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Report

Geotechnical Investigation for Coastal Erosion Vulnerability Assessment.

Peaceful Bay, Shire of Denmark WA.

Date: 8 September 2023 Report Ref: 3073B FINAL



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EXECUTIVE SUMMARY

A geotechnical investigation has been carried out as part of a coastal erosion assessment at Peaceful Bay in the Shire of Denmark, Western Australia. During the investigation ground geophysical and intrusive geotechnical testing was conducted within a 700m corridor of coastal beach and dune formation adjacent to the Peaceful Bay settlement which has been identified as an at-risk site as part of Coastal Hotspot #50.

The investigation scope consisted of acquiring multi-channel analysis of surface waves data as a series of specified transects either along-shore (parallel to the coast) or cross-shore (perpendicular to the coast) and cone penetration testing at spot locations along these transects. This was supplemented with geological mapping of surface rock outcrops and topographic survey using high resolution aerial photogrammetry for the generation of a surface level model and orthomosaic image.

The acquired MASW dataset was processed for the generation of seismic velocity sections along the transects showing variations in the seismic shear wave velocity of the subsurface material to a target depth of 10-15m below ground level. The seismic velocity sections were calibrated with the CPT plots and demarcated into velocity ranges representing different material types and conditions for the generation of interpreted geological sections consisting of loose to compacted sediment and variably weathered to fresh rock.

The interpreted geological sections have been compiled to develop subsurface models of the level to rock substrate (relative to AHD) and overlying sand thickness within the region between the foreshore and the future development. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the future development.

The following observations have been made:

- Interpreted rock substrate was observed along the majority of the transects and within the maximum target investigation depth of 10-15m below ground level.
- Interpreted top of rock substrate on the along-shore transects on the beach ranges from -11.5mAHD to -0.5mAHD and averages approximately -5mAHD, and is overlain by an average of 6.5m of variably compacted sediment.
- Interpreted top of rock substrate on the along-shore transects adjacent to the settlement including along Old Peaceful Bay Road ranges from -14mAHD to 1mAHD and averages approximately -7mAHD, and is overlain by an average of 12m of variably compacted sediment.
- Interpreted top of rock substrate for the cross-shore transects extending over the dune formation ranges from -3mAHD to 2.5mAHD and averages -0.25mAHD, and is overlain by an average of 5m of variably compacted sediment.



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1 INTRODUCTION

At the request of The Government of Western Australia Department of Transport (DoT), GBG Group carried out a geotechnical investigation at Peaceful Bay, Shire of Denmark in July 2023. During the investigation seismic geophysical testing and intrusive geotechnical testing was conducted within a 700m corridor of coastal beach and dune formation which has been identified as an at risk site as part of Coastal Hotspot #50.

The objective of the investigation was to provide detailed mapping of the extent, elevation and consistency/strength of the rock underlying the coastal beach and dune formation. In particular, the key outcome of the investigation was to develop a subsurface model of the level to competent rock substrate (relative to AHD) within the region between the foreshore and the settlement. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the settlement.

To achieve the project objectives, data from the following investigation methods was acquired, processed and analysed so as to obtain the required subsurface information within the anticipated geological conditions:

- 1. **Geological mapping** of surface rock outcrops within the study area using high resolution photogrammetry.
- 2. **Geophysical testing** by way of Multi-channel Analysis of Surface Waves (MASW) to obtain seismic shear wave velocity models related to variations in subsurface material stiffness.
- 3. **Intrusive geotechnical testing** by way of Cone Penetration Testing (CPT) to measure sediment strength and compressibility, and for calibration and ground truthing of the geophysical dataset.
- 4. Topographic survey using Differential GNSS receiver and photogrammetry.

2 INVESTIGATION SITE

The investigation was carried out within an approximate 700m corridor of coastal beach and dune formation extending from the foreshore to the east, and to Old Peaceful Bay Road to the west from East Avenue to north of the Peaceful Bay Boat Ramp. The extent of the investigation site is shown as a yellow dashed area in Figure 1.

Data was acquired as a series of transects for the seismic geophysical testing and point locations for the intrusive geotechnical testing. These were positioned so as to best utilise existing roads, tracks, and beach whilst not impacting native vegetation and in order to ensure the most optimal, efficient and economical acquisition methodology. Data was not acquired where surface obstructions were present such as thick vegetation, steep topography or where the beach was inundated with seawater. Photographs showing the typical site conditions are provided in Figure 2.



Topography at the site was undulating with an elevation difference between the foreshore at ~0-2mAHD, the dune formation at ~2-6mAHD, and the existing settlement including the Peaceful Bay Caravan Park greater than 4mAHD. A topographic high of greater than 18mAHD is located to then north of the caravan park. A topographic map showing surface level is provided in Appendix C drawing 3073B-07.

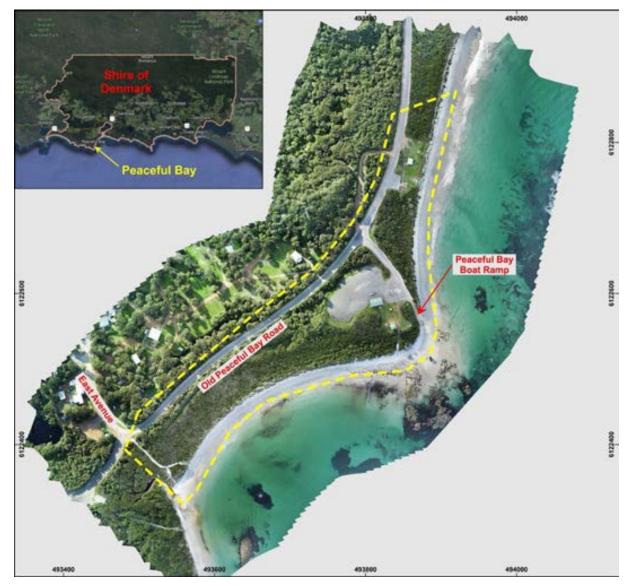


Figure 1: The extent of the geophysical investigation (yellow polygon) at Parry Beach. Aerial imagery from drone photogrammetry (main image) and Google Maps (inset image).





Figure 2: Site conditions at Peaceful Bay including on Old Peaceful Bay Road (left image) and the Peaceful Bay Boat Ramp (right image).

3 INVESTIGATION METHODOLOGY

3.1 FIELD SURVEY LOGISTICS

Geophysical data acquisition was carried out on the 12 and 13 July 2023 by a two-person crew from GBG Group consisting of qualified geophysicists. CPT data acquisition was carried out by a technician from Probedrill on the 12 July 2023. Where required, the site work was carried out under appropriate traffic and pedestrian management commissioned by the Shire of Denmark.

Prior to the commencement of data acquisition, a site assessment was carried out with representatives from the Shire of Denmark. Potential concerns and issues including the placement of and access to the MASW transects and CPT points were addressed and the initial indicative survey plan was adjusted, where necessary.

The site work for the investigation consisted of a total of 1464m MASW profiling acquired as 3 alongshore transects (parallel to the coast) and 2 cross-shore transects (perpendicular to the coast), and a total of 5 CPT points along the transects. Details of the acquired MASW transects and CPT points are provided in Tables 1 and 2 respectively. The extents of the MASW transects and locations of the CPT points overlaid onto aerial imagery are shown in Appendix A drawing 3073B-01.

Transect	Orientation	Start Co	oordinate	End Co	Length		
ID	Onentation	East	North	East	North	(m)	
MASW01	Along-shore	493560.9	6122345.0	493847.0	6122508.4	352	
MASW02	Along-shore	493877.6	6122540.3	493908.2	6122853.9	320	
MASW03	Along-shore	493506.7	6122427.5	493847.3	6122831.7	544	
MASW04	Cross-shore	493552.9	6122340.9	493495.7	6122402.1	88	
MASW05	Cross-shore	493875.3	6122550.6	493790.3	6122688.6	160	

 Table 1 – Acquired MASW Transects (Coordinates in GDA94, MGA Zone 50).

СРТ	Соог	rdinate	Surface	Probing Depth (m)	
ID	East	North	Level (mAHD)		
CPT12	493886.4	6122768.8	1.60	18.02	
CPT13	493726.4	6122491.2	1.40	12.74	
CPT14	493534.3	6122444.7	4.44	14.66	
CPT15	493790.4	6122689.5	5.39	19.02	
CPT16	493592.0	6122400.6	1.35	12.14	

Table 2 – Acquired CPT Points (Coordinates in GDA94, MGA Zone 50).

3.2 MULTI-CHANNEL ANALYSIS OF SURFACE WAVES

MASW is a seismic geophysical method that utilises phase and frequency information to calculate Shear wave (S-wave) velocities in vertical layer models averaged over an array of linearly spaced geophones. These 1D models can be laterally stacked to provide 2D cross-sections of S-wave velocity in layers. Under most circumstances it is an indicator of material stiffness and as such the method can be used to provide quantitative results on the compaction of the subsurface material.

MASW data was acquired using a Geode (Geometrics) seismograph connected to a receiver array of 24 geophones set at 1m intervals for a total array length of 23m. The receiver array was mobilised on a land streamer whereby the geophones are mounted on base plates attached to webbing, and either towed behind a 4WD light vehicle or manually pulled by the field team. Seismic energy was generated using summed impacts from a PEG-40 (R.T. Clark) vehicle mounted accelerated weight drop or softened steel sledgehammer with source points made at a constant offset from receiver array. MASW acquisition parameters are provided in Table 3. Photographs of MASW data acquisition are shown in Figure 3.

Parameter	Value
Number of geophones	24
Geophone spacing	1 m
Array length	23 m
Geophone frequency	4.5 Hz
Record length	1 s
Sample interval	0.25 ms
Source	40kg AWD or 6.35kg sledgehammer
Source offset	4 m
Sounding interval	8m
Source stacks	3





Figure 3: MASW data acquisition using a seismic streamer.

The MASW data was observed to be of high quality with the seismic records having high signal to noise ratio. The generated overtone images plotting phase velocity against frequency showed a prominent dispersion curve of the surface wave component. The MASW data was processed using SurfSeis version 6++ (Kansas Geological Survey, 2017) with the following processing routine:

- 1. Import acquired seismic data files and apply geometry including geophone spacing, source offset and sounding interval.
- 2. Generate overtone images giving the percentage intensity of phase velocity versus frequency for each seismic record (Figure 4, left image).
- 3. Pick the maximum intensity across the useful range of frequencies for each overtone image resulting in a dispersion curve.
- 4. Run the dispersion curves through a 10-layer inversion algorithm to produce 1D soundings plotting seismic S-wave velocity with depth (Figure 4, right image).

The S-wave velocity soundings were compiled with reference to distance along the transects and gridded with Surfer version 25 (Golden Software, 2023). The resulting contoured cross-sections show the variation in the modelled S-wave velocity of the subsurface material in metres per second laterally along each of the transects and with elevation.

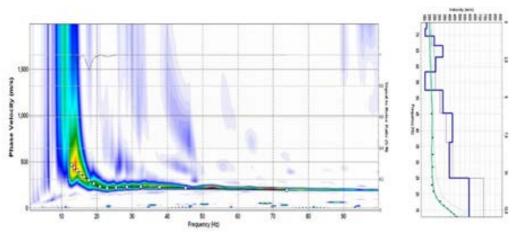


Figure 4: MASW overtone image with high signal to noise ratio and picked dispersion curve.

3.3 CONE PENETRATION TESTING

CPT is a geotechnical test method for evaluating the properties of soils and assessing subsurface stratigraphy including the sediment/rock interface at spot locations. The method involves pushing a calibrated cone and rod into the ground with a measured force with the resulting friction resistance plotted against depth to provide sediment compaction rates as well as the refusal depth indicating the depth to competent rock.

Testing was carried out using a M2 (Morooka) 11 tonne track mounted CPT Rig, specifications of which are provided in Appendix D. The test points were initially marked out at suitable locations within 2m of the intersecting geophysical transects. Dial Before You Dig enquiries and if necessary, utility locating was carried out prior to testing commencing.

CPT readings was made with sufficient ground bearing pressure to obtain a target depth of 10m or prior refusal. Where shallow refusal depths of less than 2m was encountered, when deemed necessary, an additional offset test was made to ascertain whether shallow refusal was due to a rock floater or other shallow obstruction. A photograph of CPT data acquisition is shown in Figure 5.



Figure 5: CPT data acquisition during a previous coastal investigation.

3.4 SPATIAL POSITIONING AND PHOTOGRAMMETRY

Spatial positioning of the acquired geophysical transects was achieved using Reach RS2 (Emlid) or S631 (Hemisphere) GNSS receivers with a coordinate recorded for each MASW sounding location and CPT point. Coordinates of the geophysical transects have been provided in GDA94, MGA zone 50 for horizontal component and Australian Height Datum (mAHD) for vertical component. An accuracy of +/- 0.2m is expected for both vertical and horizontal components.

To achieve precise reduced levels referenced to AHD, a local base correction with an Atlas Satellite-Based Differential Correction Service (L-Band) was used. This correction was utilised as no Standard Survey Markers were located within the vicinity of the survey area to use as a base correction reference point.



A reduced level of 0.0mAHD is considered to be the Mean Sea Level (MSL) for the purpose of this investigation. This relationship for Mean Sea Level was established by the Geoscience Australia Survey in 1971 (http://www.ga.gov.au/scientific-topics/positioning-navigation/geodesy/datums-projections/australian-height-datum-ahd).

Aerial photogrammetry was carried out to obtain an up-to-date high-resolution aerial image and a surface level model of the survey area. Data was acquired with a Matrice 300 (DJI) multi-rotor drone, equipped with a L1 (Zenmuse) camera for the capture of multiple overlapping images.

The acquired photogrammetry images were processed using Metashape Professional (Agisoft) for the generation of a point cloud, surface level model and orthomosaic image of the survey area. Note: for this investigation, vegetation has not been removed during the processing stage and as such the height of existing vegetation needs to be considered when assessing surface levels.

4 RESULTS AND INTERPRETATION

4.1 PRESENTATION OF RESULTS

The results of the geotechnical investigation at Peaceful Bay, Shire of Denmark are presented in Appendices B and C of this report as follows:

Appendix B – Geophysical and Interpreted Sections

- **3073B-02.** Transects 1 seismic S-wave velocity model and interpreted geological section.
- **3073B-03.** Transect 2 seismic S-wave velocity model and interpreted geological section.
- **3073B-04 and -05.** Transect 3 seismic S-wave velocity model and interpreted geological section.
- **3073C-06.** Transects 4 and 5 seismic S-wave velocity model and interpreted geological section.

Appendix C – Modelled Level to Top of Rock and Sand Thickness

- **3073B-07 and 3073B-08.** Contoured surface level model derived from aerial photogrammetry.
- **3073B-09 and 3073B-10.** Contoured level to modelled top of rock.
- **3073B-11.** Class post map level to modelled top of rock.
- **3073C-12 and 3073B-13.** Contoured modelled sand thickness over rock.
- **3073B-14.** Class post map modelled sand thickness over rock.

4.2 SEISIMC SHEAR WAVE VELOCITY SECTIONS

The seismic S-wave velocity (Vs) sections modelled from the MASW data acquired along the alongshore and cross-shore transects are presented at the top of each drawing in Appendix B. These sections show variations in the modelled Vs as per the colour scale with velocity ranging from 150m/s to 1000m/s representing a wide range of material types and conditions.

Seismic S-wave velocity is governed by the elastic properties of the medium that the wave propagates through as shown in the equation below. In particular, it is primarily a function of soil density, void ratio and effective stress. As such calculated values can provide a useful guide to the subsurface material condition with increasing velocity an indication of increasing material stiffness.

Seismic S-wave velocity

$$V_s = \sqrt{\frac{G}{\rho}}$$

where; G = Shear modulus, ρ = In-situ material density

4.3 INTERPRETED GEOLOGICAL SECTIONS

Below the seismic S-wave velocity sections are the interpreted geological sections based on detectable seismic velocity contrasts correlated with the CPT. Four classes have been defined representing different subsurface material conditions as follows:

- 1. Very low seismic S-wave velocity (Vs <250m/s). Representing the lowest seismic velocities modelled during the investigation, this class is interpreted as sediment consisting of SAND of low compaction from either the beach or dune formation.
- 2. Low seismic S-wave velocity (Vs 250-350m/s). This class is interpreted as sediment consisting of SAND of moderate compaction due to increased depth of cover particularly in the beach and dune formation, or due to development adjacent to the settlement.
- 3. Moderate seismic S-wave velocity (Vs 350-475m/s). This class is interpreted as low strength rock consisting of variably weathered CALCARENITE. Where continuous and at base of the sections it likely represents a transitional zone to stronger, more competent underlying CALCARENITE. Where present as isolated anomalies within the interpreted SAND it is likely to represent partially lithified SAND and/or CALCARENITE lenses.
- 4. **Moderate to high seismic wave velocity** (Vs >475m/s). This class is interpreted as moderate strength rock consisting of slightly weathered to fresh CALCARENITE. It is typically observed at the base of the sections as competent rock underlying the variably weathered CALCARENITE.

4.4 CALIBRATION WITH GEOTECHNICAL TESTING AND ROCK MAPPING

The results of the CPTs are presented in Appendix D showing the plots of cone tip resistance in megapascals against depth in metres. The CPT plots are also shown in Appendix B and overlayed onto the interpreted geological sections with the following observations being made:

- **CPT-12 on Transect 2** refusal of 45MPa plus lateral rod support was at a depth of 18m Below Ground Level (BGL). This was beyond the imaging depth of the MASW testing which sampled interpreted sand from surface to a depth of 12mBGL.
- CPT-13 on Transect 1 refusal due to rod friction was at 12.74mBGL, approximately 4.5m into interpreted low strength rock, and at the top of interpreted moderate strength rock. An increase in CPT tip resistance at 8.0mBGL corresponds to the top of interpreted low strength rock suggesting highly variable weathering.
- **CPT-14 on Transect 3** refusal of 40MPa plus lateral rod support and rod friction was at a depth of 14.66mBGL, approximately 3.0m into interpreted low strength rock, and at the top of interpreted moderate strength rock.
- **CPT15 on Transects 3 and 5** refusal of 40MPa plus lateral rod support and rod friction was at 19mBGL. This was beyond the imaging depth of the MASW testing which sampled interpreted sand from surface to a depth of 17mBGL.
- CPT-16 on Transect 1 refusal due to rod friction was at 12.14mBGL, approximately 5.5m into interpreted low strength rock, and at the top of interpreted moderate strength rock. An increase in CPT tip resistance at 6.5mBGL corresponds to the top of interpreted low strength rock suggesting highly variable weathering.

The differences in the modelled level to low strength and moderate strength rock as interpreted from the MASW transects and from the CPT data can be attributed to the fact that the geophysical methods used are broad scale whilst the CPT is a point method. Geophysical methods sample a volume of subsurface material with the calculated depths at any particular point representing an average value over this volume. The CPT method samples the subsurface directly below the probe and is influenced by local variations in the subsurface such as rock floaters, highly weathered zones or lenses of partially lithified sediment. The differences in the type of subsurface sampling of the methods will not adversely affect the results as the CPT results have been used to constrain the geophysics interpretation and as such the results represent the best modelled fit between the datasets.

Surface outcropping rock was observed on the beach foreshore between the end of Transect 1 and start of Transect 2, and an offshore rock outcrop adjacent to this. The outcropping rock corresponds to sections in these transects with thin sediment cover over interpreted rock.

4.5 MODELLED LEVEL TO TOP OF ROCK AND SAND THICKNESS

Subsurface models for the level to top of rock substrate and overlying sand thickness within the region between the coastal foreshore and settlement are presented in Appendix C. These has been generated by digitising the interface between the interpreted sediment and underling rock profile from the interpreted geological sections along the acquired along-shore and cross-shore transects and calibrated with the CPT plots. The modelled sand thickness was then generated by subtracting this from the surface elevation. The following subsurface models have been provided:

- **Contoured Surface Level Model** (drawing 3073B-07 and 3073B-08) generated from the aerial photogrammetry, this presents the level to ground surface ranging from 0mAHD to 18mAHD. Note: vegetation height has not been removed from these models.
- **Contoured Level to Top of Rock Substrate** (drawing 3073B-09 and 3073B-10) this presents the level to the top of rock substrate ranging from -14mAHD to 2mAHD.
- Classed Post Map Level to Top of Rock Substrate (drawing 3073B-11) this presents the level to the top of rock substrate along the acquired transects at 2m level increments from -10mAHD to 2mAHD.
- **Contoured Sand Thickness Over Rock** (drawing 3073B-12 and 3073B-13) this presents the thickness of sand overlying the rock substrate ranging from 2mBGL to 14mBGL.
- Classed Post Map Sand Thickness Over Rock (drawing 3073B-14) this presents the thickness of sand overlying the rock substrate along the acquired transects at 2.5m depth increments from 2.5mBGL to 15mBGL.

The following limitations should be considered when assessing the subsurface models for the level to top of rock substrate and overlying sand thickness:

The expected accuracy of the top of rock substrate modelled from this investigation is +/-0.5mAHD. Similarly, an accuracy of +/-0.5m is expected for the modelled sand thickness over rock. The quoted accuracies have been based on consideration to the accuracy of the GNSS receivers using during the site work, 1D inversion of the MASW dataset using a 10-layer model, and expected undulations in the sand/rock interface. Note the quoted accuracies are only valid along the geophysical transects. Values given between transects have been interpolated in the contour maps and as such the accuracy in this case is indeterminable.

The generated contours will give the general trend of the top of rock profile however will not image local variations when the extent of these is less than transect spacing. Spatially small features such as karst sinkholes or pinnacle features may not be imaged. The significance of this limitation is considered minor for this investigation since although local geological features such as pinnacles may not be represented in the data, the generated surface of the top of rock will show the broad trends in the geology over the site which is suitable for a coastal erosion assessment.



Transition zones including between fresh and weathered rock and between sediment and lithified/partially lithified sediment may be gradational and as such the interface between these layers are not well defined.

The calculated levels to the top of rock will only be valid along the geophysical transects. Values shown on the contour maps not on the transects have been interpolated using the krigging algorithm and as such the accuracy of these levels is indeterminable. The contour surface will give the general trend of the interface however may not image local variations, it is recommended that the interpreted geological sections presented in Appendix B be used to obtain more accurate top of rock levels and overlying sand thickness.

5 PROJECT SUMMARY

A geotechnical investigation has been carried out as part of a coastal erosion assessment at Peaceful Bay in the Shire of Denmark, Western Australia. During the investigation ground geophysical and intrusive geotechnical testing was conducted within a 700m corridor of coastal beach and dune formation adjacent to the Peaceful Bay settlement which has been identified as an at risk site as part of Coastal Hotspot #50.

The investigation scope consisted of acquiring multi-channel analysis of surface waves data as a series of specified transects either along-shore (parallel to the coast) or cross-shore (perpendicular to the coast) and cone penetration testing at spot locations along these transects. This was supplemented with geological mapping of surface rock outcrops and topographic survey using high resolution photogrammetry for the generation of a surface level model and orthomosaic image.

The acquired MASW dataset was processed for the generation of seismic velocity sections along the transects showing variations in the seismic shear wave velocity of the subsurface material to a target depth of 10-15m below ground level. The seismic velocity sections were calibrated with the CPT plots and demarcated into velocity ranges representing different material types and conditions for the generation of interpreted geological sections consisting of loose to compacted sediment and variably weathered to fresh rock.

The interpreted geological sections have been compiled to develop subsurface models of the level to rock substrate (relative to AHD) and overlying sand thickness within the region between the foreshore and the future development. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the future development.

The methods used during the investigation are geophysical and as such the results are based on indirect measurements and the processing and interpretation of seismic wave signals calibrated with limited intrusive geotechnical testing. The findings in this report represent the professional opinions of the authors, based on experience gained during previous similar investigations.



We trust that this report and the attached drawings provide you with the information required. If you require clarification on any points arising from this geophysical investigation, please do not hesitate to contact the undersigned on 08 9354 6300.

For and on behalf of GBG GEOTECHNICS (AUSTRALIA)

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ANDREW SPYROU Operations Manager, Western Australia / Senior Geophysicist



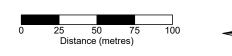
APPENDIX A – INVESTIGATION SITE MAP



INVESTIGATION SITE MAP



NOTES Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



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DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

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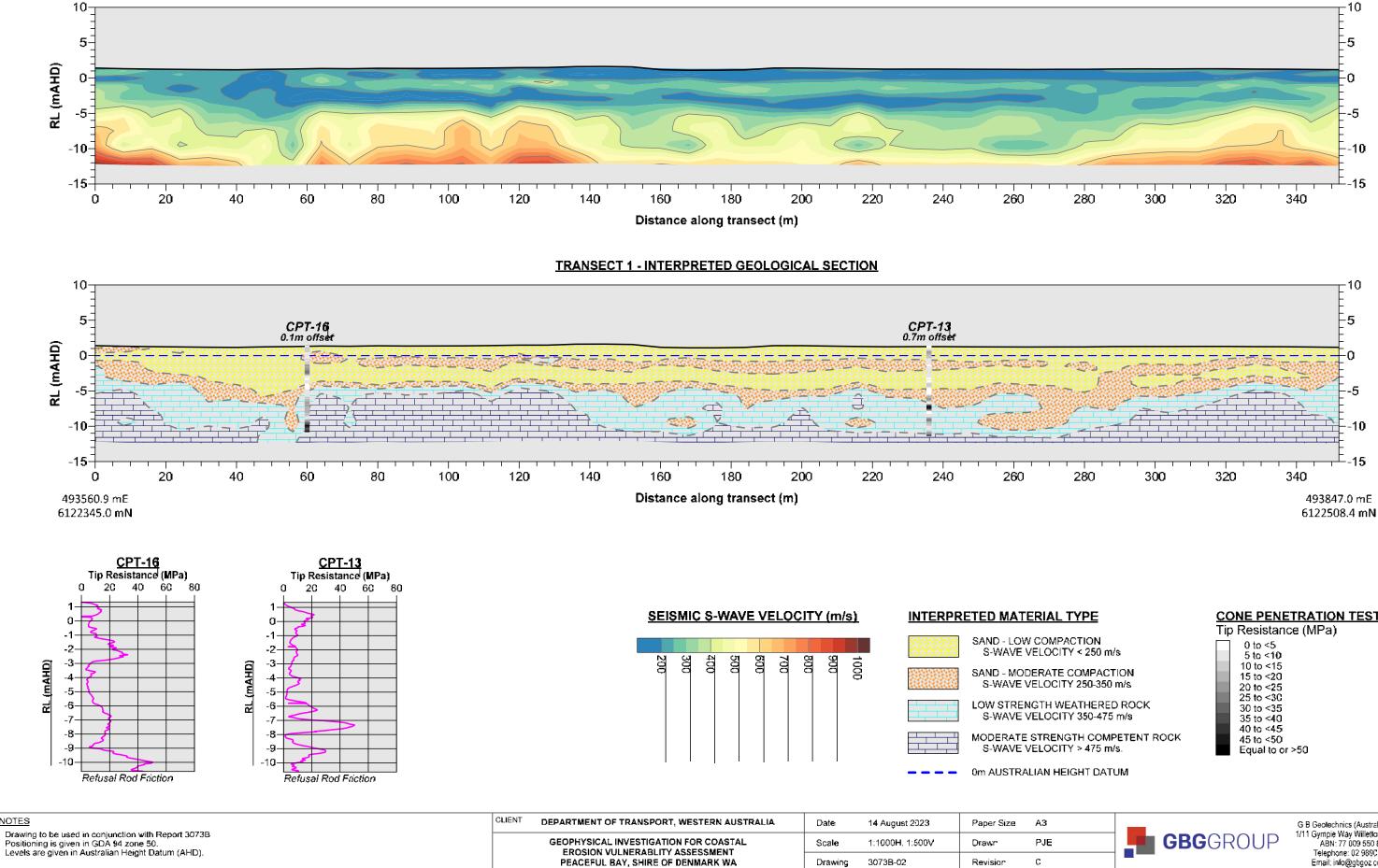
APPENDIX B – GEOPHYSICAL AND INTERPRETED SECTIONS



NOTES

GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WESTERN AUSTRALIA





CONE PENETRATION TEST

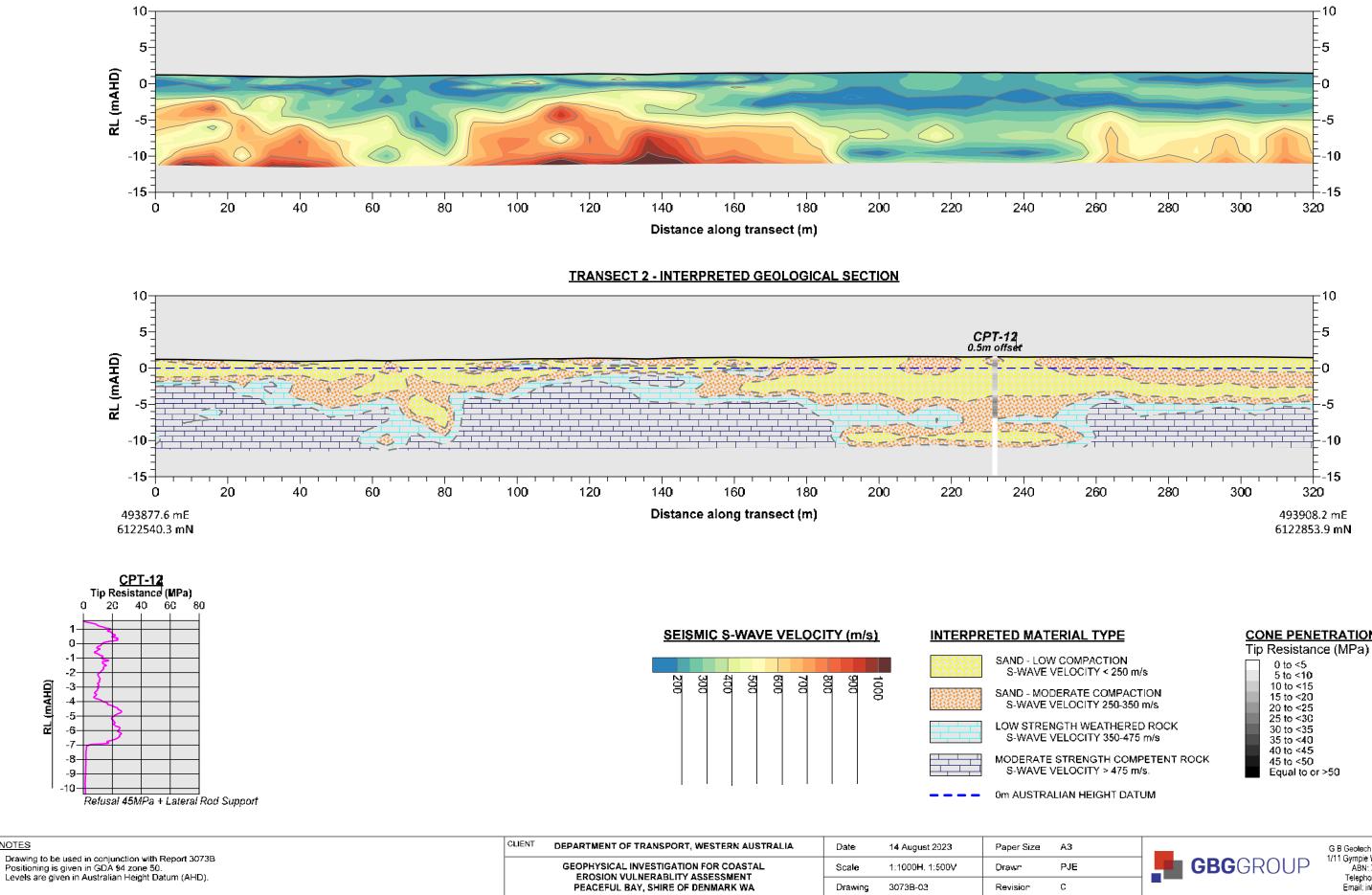


RL (mAHD)

NOTES

GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WESTERN AUSTRALIA

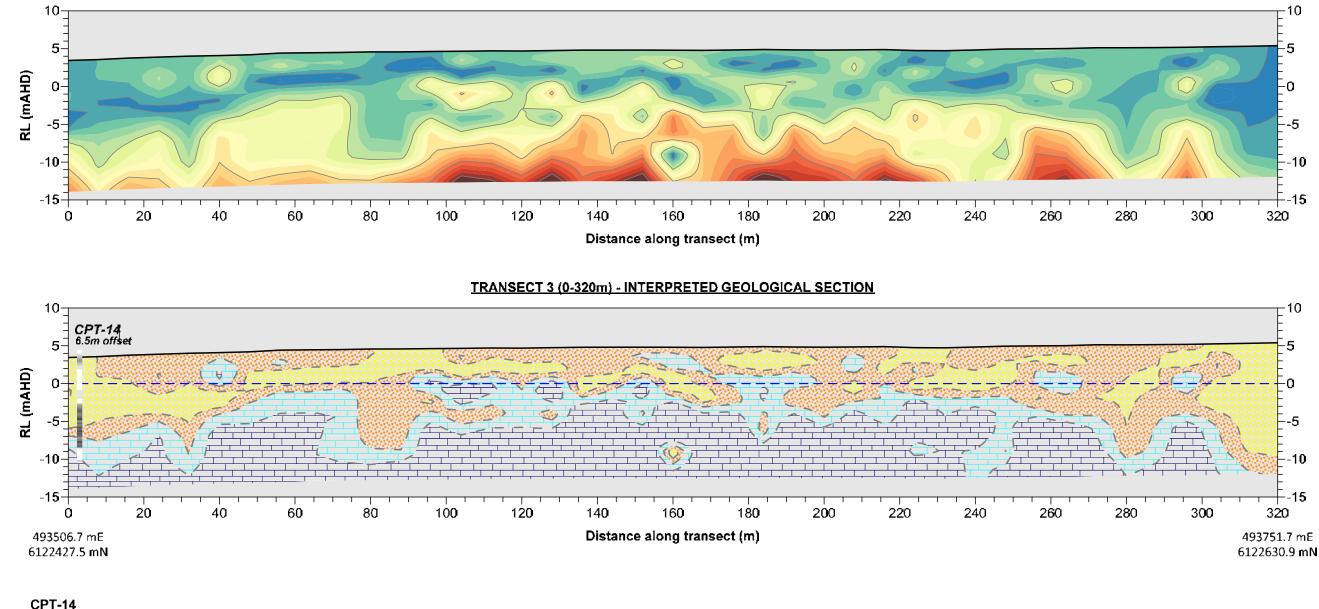
TRANSECT 2 - SEISMIC SHEAR WAVE VELOCITY MODEL

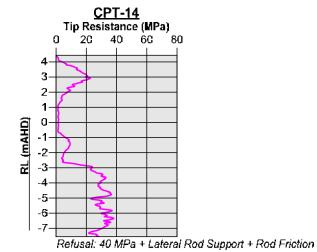


CONE PENETRATION TEST



TRANSECT 3 (0-320m) - SEISMIC SHEAR WAVE VELOCITY MODEL





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	6.8		679			~	(7)	,		SAND - LOW COMPACTION S-WAVE VELOCITY < 250
200	300	400	500	600	700	800	006	1000		SAND - MODERATE COMPA S-WAVE VELOCITY 250-3
										LOW STRENGTH WEATHER S-WAVE VELOCITY 350-4
										MODERATE STRENGTH CO S-WAVE VELOCITY > 475
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NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073B Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT	Scale	1:1000 H . 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		PEACEFUL BAY, SHIRE OF DENMARK WA	Drawing	3073B-04	Revision	С

Έ DN -

50 m/s

PACTION 1-350 m/s

ERED ROCK)-475 m/s

COMPETENT ROCK 75 m/s.

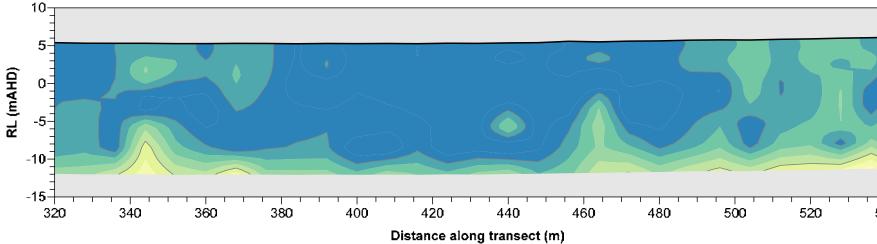
GBGGROUP

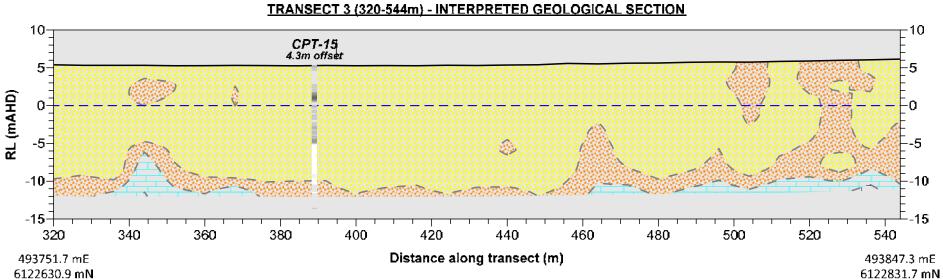
DATUM

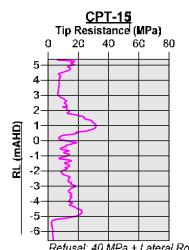
CONE PENETRATION TEST

Tip Resistance (MPa) 0 to <5 5 to <10 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50

TRANSECT 3 (320-544m) - SEISMIC SHEAR WAVE VELOCITY MODEL



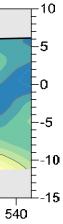




Refusal: 40 MPa + Lateral Rod Support + Rod Friction

<u>SEIS</u>	MIC	: S-V	VAV	<u>E V</u>	ELO	CITY	<u>′ (m</u>	<u>/s)</u>	INTERPR	ETED MATERIA
N	لى)	4	cn	G	7	a	á			SAND - LOW COM S-WAVE VELOC
200	300	400	500	600	00	800	006	1000		SAND - MODERAT S-WAVE VELOO
										LOW STRENGTH V S-WAVE VELOC
										MODERATE STRE S-WAVE VELOC
I	I	Į	I	I	I	I	I			0m AUSTRALIAN F

NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073B Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT	Scale	1:1000 H , 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		PEACEFUL BAY, SHIRE OF DENMARK WA	Drawing	3073B-05	Revision	С



AL TYPE

MPACTION CITY < 250 m/s

TE COMPACTION CITY 250-350 m/s

WEATHERED ROCK CITY 350-475 m/s

ENGTH COMPETENT ROCK CITY > 475 m/s.

I HEIGHT DATUM

CONE PENETRATION TEST

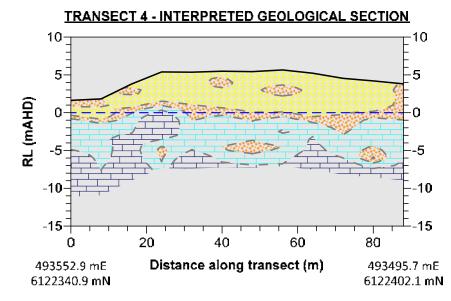
Tip Resistance (MPa)

0 to <5 5 to <10 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50

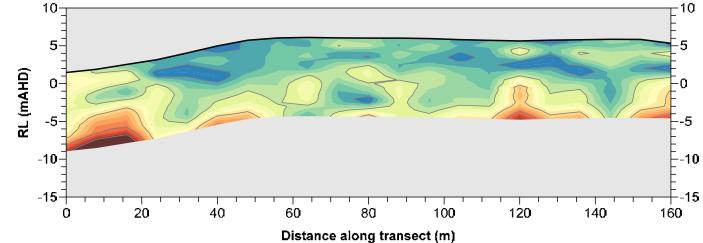
GBGGROUP



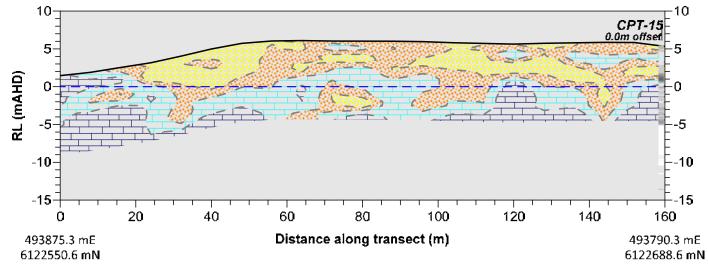
TRANSECT 4 - SEISMIC SHEAR WAVE VELOCITY MODEL 10--10 5--5 RL (mAHD) 0 n -5 -5 -10· -10 -15 -15 0 20 40 60 80 Distance along transect (m)

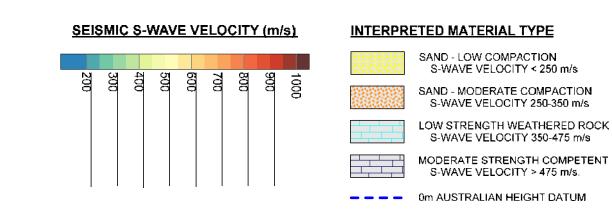




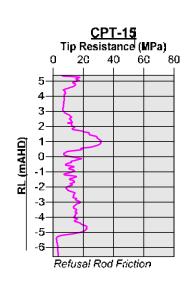


TRANSECT 5 - INTERPRETED GEOLOGICAL SECTION





	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	14 August 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073B Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT	Scale	1:1000 H . 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		PEACEFUL BAY, SHIRE OF DENMARK WA	Drawing	3073B-06	Revision	С



CONE PENETRATION TEST Tip Resistance (MPa) 0 to <5 5 to <10 10 to <15 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 MODERATE STRENGTH COMPETENT ROCK 45 to <50 Equal to or >50

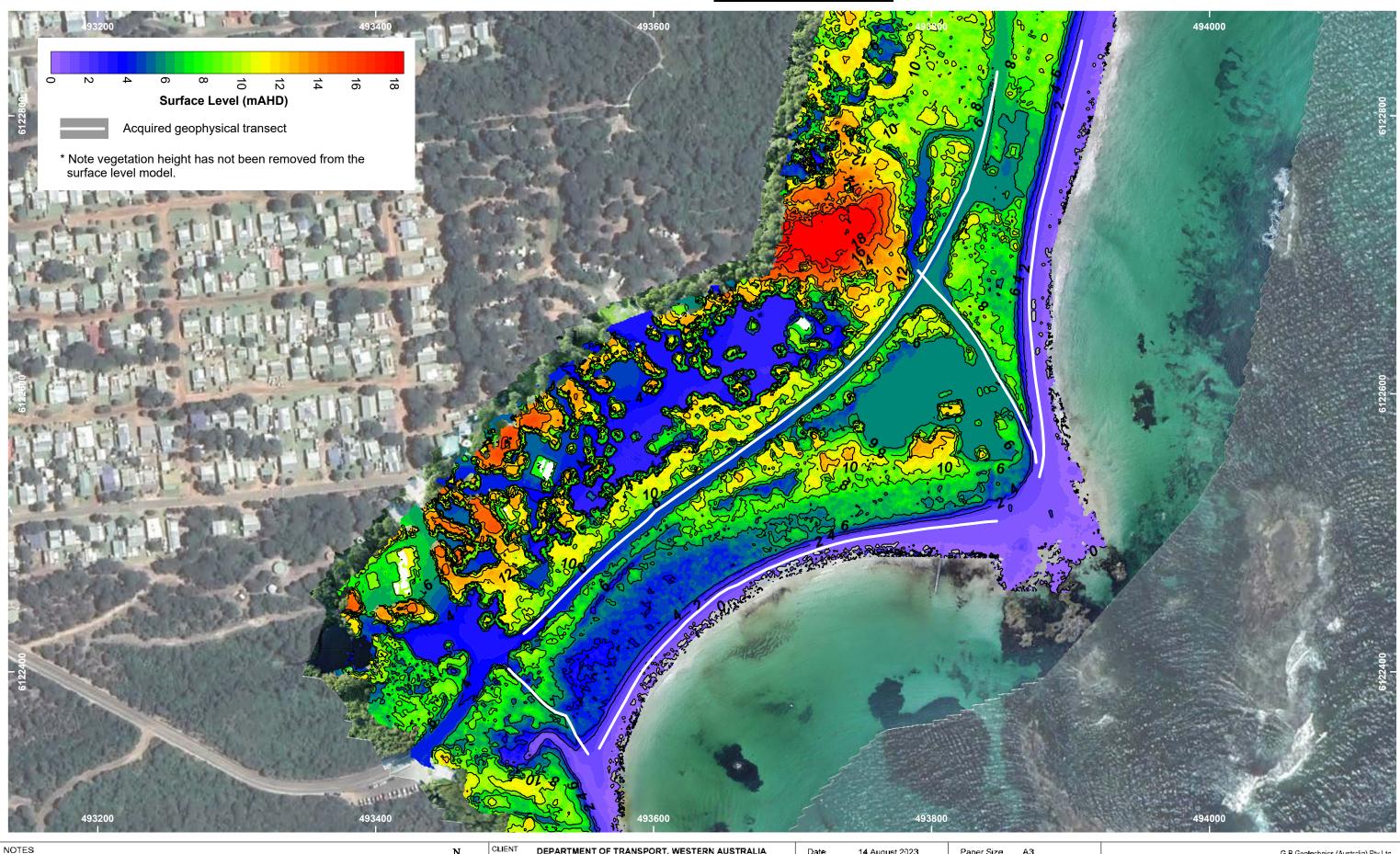
GBGGROUP



APPENDIX C – MODELLED TOP OF ROCK AND SAND THICKNESS



SURFACE LEVEL MODEL



NOTES

Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



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DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

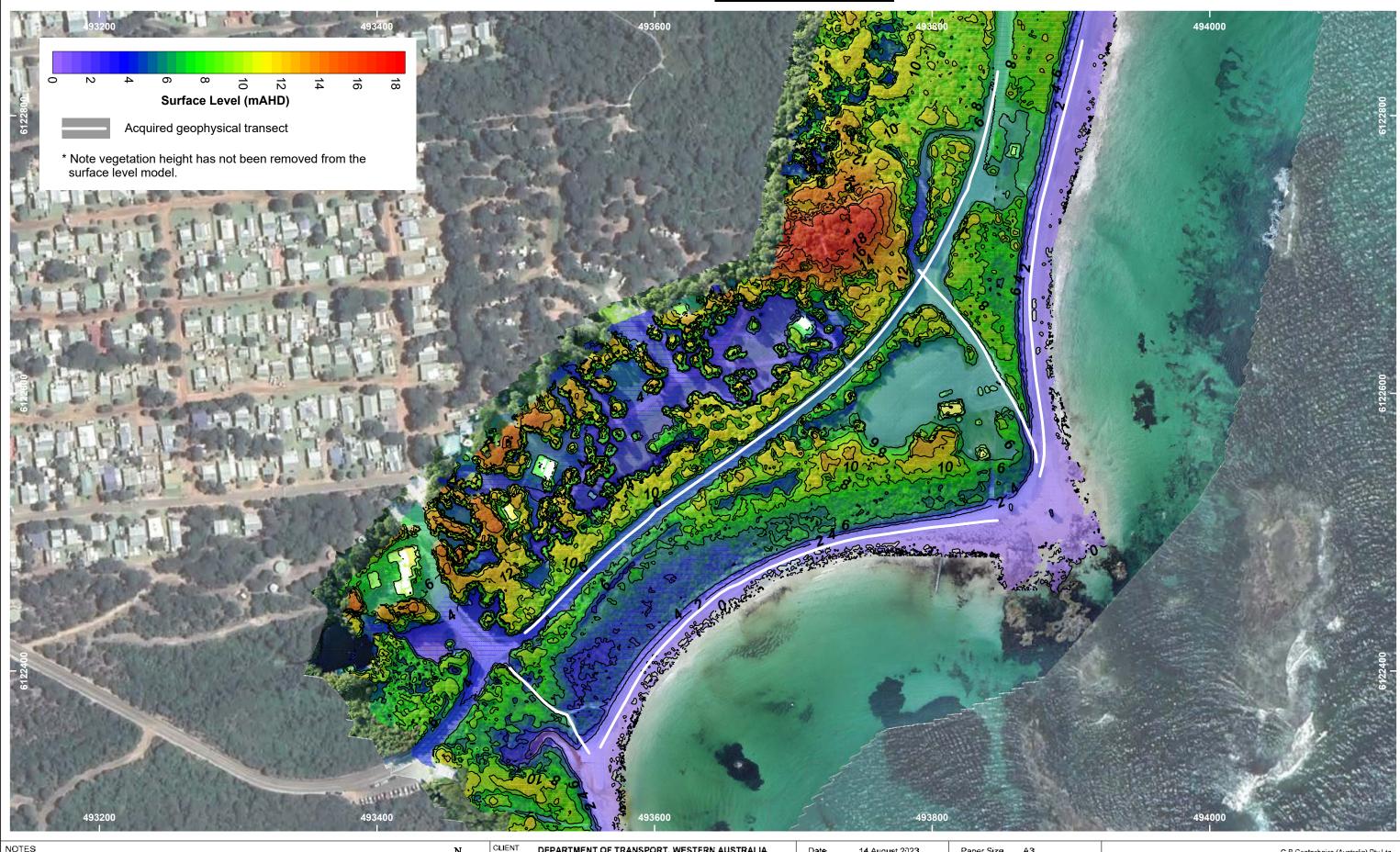
GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

Date	14 August 2023	Paper Size	A3
Scale	1:2500	Drawn	PJE
Drawing	3073B-07	Revision	с



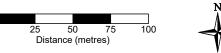


SURFACE LEVEL MODEL



NOTES

Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



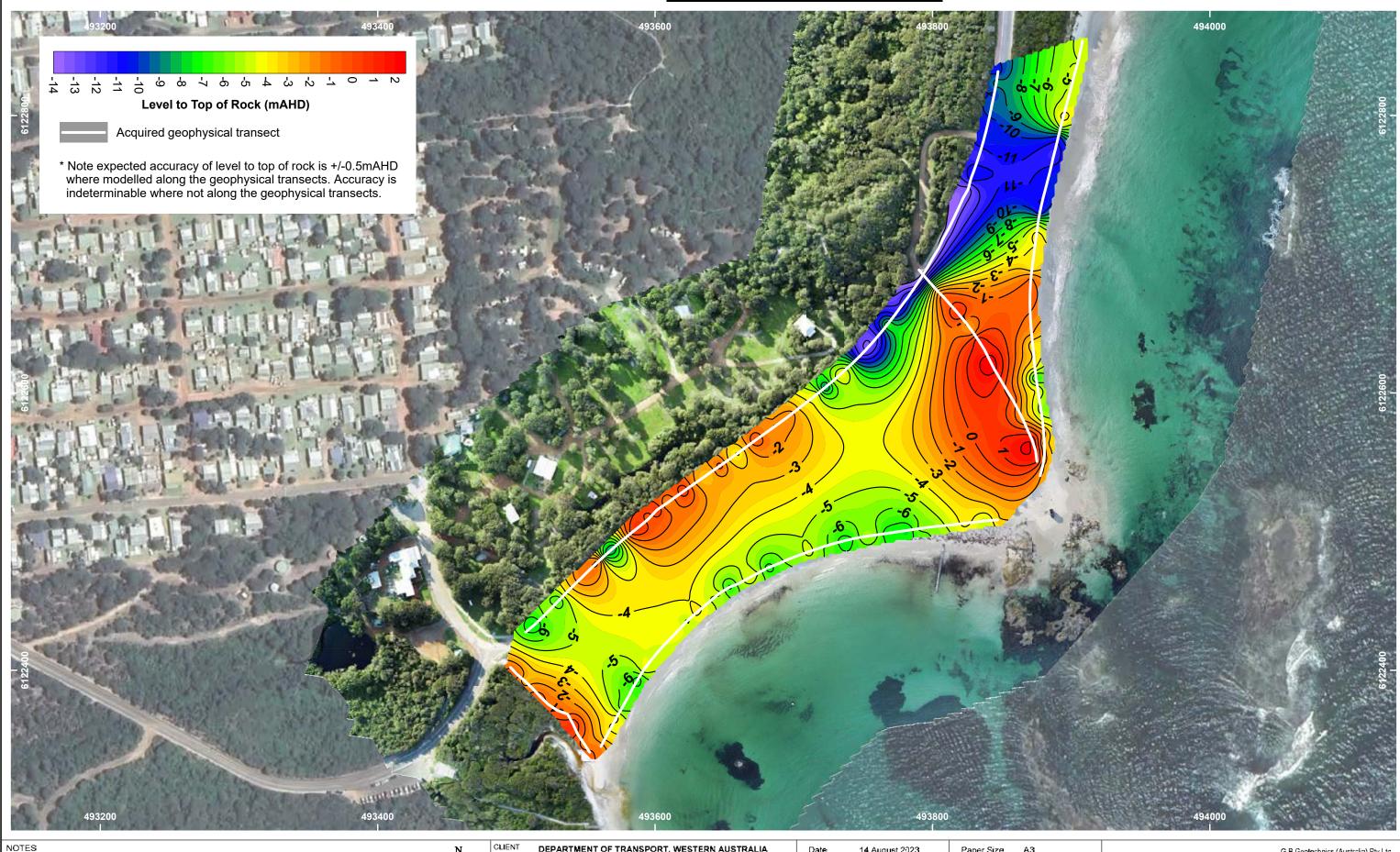
DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

Date 14 August 2023 Paper Size A3 GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA Scale 1:2500 Drawn PJE Drawing Revision С 3073B-08



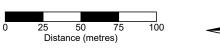


CONTOURED LEVEL TO TOP OF ROCK



NOTES

Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

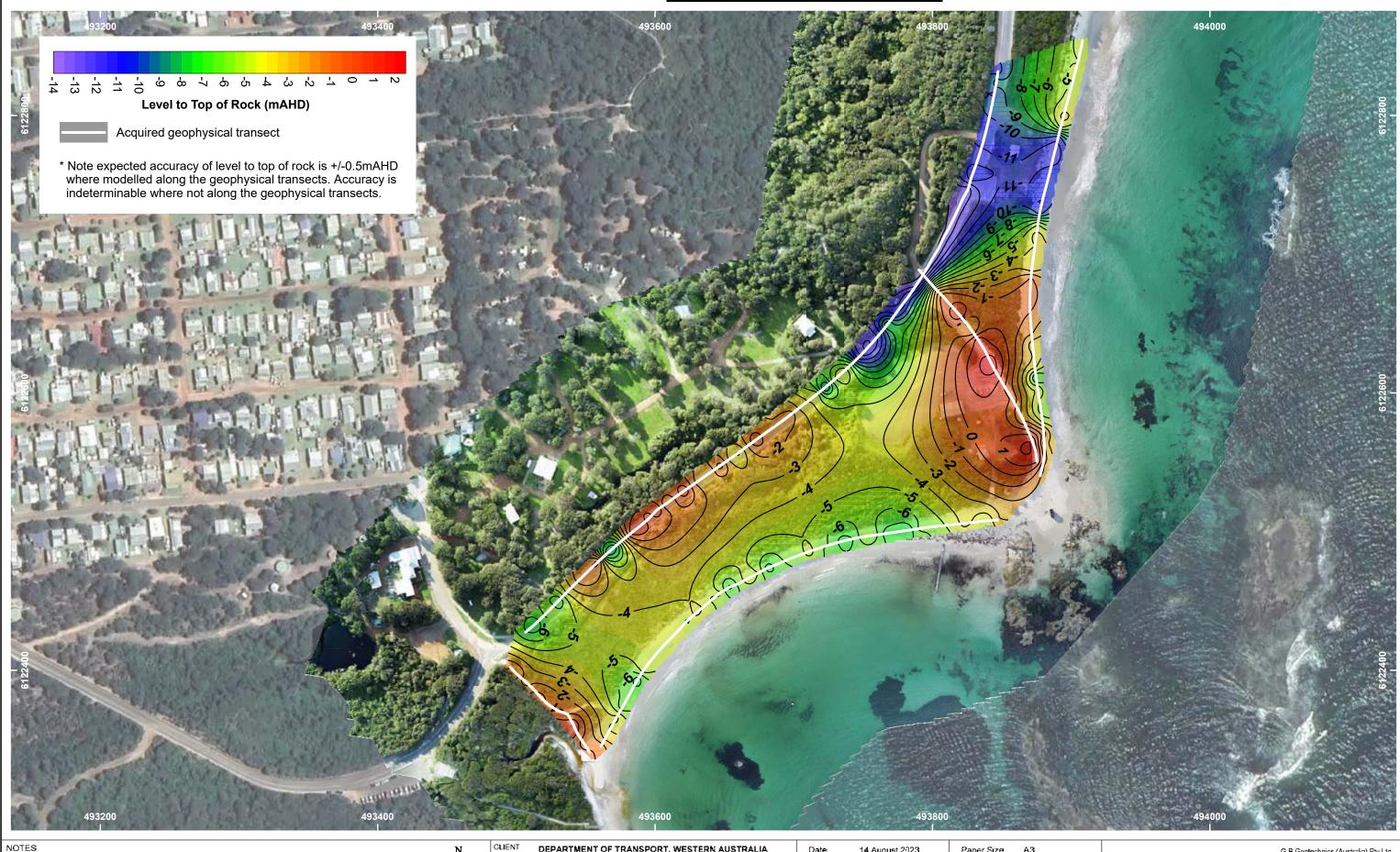
GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

Date	14 August 2023	Paper Size	A3	
Scale	1:2500	Drawn	PJE	
Drawing	3073B-09	Revision	с	





CONTOURED LEVEL TO TOP OF ROCK



NOTES

Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

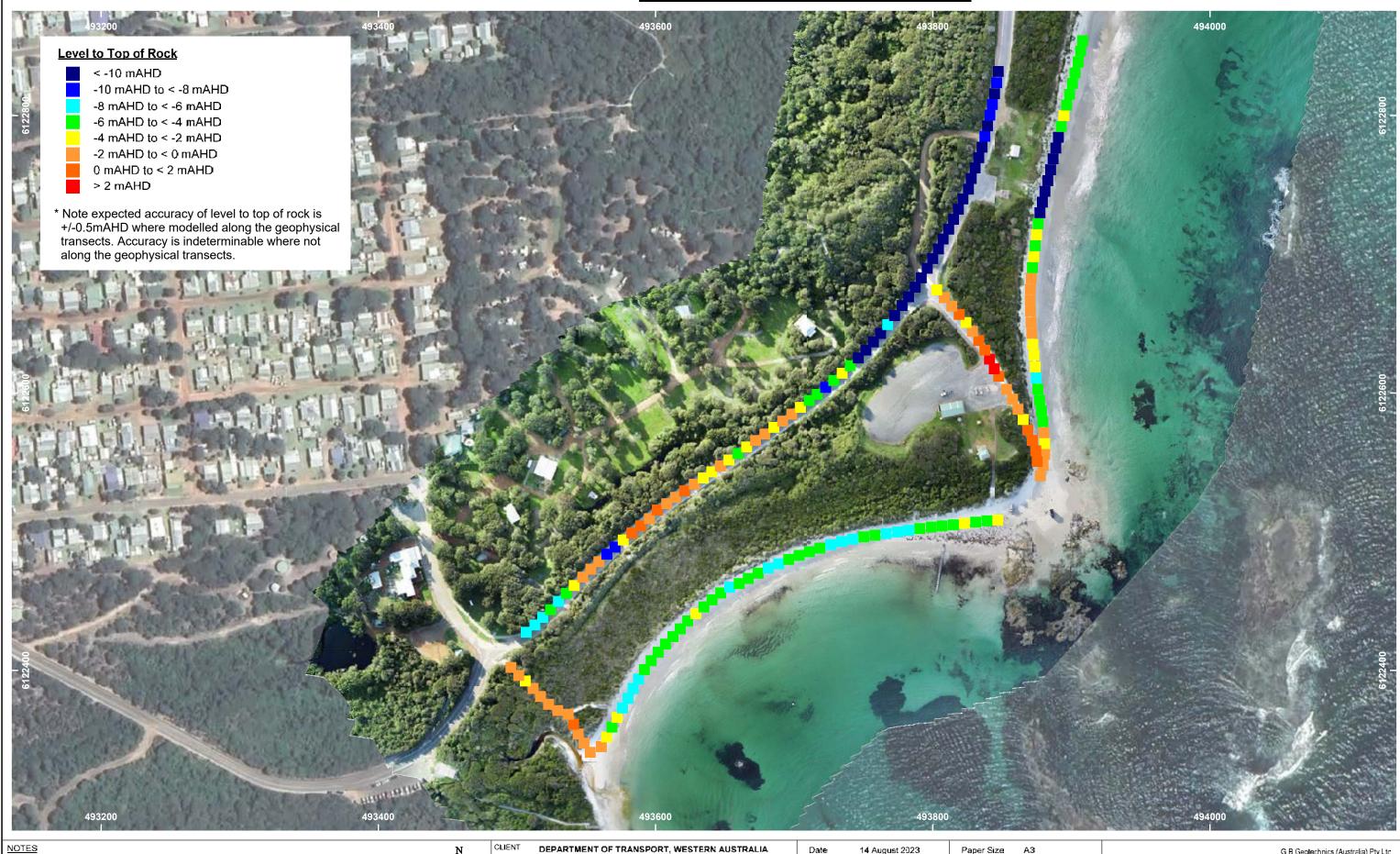
GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

Date	14 August 2023	Paper Size	A3
Scale	1:2500	Drawn	PJE
Drawing	3073B-1C	Revision	С

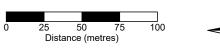




CLASSED POST MAP LEVEL TO TOP OF ROCK



Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

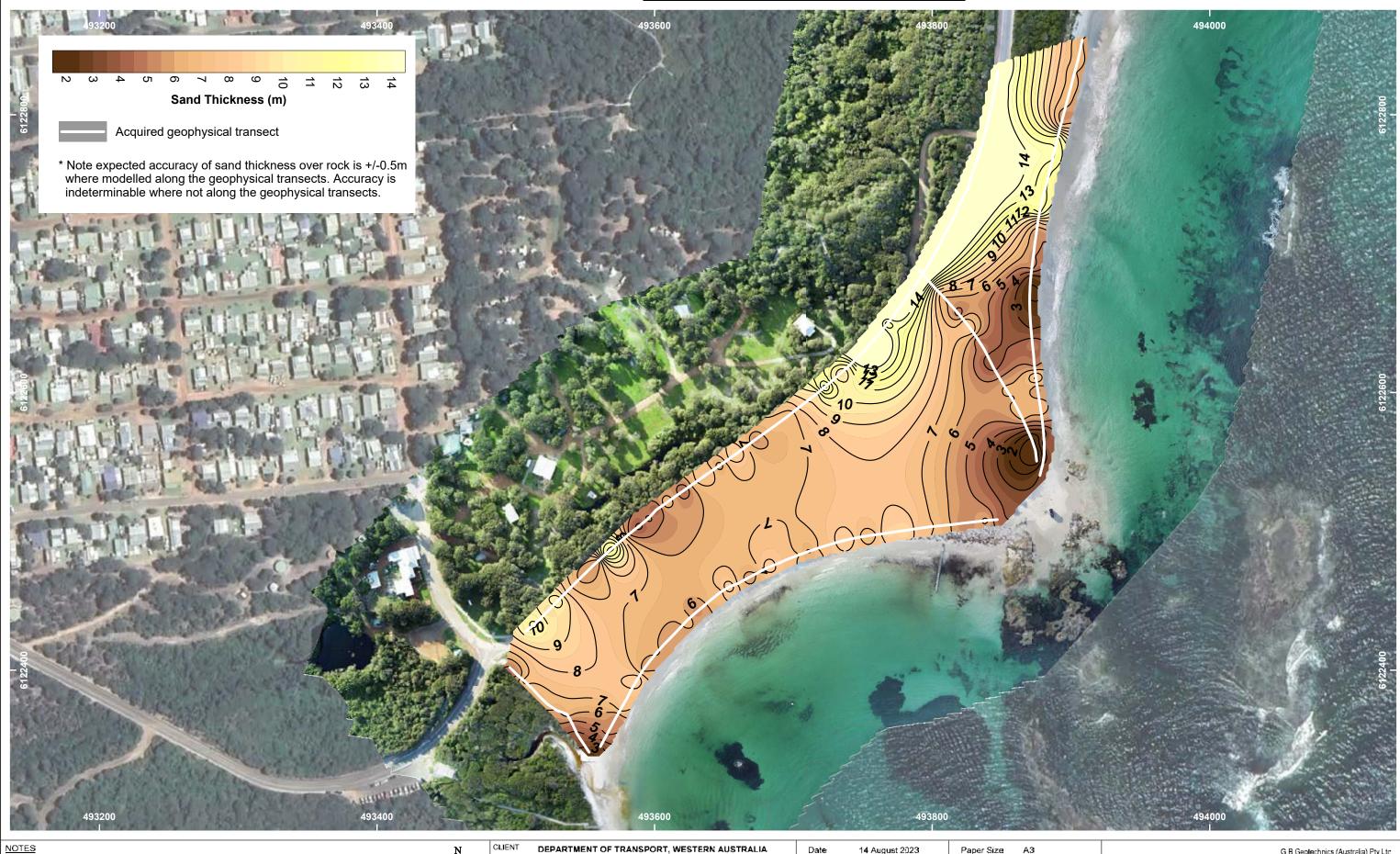
GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

Date	14 August 2023	Paper Size	A3
Scale	1:2500	Drawn	PJE
Drawing	3073B-11	Revision	С

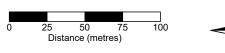




CONTOURED SAND THICKNESS OVER ROCK



Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

Date	14 August 2023	Paper Size	A3
Scale	1:2500	Drawn	PJE
Drawing	3073B-12	Revision	С

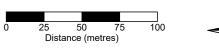




CONTOURED SAND THICKNESS OVER ROCK



Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

Date	14 August 2023	Paper Size	A3
Scale	1:2500	Drawn	PJE
Drawing	3073B-13	Revision	с



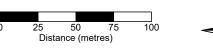


CLASSED POST MAP SAND THICKNESS OVER ROCK



NOTES

Drawing to be used in conjunction with Report 3073B Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBC photogrammetry.



DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

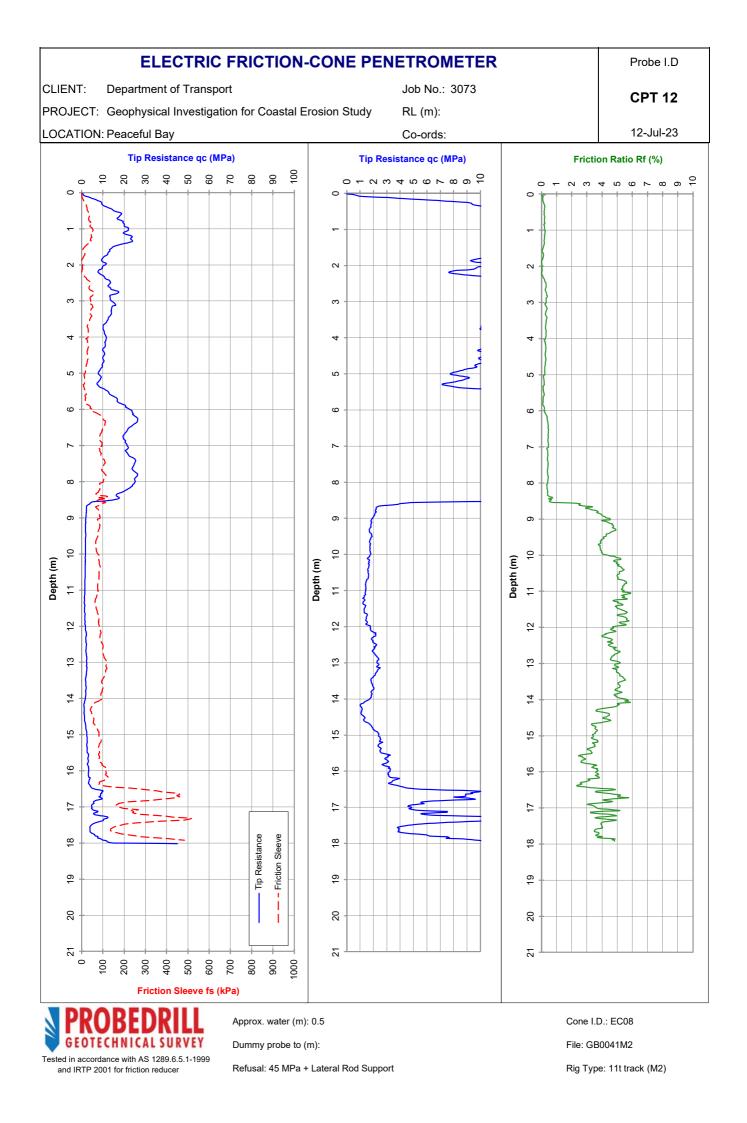
GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT PEACEFUL BAY, SHIRE OF DENMARK WA

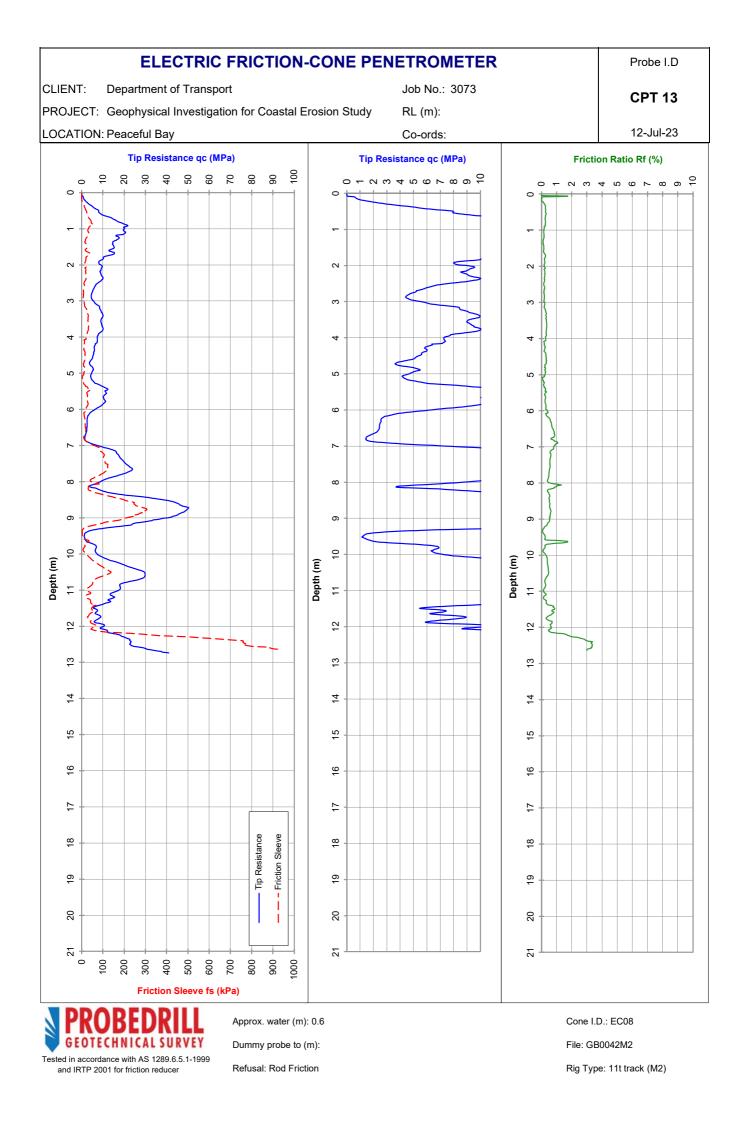
Date	14 August 2023	Paper Size	A3	
Scale	1:2500	Drawn	PJE	
Drawing	3073B-1 4	Revision	с	

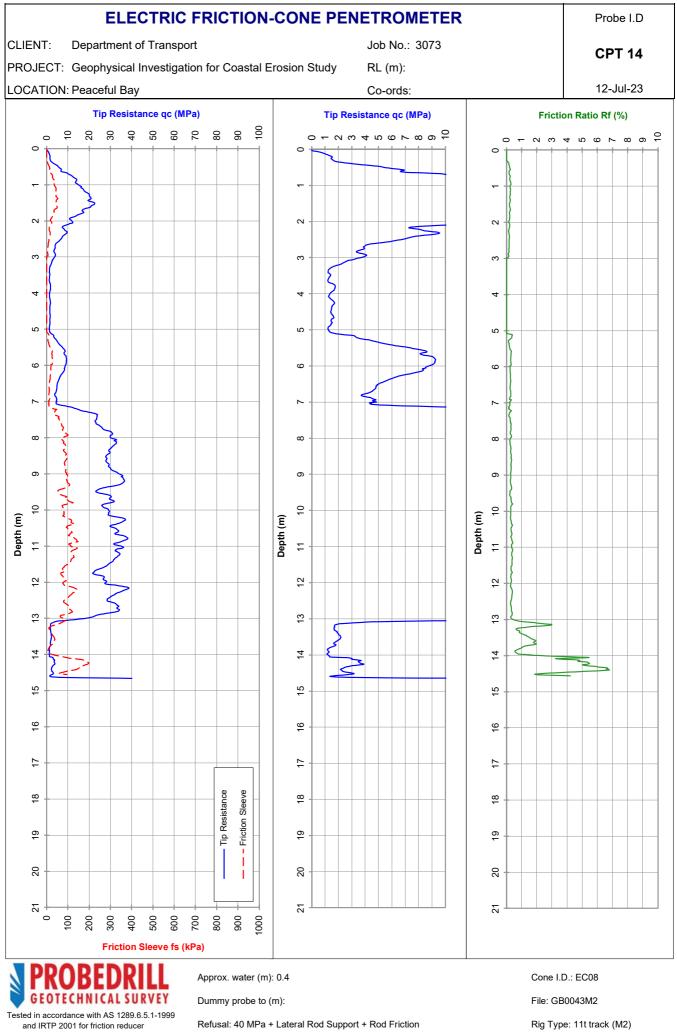




APPENDIX D – CONE PENETRATION TEST PLOTS

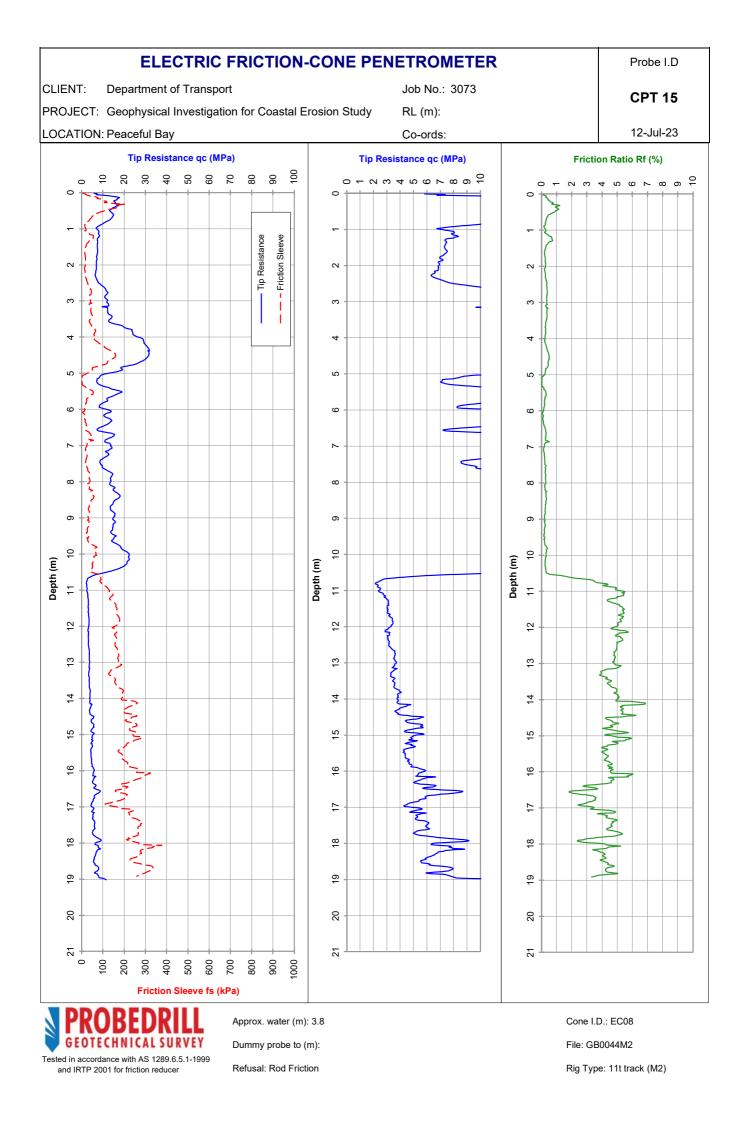


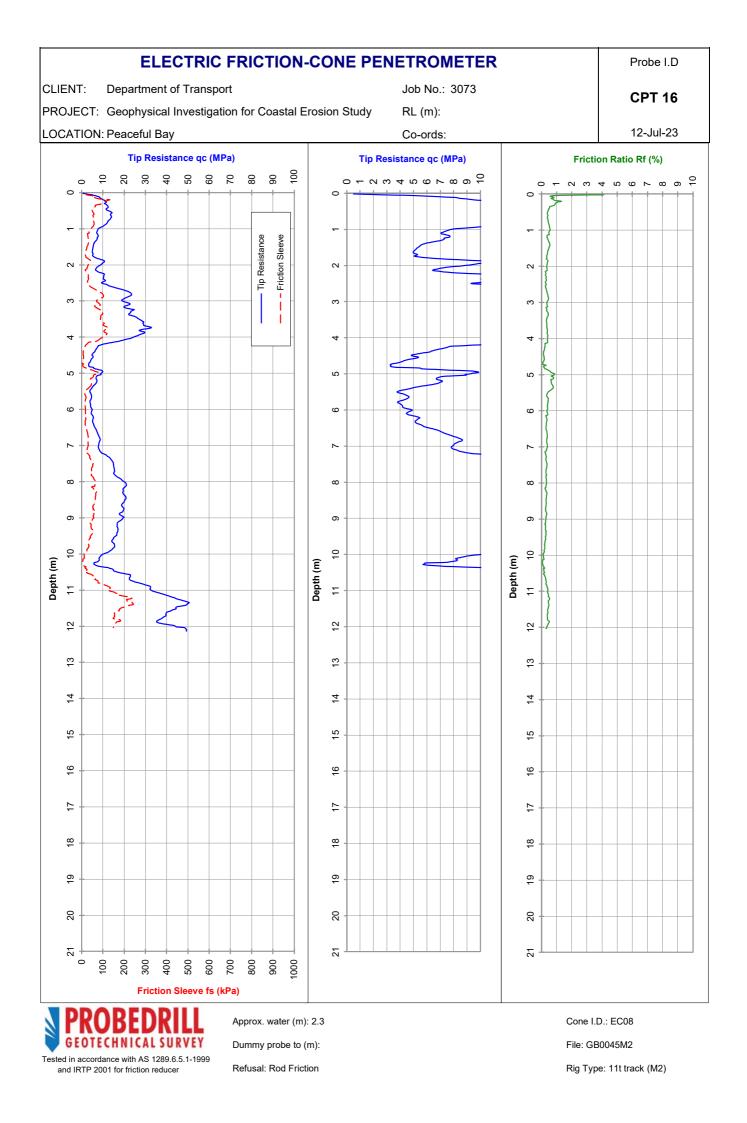




Refusal: 40 MPa + Lateral Rod Support + Rod Friction

Rig Type: 11t track (M2)







CALIBRATION CERTIFICATE

CONE ID:

Cone Type: Calibration Date (qc/fs): Calibration Date (u): Preliminary Inspection: Calibrated By: Calibration Procedure: Force Application: Reference Equipment:

EC08

Compression 2 June 2023 21 March 2023 Pass Sean Wilkins ISO 22476-1:2012, IRTP 2001 Compression PT - S type 100kN Serial # 5126009 (Calibrated 10/03/23 - NATA approved Cert. No. 230664) Bongshin - S type 50kN Serial #W05345 (Calibrated 10/03/23 - NATA approved Cert. No. 230663) Dieitron Panel Meter Serial #: 060213/01 (Calibrated 09/03/23 - NATA endorsed Renort No. 230663)

Digitron Panel Meter Serial #: 060213/01 (Calibrated 09/03/23 - NATA endorsed Report No. 230658, 230659, 230660) Note: In accordance with AS1289 F5.1 the force calibration derived by NATA Calibration Certificates are converted to a qc reading in MPa and fs reading in kPa by dividing by 1000 mm² and 15000mm² respectively.

Results of Calibration:

qc (tip resis Capacity:		(MPa)	Capacity:	, ,) (kPa)	u (pore pre Capacity:		(kPa)
• •								
Area		(mm²)	Area	15000 (mm²)		Position	u2	
Applied	Eqv.	Mean	Applied	Eqv.	Mean	Applied	Eqv.	Mean
Load	Pressure	Observed	Force	Load	Observed	Pressure	Pressure	Observed
kN	MPa	Reading	kN	kPa	Reading	bar	kPa	Reading
		Volts			Volts			Volts
0	0	0.000	0	0	0.000	0	0	0.000
10	10	0.784	3	200	0.804	3	300	0.348
20	20	1.583	6	400	1.585	6	600	0.695
30	30	2.383	9	600	2.377	9	900	1.042
40	40	3.183	12	800	3.175	12	1200	1.390
50	50	3.981	15	1000	3.971	15	1500	1.737
60	60	4.777	18	1200	4.769	18	1800	2.083
70	70	5.573	21	1400	5.567	21	2100	2.430
80	80	6.368	24	1600	6.363	25	2500	2.890
90	90	7.164	27	1800	7.166	30	3000	3.464
100	100	7.959	30	2000	7.967	35	3500	4.037
90	90	7.173	27	1800	7.176	30	3000	3.469
80	80	6.385	24	1600	6.379	25	2500	2.894
70	70	5.591	21	1400	5.578	21	2100	2.433
60	60	4.797	18	1200	4.776	18	1800	2.087
50	50	4.003	15	1000	3.979	15	1500	1.741
40	40	3.206	12	800	3.179	12	1200	1.393
30	30	2.406	9	600	2.375	9	900	1.045
20	20	1.604	6	400	1.583	6	600	0.697
10	10	0.802	3	200	0.808	3	300	0.349
0	0	0.002	0	0	0.003	0	0	0.000
R^2 Value =	1.000		R^2 Value =	1.000		R^2 Value =	1.000	
Zero Load Erro	or:	0.02%	Zero Load Err	or	0.04%	Zero Load Err	or:	0.01%
Max. Linearity		0.22%	Max. Linearit		0.18%	Max. Linearit		0.21%
Max. Hysteris		0.29%	Max. Hysteris	•	0.20%	Max. Hysteris	•	0.23%
MPa/Volt:		12.551	kPa/Volt:		251.08	kPa/Volt:		865.87
		12.331			231.00	•	calibrated):	0.83

"Class 1" Application Accuracy achieved (in accordance with ISO 22476:2012 classification)

Calibration Checked & Authorised:	Kylie Walker		
Job Details			
Client:	GB Geotechnics	Date of Job:	11/07/23
Rep:	Peter Eccleston	Tip Diameter:	35.65
Location: _	Parry Beach	Sleeve Diameter:	36.0

Tel:(08) 9417 9933 | Fax:(08)9417 3393 | Email: office@probedrill.com.au

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MOROOKA (M2)

11 tonne track mounted CPT Rig





SPECIFICATIONS

Overall Dimensions	Width: 2.3m; Length: 5.3m; Height: 3.2m (while travelling) Height: 4.4m (while probing)
Gross Weight	11 tonne
Ground Bearing Capacity	0.38 kg/cm ² (37kPa / 5.4psi)
Speed (Low/High)	Low gear: 8.3km High gear: 12km/h on level ground
Grade ability	60%
Engine	Mitsubishi (3910cc) 110 HP @ 2,800 rpm
Fuel Tank	80 L (Diesel)
Drive System	HST
Tracks	600mm wide rubber tracks
Levelling Jacks	0.8m stroke

EQUIPMENT / FEATURES

Other Equipment / Features	2.4m x 1.2m Plastic Bog Boards
	1 x 9kg ABE Fire extinguisher
	Air conditioned work cabin and drive cabin
Transport	Prime Mover & 10m Drop-deck trailer with ramps

SERVICES

Geotechnical Services	CPT, CPTu, SCPT, SCPTu (1, 5, 10, & 15 tonne cones)
provided	DMT, SDMT
	Dissipation Testing
	Ball Penetrometer
	CPT casing for additional rod support
	Dual Tube (percussion) sampling
	Piston Sampling
	MOSTAP and PROBEDRILL soil sampling
	Vane Shear Testing (Electronically driven)
	Vibrating Wire Installation
	Water Sampling
	Standpipe Installation (20mm; 32mm & 50mm)

Tel:(08) 9417 9933 | Fax:(08)9417 3393 | Email: office@probedrill.com.au

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