES
Drawing to be used in conjunction with GBG report 30731
Map Projection GDA94 MGA Zone 50.
Aerial image from Google Earth Pro



Date	23 August 2023	Paper Size	A3
Scale	1:4000	Drawn	AHWS
Drawing	30731-14	Revised	C

DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA
GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.
LEDGE POINT, SHIRE OF GINGIN WA

CLASSED POST MAP LEVEL TO TOP OF ROCK



Modelled Level to Top of Rock

- < -8 mAHD
- 8 mAHD to < -7 mAHD
- 7 mAHD to < -6 mAHD
- 6 mAHD to < -5 mAHD
- 5 mAHD to < -4 mAHD
- 4 mAHD to < -3 mAHD
- 3 mAHD to < -2 mAHD
- > -2 mAHD

* Note expected accuracy of level to top of rock is +/-0.5mAHD where modelled along the geophysical transects. Accuracy is indeterminable where not along the geophysical transects.

NOTES

Drawing to be used in conjunction with GBG report 30731
Map Projection GDA94 MGA Zone 50.
Aerial image from Google Earth Pro

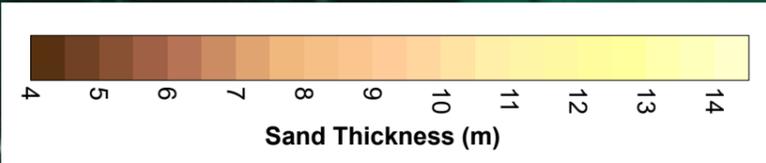
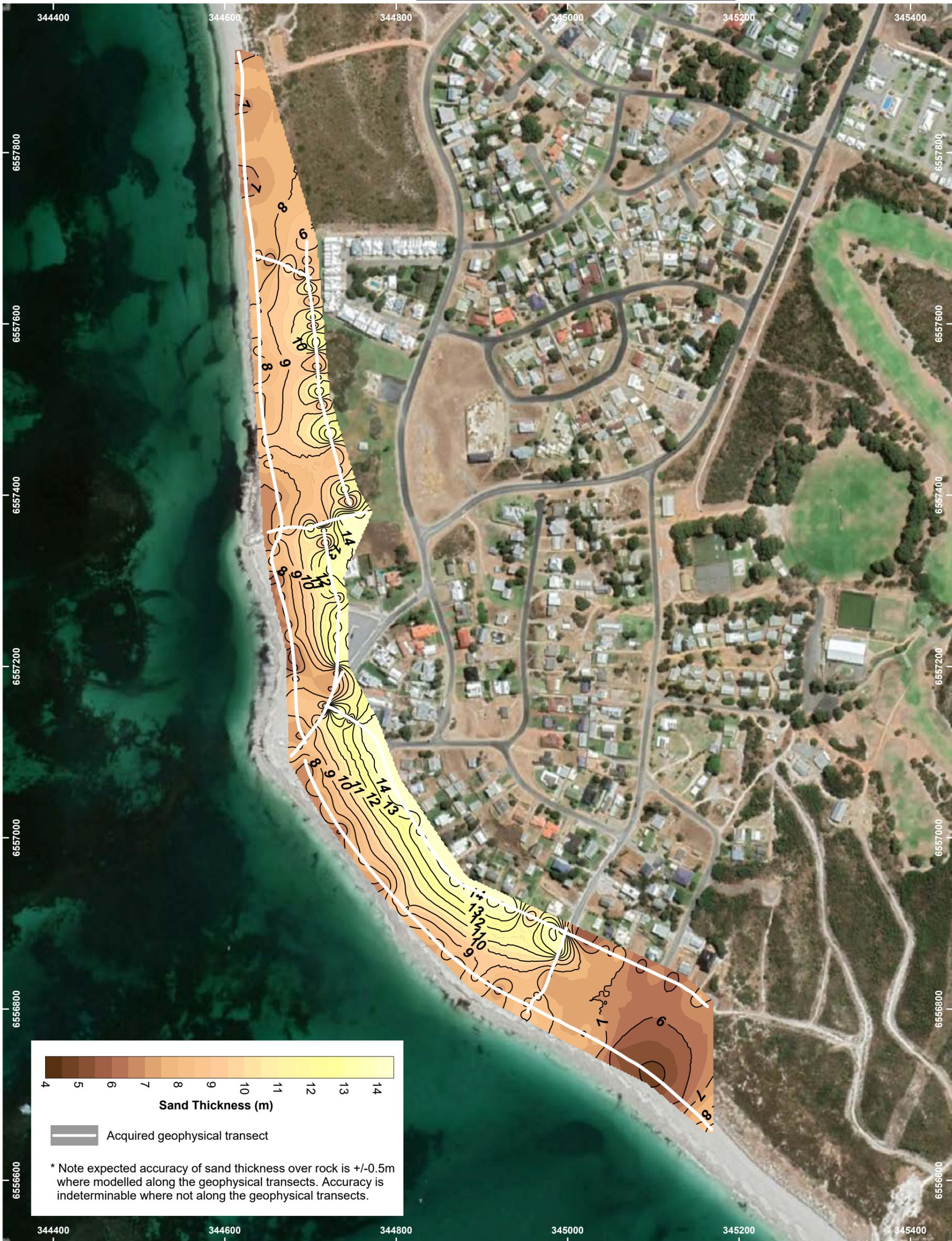


Date	23 August 2023
Scale	1:4000
Drawing	30731-15

Paper Size	A3
Drawn	AHWS
Revisor	C

DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA
GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.
LEDGE POINT, SHIRE OF GINGIN WA

CONTOURED SAND THICKNESS OVER ROCK



— Acquired geophysical transect

* Note expected accuracy of sand thickness over rock is +/-0.5m where modelled along the geophysical transects. Accuracy is indeterminable where not along the geophysical transects.

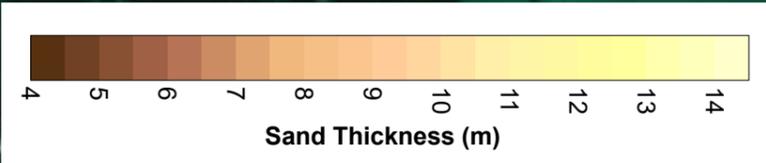
NOTES
Drawing to be used in conjunction with GBG report 30731
Map Projection GDA94 MGA Zone 50.
Aerial image from Google Earth Pro



Date	23 August 2023	Paper Size	A3
Scale	1:4000	Drawn	AHWS
Drawing	30731-16	Revisor	C

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GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.
LEDGE POINT, SHIRE OF GINGIN WA

CONTOURED SAND THICKNESS OVER ROCK



— Acquired geophysical transect

* Note expected accuracy of sand thickness over rock is +/-0.5m where modelled along the geophysical transects. Accuracy is indeterminable where not along the geophysical transects.

NOTES
Drawing to be used in conjunction with GBG report 30731
Map Projection GDA94 MGA Zone 50.
Aerial image from Google Earth Pro



Date	23 August 2023	Paper Size	A3
Scale	1:4000	Drawn	AHWS
Drawing	30731-17	Revised	C

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LEDGE POINT, SHIRE OF GINGIN WA

CLASSIFIED POST MAP SAND THICKNESS OVER ROCK



Modelled Sand Thickness Over Rock

- < 4 m
- 4 m to < 6 m
- 6 m to < 8 m
- 8 m to < 10 m
- 10 m to < 12 m
- 12 m to < 14 m
- > 14 m

* Note expected accuracy of sand thickness over rock is +/-0.5m where modelled along the geophysical transects. Accuracy is indeterminable where not along the geophysical transects.

NOTES

Drawing to be used in conjunction with GBG report 30731
Map Projection GDA94 MGA Zone 50.
Aerial image from Google Earth Pro



Date	23 August 2023
Scale	1:4000
Drawing	30731-18

Paper Size	A3
Drawn	AHWS
Revised	C

DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA
GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.
LEDGE POINT, SHIRE OF GINGIN WA

ELECTRIC FRICTION-CONE PENETROMETER

Probe I.D

CLIENT: Department of Transport

Job No.: 3073

PROJECT: Geophysical Investigation for Coastal Erosion Study

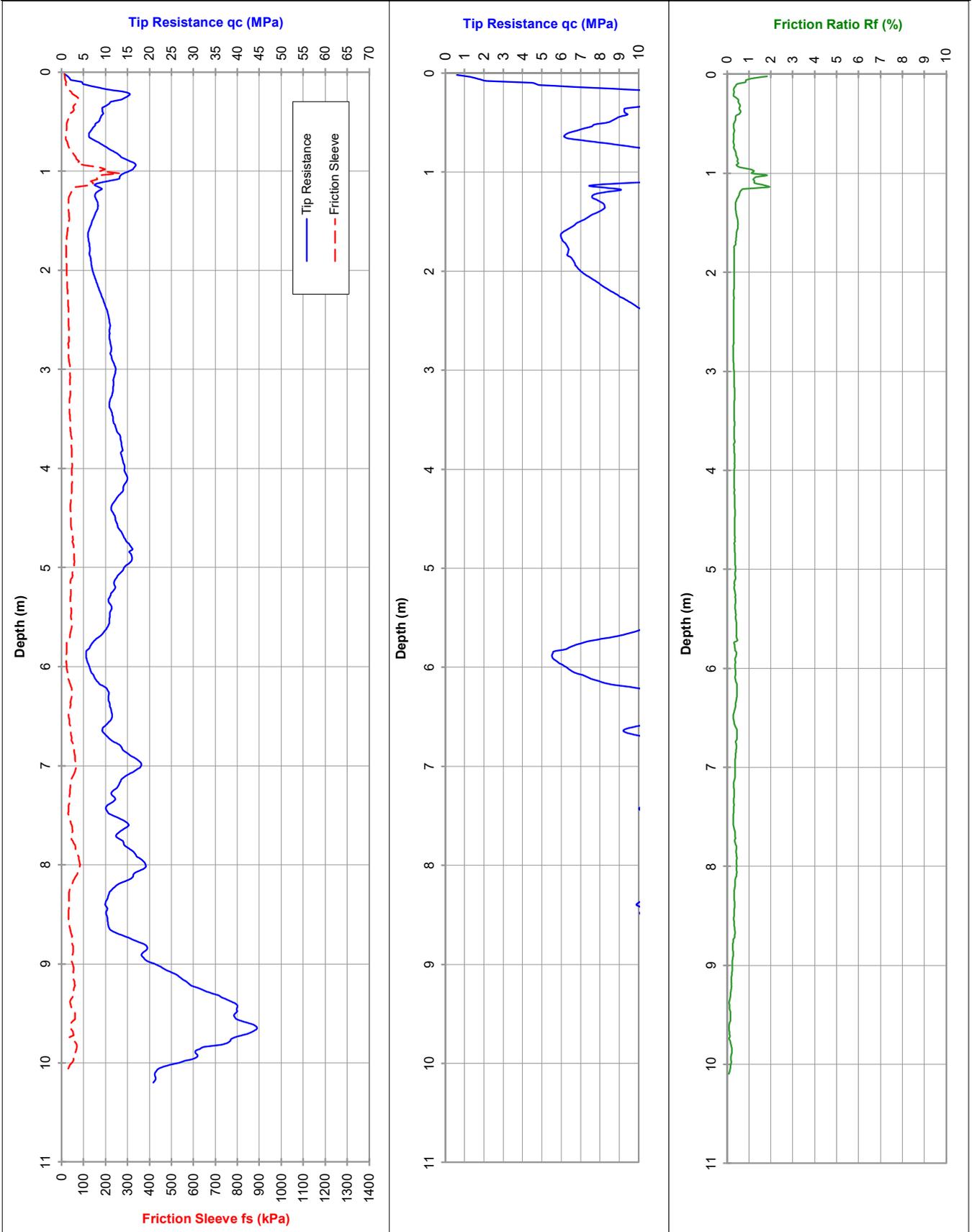
RL (m):

LOCATION: Ledge Point

Co-ords:

CPT 01

10-Jul-23



Tested in accordance with AS 1289.6.5.1-1999 and IRTF 2001 for friction reducer

Approx. water (m): 9.2

Dummy probe to (m):

Refusal:

Cone I.D.: EC46

File: GB0029TT

Rig Type: 22t truck (Track-Truck)

ELECTRIC FRICTION-CONE PENETROMETER

Probe I.D

CLIENT: Department of Transport

Job No.: 3073

PROJECT: Geophysical Investigation for Coastal Erosion Study

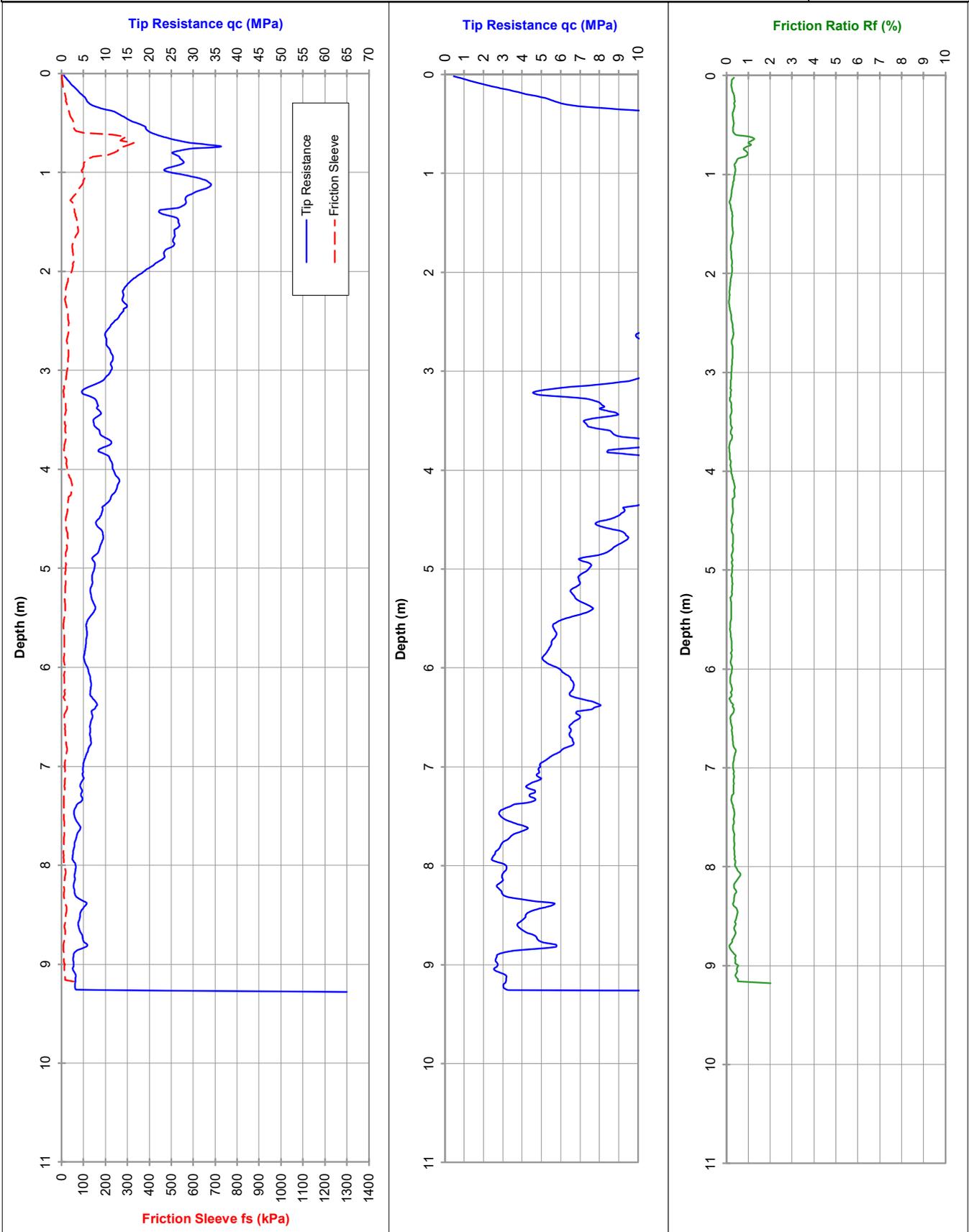
RL (m):

LOCATION: Ledge Point

Co-ords:

CPT 02

11-Jul-23



Tested in accordance with AS 1289.6.5.1-1999 and IRTTP 2001 for friction reducer

Approx. water (m): Dry to 1.0

Dummy probe to (m):

Refusal: 65 MPa + Rod Friction

Cone I.D.: EC46

File: GB0031T

Rig Type: 7t track

ELECTRIC FRICTION-CONE PENETROMETER

Probe I.D

CLIENT: Department of Transport

Job No.: 3073

PROJECT: Geophysical Investigation for Coastal Erosion Study

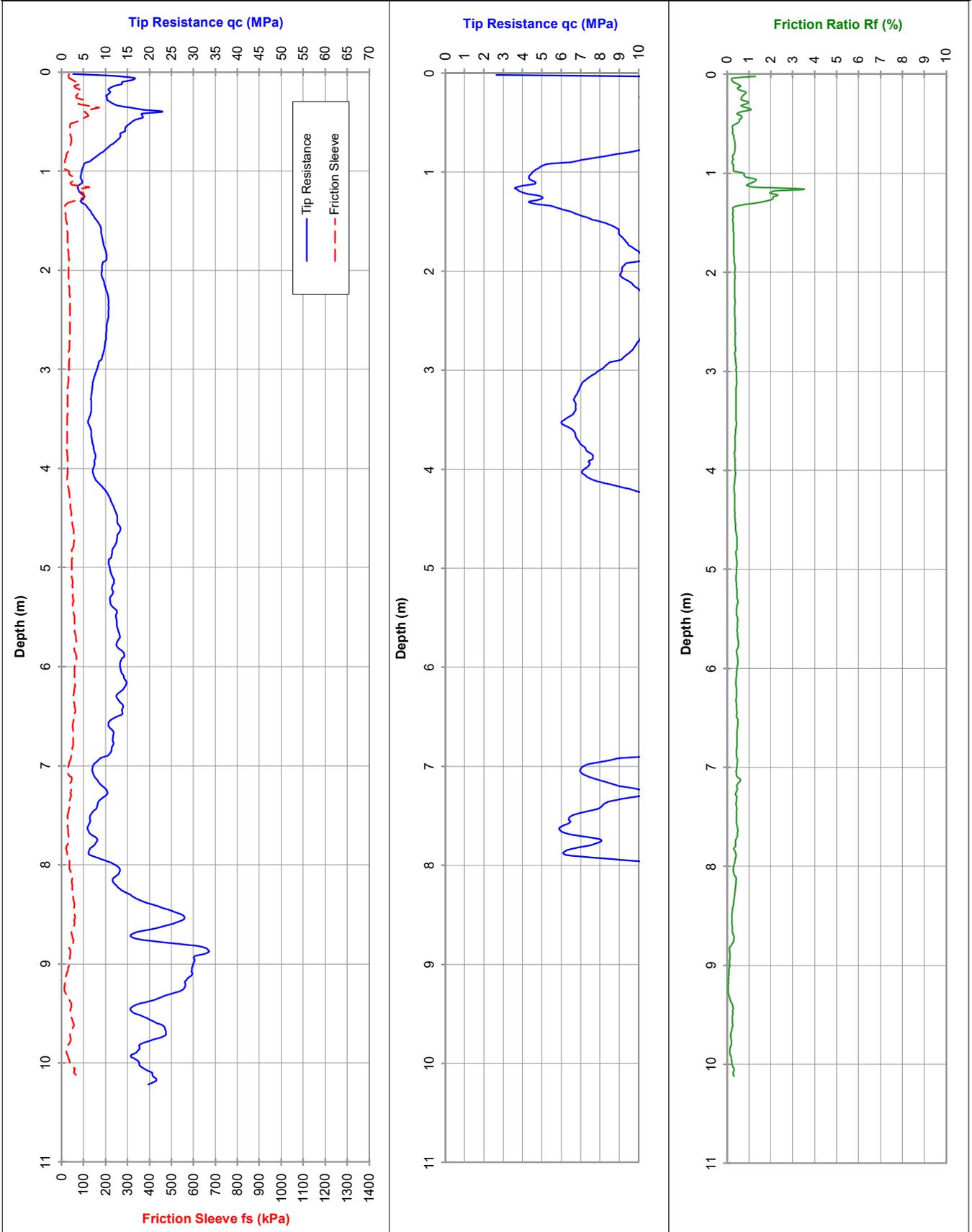
RL (m):

CPT 03

LOCATION: Ledge Point

Co-ords:

10-Jul-23



Tested in accordance with AS 1289.6.5.1-1999 and IRTF 2001 for friction reducer

Approx. water (m): Dry to 10.0

Dummy probe to (m):

Refusal:

Cone I.D.: EC46

File: GB0030TT

Rig Type: 22t truck (Track-Truck)

ELECTRIC FRICTION-CONE PENETROMETER

Probe I.D

CLIENT: Department of Transport

Job No.: 3073

PROJECT: Geophysical Investigation for Coastal Erosion Study

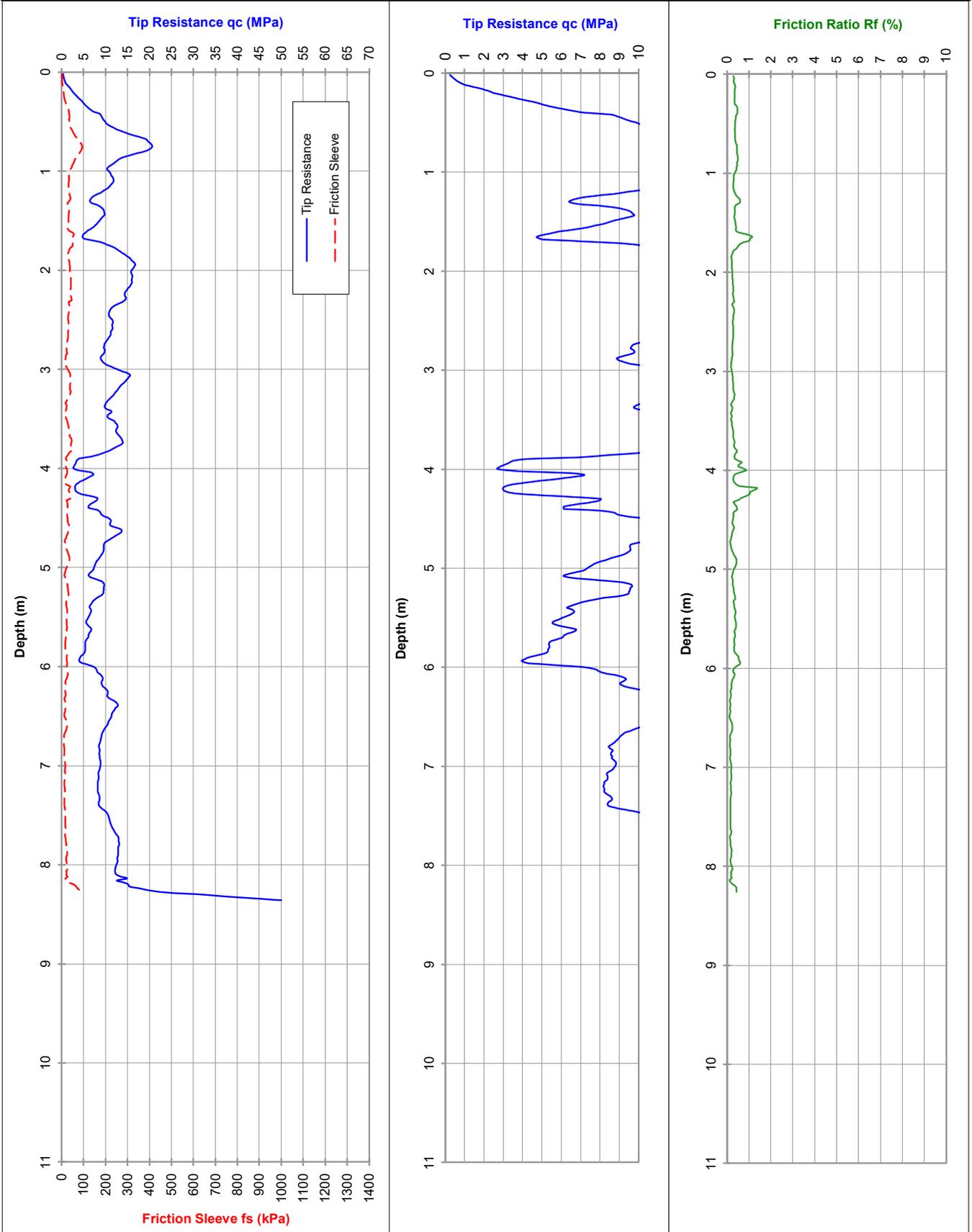
RL (m):

CPT 04

LOCATION: Ledge Point

Co-ords:

11-Jul-23



Tested in accordance with AS 1289.6.5.1-1999 and IRTTP 2001 for friction reducer

Approx. water (m): Dry to 1.0

Dummy probe to (m):

Refusal: 50 MPa + Rod Friction

Cone I.D.: EC46

File: GB0032T

Rig Type: 7t track

ELECTRIC FRICTION-CONE PENETROMETER

Probe I.D

CLIENT: Department of Transport

Job No.: 3073

PROJECT: Geophysical Investigation for Coastal Erosion Study

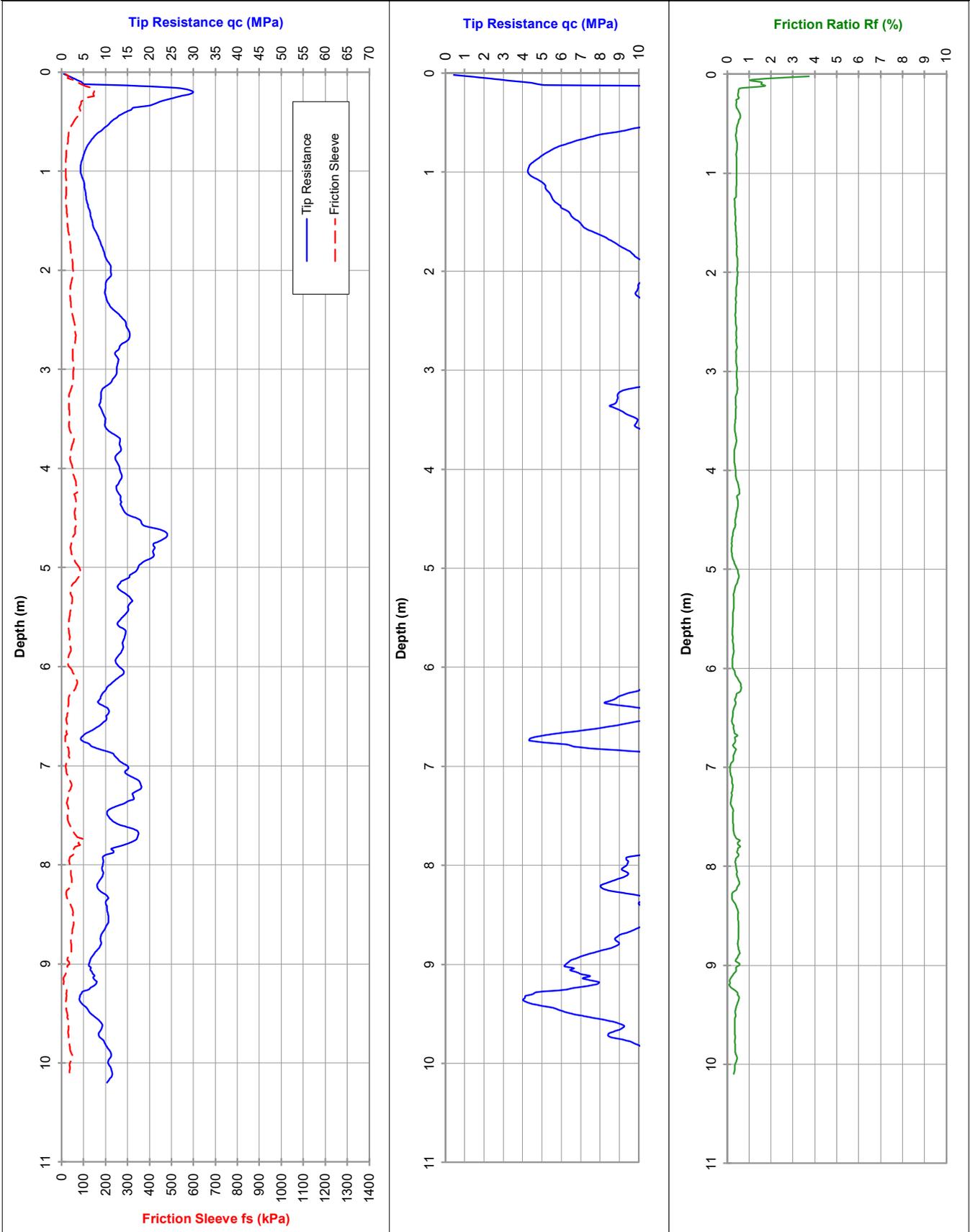
RL (m):

CPT 05

LOCATION: Ledge Point

Co-ords:

11-Jul-23



Tested in accordance with AS 1289.6.5.1-1999 and IRTF 2001 for friction reducer

Approx. water (m): 4.2

Dummy probe to (m):

Refusal:

Cone I.D.: EC46

File: GB0033T

Rig Type: 7t track

ELECTRIC FRICTION-CONE PENETROMETER

Probe I.D

CLIENT: Department of Transport

Job No.: 3073

PROJECT: Geophysical Investigation for Coastal Erosion Study

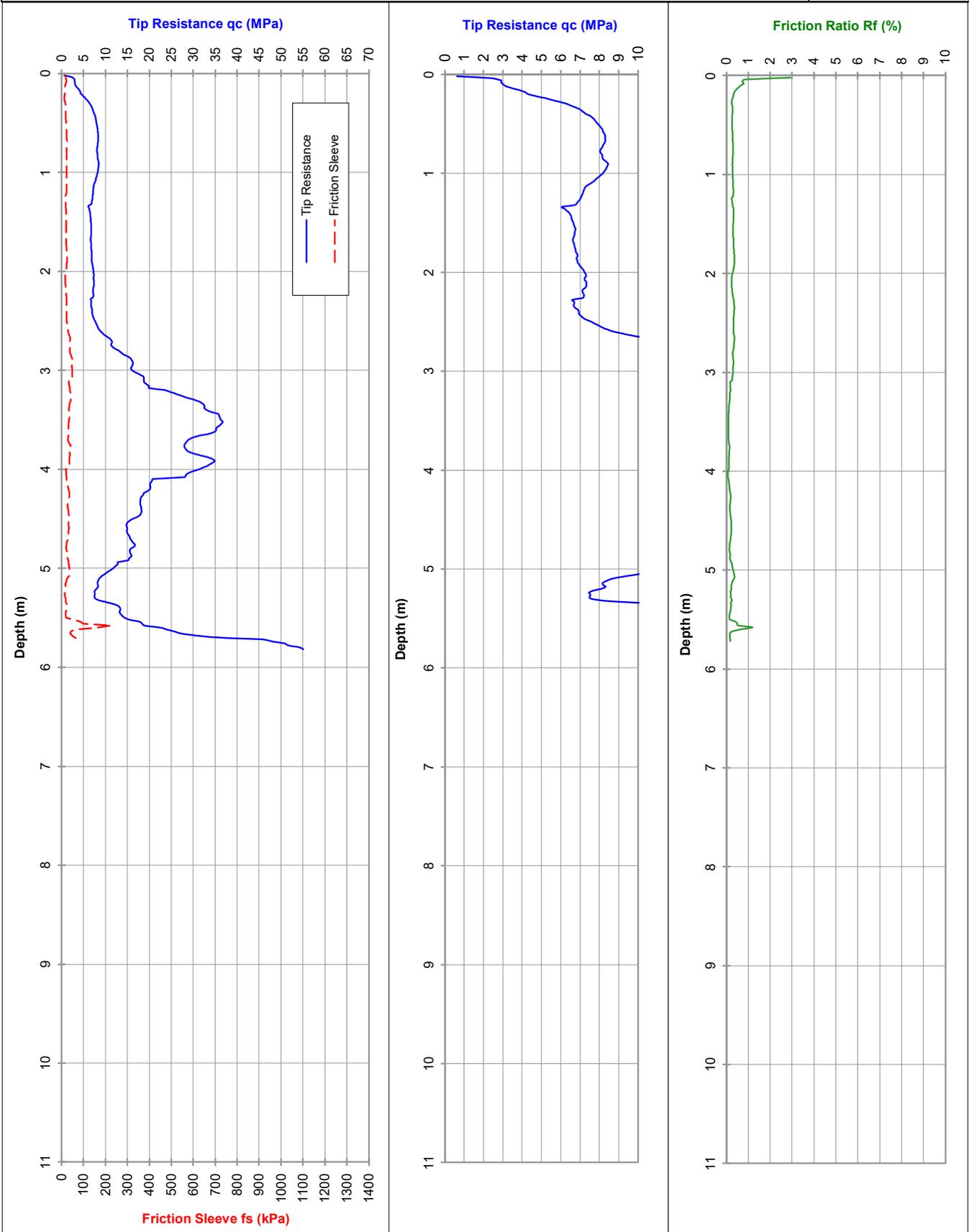
RL (m):

CPT 06

LOCATION: Ledge Point

Co-ords:

11-Jul-23



Tested in accordance with AS 1289.6.5.1-1999 and IRTTP 2001 for friction reducer

Approx. water (m): Dry to 4.8

Dummy probe to (m):

Refusal: 55 MPa + Rod Friction

Cone I.D.: EC46

File: GB0035T

Rig Type: 7t track

ELECTRIC FRICTION-CONE PENETROMETER

Probe I.D

CLIENT: Department of Transport

Job No.: 3073

PROJECT: Geophysical Investigation for Coastal Erosion Study

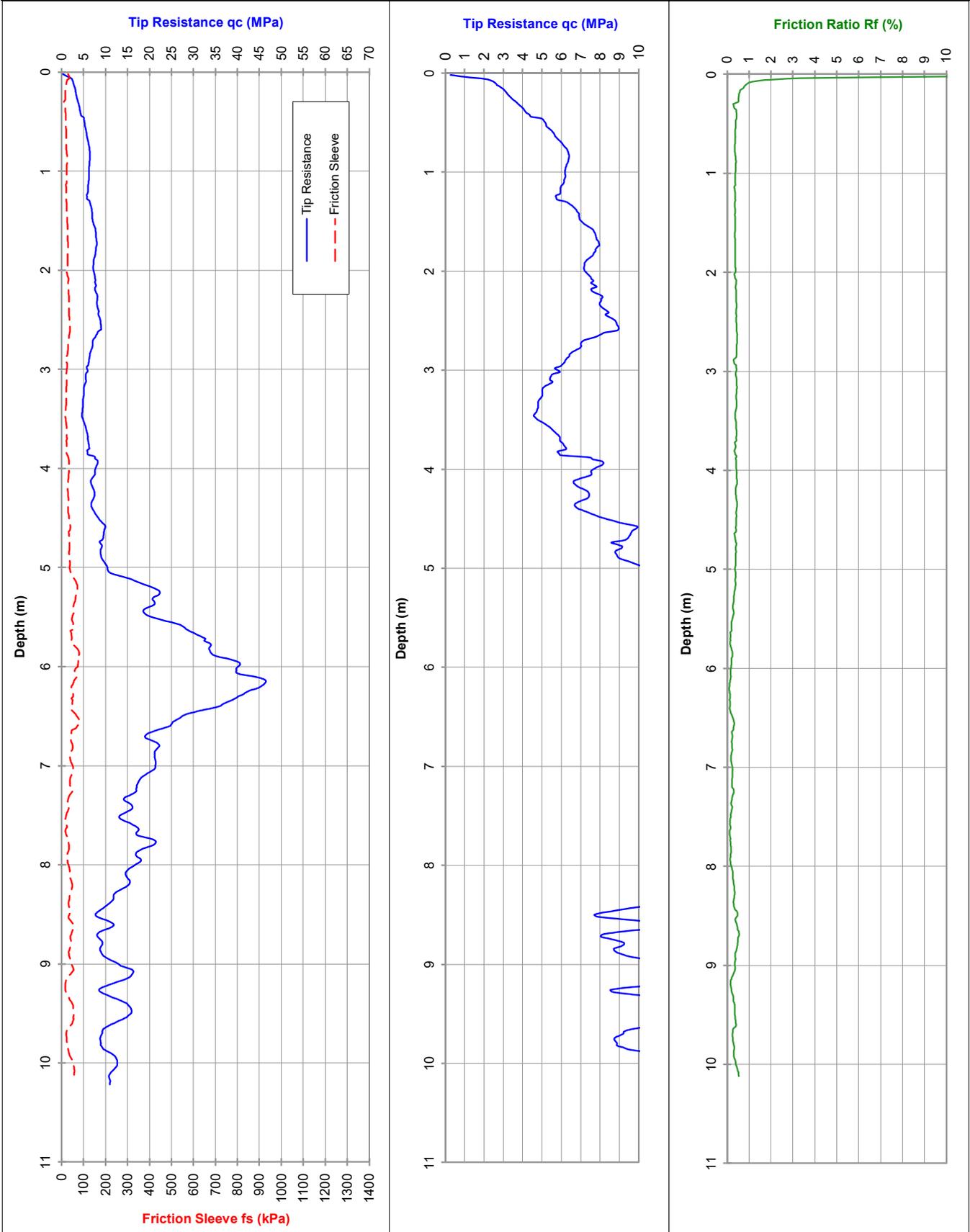
RL (m):

CPT 07

LOCATION: Ledge Point

Co-ords:

11-Jul-23



Tested in accordance with AS 1289.6.5.1-1999 and IRTF 2001 for friction reducer

Approx. water (m): 6.2

Dummy probe to (m):

Refusal:

Cone I.D.: EC46

File: GB0034T

Rig Type: 7t track

CALIBRATION CERTIFICATE

CONE ID: EC46

Cone Type:	Compression
Calibration Date (qc/fs):	9 May 2023
Calibration Date (u):	7 December 2022
Preliminary Inspection:	Pass
Calibrated By:	Henry Lawer
Calibration Procedure:	ISO 22476-1:2012, IRTP 2001
Force Application:	Compression
Reference Equipment:	PT - S type 100kN Serial # 5126009 (Calibrated 10/03/23 - NATA approved Cert. No. 230664) Bongshin - S type 50kN Serial #W05345 (Calibrated 10/03/23 - NATA approved Cert. No. 230663) Digitron Panel Meter Serial #: 060213/01 (Calibrated 09/03/23 - NATA endorsed Report No. 230658, 230659, 230660)

Note: In accordance with AS1289 F5.1 the force calibration derived by NATA Calibration Certificates are converted to a qc reading in MPa and fs reading in kPa by dividing by 1000 mm² and 15000mm² respectively.

Results of Calibration:

qc (tip resistance):		
Capacity:		100 (MPa)
Area		1000 (mm ²)
Applied Load kN	Eqv. Pressure MPa	Mean Observed Reading Volts
0	0	0.000
10	10	0.742
20	20	1.502
30	30	2.267
40	40	3.035
50	50	3.800
60	60	4.564
70	70	5.324
80	80	6.087
90	90	6.852
100	100	7.616
90	90	6.860
80	80	6.101
70	70	5.343
60	60	4.582
50	50	3.820
40	40	3.058
30	30	2.291
20	20	1.523
10	10	0.753
0	0	0.002
R ² Value =	1.000	

fs (sleeve friction):		
Capacity:		2000 (kPa)
Area		15000 (mm ²)
Applied Force kN	Eqv. Load kPa	Mean Observed Reading Volts
0	0	0.000
3	200	0.738
6	400	1.498
9	600	2.265
12	800	3.022
15	1000	3.776
18	1200	4.531
21	1400	5.286
24	1600	6.042
27	1800	6.800
30	2000	7.558
27	1800	6.835
24	1600	6.085
21	1400	5.332
18	1200	4.577
15	1000	3.821
12	800	3.064
9	600	2.302
6	400	1.535
3	200	0.772
0	0	0.003
R ² Value =	1.000	

u (pore pressure):		
Capacity:		3500 (kPa)
Position		u2
Applied Pressure bar	Eqv. Pressure kPa	Mean Observed Reading Volts
0	0	0.000
3	300	0.414
6	600	0.830
9	900	1.243
12	1200	1.656
15	1500	2.070
18	1800	2.483
21	2100	2.895
25	2500	3.444
30	3000	4.130
35	3500	4.816
30	3000	4.137
25	2500	3.455
21	2100	2.900
18	1800	2.489
15	1500	2.074
12	1200	1.660
9	900	1.246
6	600	0.830
3	300	0.416
0	0	0.000
R ² Value =	1.000	

Zero Load Error: 0.03%
Max. Linearity 0.31%
Max. Hysteris 0.33%

Zero Load Error: 0.03%
Max. Linearity 0.47%
Max. Hysteris 0.62%

Zero Load Error: 0.01%
Max. Linearity 0.24%
Max. Hysteris 0.23%

MPa/Volt: 13.109

kPa/Volt: 264.13

kPa/Volt: 726.10
Net Area (calibrated): 0.83

"Class 1" Application Accuracy achieved (in accordance with ISO 22476:2012 classification)

Calibration Checked & Authorised: Kylie Walker

Job Details

Client: GB Geotechnics
Rep: Stephen Kelly
Location: Seabird

Date of Job: 10/07/23
Tip Diameter: 35.52
Sleeve Diameter: 35.81

MOROOKA (M2)

11 tonne track mounted CPT Rig



SPECIFICATIONS

Overall Dimensions	Width: 2.3m; Length: 5.3m; Height: 3.2m (while travelling) Height: 4.4m (while probing)
Gross Weight	11 tonne
Ground Bearing Capacity	0.38 kg/cm ² (37kPa / 5.4psi)
Speed (Low/High)	Low gear: 8.3km High gear: 12km/h on level ground
Grade ability	60%
Engine	Mitsubishi (3910cc) 110 HP @ 2,800 rpm
Fuel Tank	80 L (Diesel)
Drive System	HST
Tracks	600mm wide rubber tracks
Levelling Jacks	0.8m stroke

EQUIPMENT / FEATURES

Other Equipment / Features	2.4m x 1.2m Plastic Bog Boards 1 x 9kg ABE Fire extinguisher Air conditioned work cabin and drive cabin
Transport	Prime Mover & 10m Drop-deck trailer with ramps

SERVICES

Geotechnical Services provided	CPT, CPTu, SCPT, SCPTu (1, 5, 10, & 15 tonne cones) DMT, SDMT Dissipation Testing Ball Penetrometer CPT casing for additional rod support Dual Tube (percussion) sampling Piston Sampling MOSTAP and PROBEDRILL soil sampling Vane Shear Testing (Electronically driven) Vibrating Wire Installation Water Sampling Standpipe Installation (20mm; 32mm & 50mm)
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APPENDIX D – CONE PENETRATION TEST PLOTS