

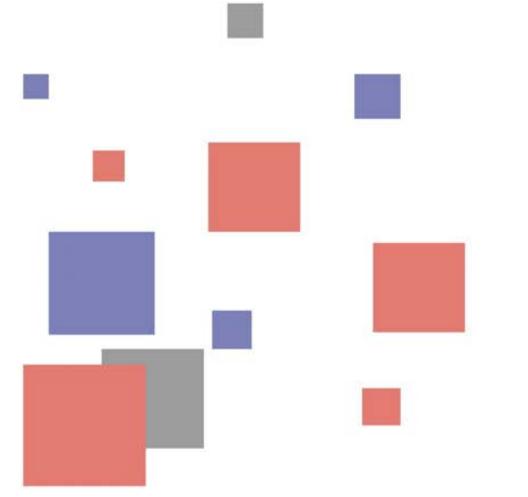
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Report

Geotechnical Investigation for Coastal Erosion Vulnerability Assessment.

Horrocks, Shire of Northampton WA.

Date: 8 September 2023 Report Ref: 3073L FINAL





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EXECUTIVE SUMMARY

A geotechnical investigation has been carried out as part of a coastal erosion assessment at Horrocks in the Shire of Northampton, Western Australia. During the investigation ground geophysical and intrusive geotechnical testing was conducted within a 900m corridor of coastal beach and dune formation adjacent to the Horrocks settlement which has been identified as an at-risk site as part of Coastal Hotspot #9.

The investigation scope consisted of acquiring multi-channel analysis of surface waves data as a series of specified transects either along-shore (parallel to the coast) or cross-shore (perpendicular to the coast) and cone penetration testing at spot locations along these transects. This was supplemented with geological mapping of surface rock outcrops and topographic survey using high resolution aerial photogrammetry for the generation of a surface level model and orthomosaic image.

The acquired MASW dataset was processed for the generation of seismic velocity sections along the transects showing variations in the seismic shear wave velocity of the subsurface material to a target depth of 10-15m below ground level. The seismic velocity sections were calibrated with the CPT plots and demarcated into velocity ranges representing different material types and conditions for the generation of interpreted geological sections consisting of loose to compacted sediment and variably weathered to fresh rock.

The interpreted geological sections have been compiled to develop subsurface models of the level to rock substrate (relative to AHD) and overlying sand thickness within the region between the foreshore and the settlement. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the settlement.

The following observations have been made:

- Interpreted rock substrate was observed along the entirety of the transects and within the maximum target investigation depth of 10-15m below ground level.
- Interpreted top of rock substrate on the along-shore transects on the beach ranged from -4mAHD to 3mAHD and averaged approximately 0.5mAHD with a thin layer of variably compacted sediment overlying this.
- Interpreted top of rock substrate on the along-shore transects on Glance Street immediately adjacent to the Horrocks settlement ranged from -1.5mAHD to 5.5mAHD and averaged approximately 1mAHD. Sand thickness overlying the top of rock for these transects averaged approximately 5m.
- Interpreted top of rock substrate was typically above 0mAHD for the cross-shore transects extending over the dune formation and with an average sand thickness of approximately 5m overlying this.



CONTENTS

1	INTF	RODUCTION	4
2	INVE	ESTIGATION SITE	4
3	INVE	ESTIGATION METHODOLOGY	6
	3.1	FIELD SURVEY LOGISTICS	6
	3.2	MULTI-CHANNEL ANALYSIS OF SURFACE WAVES	7
	3.3	CONE PENETRATION TESTING	9
	3.4	SPATIAL POSITIONING AND PHOTOGRAMMETRY	9
4	RES	ULTS AND INTERPRETATION	10
	4.1	PRESENTATION OF RESULTS	10
	4.2	SEISIMC SHEAR WAVE VELOCITY SECTIONS	11
	4.3	INTERPRETED GEOLOGICAL SECTIONS	11
	4.4	CALIBRATION WITH GEOTECHNICAL TESTING AND ROCK MAPPING	12
	4.5	MODELLED LEVEL TO TOP OF ROCK AND SAND THICKNESS	13
5	PRC	DJECT SUMMARY	14

APPENDIX A – INVESTIGATION SITE MAP	16
APPENDIX B – GEOPHYSICAL AND INTERPRETED SECTIONS	17
APPENDIX C – MODELLED TOP OF ROCK AND SAND THICKNESS	18
APPENDIX D – CONE PENETRATION TEST PLOTS	19

1 INTRODUCTION

At the request of The Government of Western Australia Department of Transport (DoT), GBG Group carried out a geotechnical investigation at Horrocks, Shire of Northampton in June 2023. During the investigation, seismic geophysical testing and intrusive geotechnical testing was conducted within a 900m corridor of coastal beach and dune formation which has been identified as an at risk site as part of Coastal Hotspot #9.

The objective of the investigation was to provide detailed mapping of the extent, elevation and consistency/strength of the rock underlying the coastal beach and dune formation. In particular, the key outcome of the investigation was to develop a subsurface model of the level to competent rock substrate (relative to AHD) within the region between the foreshore and the settlement. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the settlement.

To achieve the project objectives, data from the following investigation methods was acquired, processed and analysed so as to obtain the required subsurface information within the anticipated geological conditions:

- 1. **Geological mapping** of surface rock outcrops within the study area using high resolution photogrammetry.
- 2. **Geophysical testing** by way of Multi-channel Analysis of Surface Waves (MASW) to obtain seismic shear wave velocity models related to variations in subsurface material stiffness.
- 3. **Intrusive geotechnical testing** by way of Cone Penetration Testing (CPT) to measure sediment strength and compressibility, and for calibration and ground truthing of the geophysical dataset.
- 4. Topographic survey using Differential GNSS receiver and photogrammetry.

2 INVESTIGATION SITE

The investigation was carried out over an approximate 900m corridor of coastal beach and dune formation extending from the foreshore to the west, and to Glance Street to the east from Killy Street to North Court. The extent of the investigation site is shown as a yellow dashed area in Figure 1.

Data was acquired as a series of transects for the seismic geophysical testing and point locations for the intrusive geotechnical testing. These were positioned so as to best utilise existing roads, tracks, and beach whilst not impacting native vegetation and in order to ensure the most optimal, efficient and economical acquisition methodology. Data was not acquired where surface obstructions were present such as thick vegetation, steep topography or where the beach was inundated with seawater. Photographs showing the typical site conditions are provided in Figure 2.



Topography at the site was undulating with an elevation difference between the foreshore at ~0-2mAHD, the dune formation and the central portion of the existing settlement at ~2-6mAHD, and the northern and southern portions of the existing settlement at ~6-8mAHD and up to ~15mAHD respectively. A topographic map showing surface level is provided in Appendix C drawing 3073L-10.



Figure 1: The extent of the geophysical investigation (yellow polygon) at Horrocks. Aerial imagery from drone photogrammetry (main image) and Google Maps (inset image).





Figure 2: Site conditions at Horrocks including along the beach foreshore (left image) and the dune system (right image).

3 INVESTIGATION METHODOLOGY

3.1 FIELD SURVEY LOGISTICS

Geophysical data acquisition was carried out on the 19 to 22 June 2023 by a three-person crew from GBG Group consisting of a qualified geophysicist, geologist and field assistant. CPT data acquisition was carried out by a technician from Probedrill on the 19 and 20 June 2023. Where required, the site work was carried out under appropriate traffic and pedestrian management commissioned by the Shire of Northampton.

Prior to the commencement of data acquisition, a site assessment was carried out with representatives from the Shire of Northampton. Potential concerns and issues including the placement of and access to the MASW transects and CPT points were addressed and the initial indicative survey plan was adjusted, where necessary.

The site work for the investigation consisted of a total of 1752m of MASW profiling acquired as 7 alongshore transects (parallel to the coast) and 4 cross-shore transects (perpendicular to the coast), and a total of 6 CPT points along the transects. Details of the acquired MASW transects and CPT points are provided in Tables 1 and 2 respectively. The extents of the MASW transects and locations of the CPT points overlaid onto aerial imagery are shown in Appendix A drawing 3073L-01.

Transect ID Orientation		Start Coordinate		End Coordinate		Length
		East	North	East	North	(m)
MASW01a	Along-shore	248260.6	6857224.8	248104.6	6857792.0	552
MASW01b	Along-shore	248111.1	6857792.7	248047.8	6858066.8	264
MASW02a	Along-shore	248309.5	6857230.9	248273.9	6857421.0	184
MASW02b & 02c	Along-shore	248269.4	6857420.2	248181.5	6857833.5	408
MASW02d	Along-shore	248180.5	6857838.4	248122.0	6857850.7	56
MASW02e	Along-shore	248126.0	6857849.6	248104.8	6857933.3	80
MASW03	Along-shore	248108.6	6858003.1	248100.0	6858035.1	32

Table 1 – Acquired MASW Transects (Coordinates in GDA94, MGA Zone 50).



MASW04	Cross-shore	248269.6	6857241.0	248312.6	6857243.2	48
MASW05	Cross-shore	248233.3	6857442.5	248243.0	6857475.6	32
MASW06	Cross-shore	248118.4	6857793.8	248177.3	6857799.4	56
MASW07	Cross-shore	248087.9	6857982.1	248124.8	6858000.4	40

Table 2 – Acquired CPT Points (Coordinates in GDA94, MGA Zone 50).

СРТ	Соог	dinate	Surface	Probing	
ID	East	North	Level (mAHD)	Depth (m)	
CPT01	248106.3	6857782.7	1.01	2.94	
CPT02	248050.2	6857938.2	1.03	2.38	
CPT03	248237.8	6857467.9	3.48	3.60	
CPT04	248189.1	6857648.1	4.13	3.96	
CPT05	248100.1	6858010.6	6.82	6.44	
CPT06	248254.2	6857353.3	1.64	0.86	

3.2 MULTI-CHANNEL ANALYSIS OF SURFACE WAVES

MASW is a seismic geophysical method that utilises phase and frequency information to calculate Shear wave (S-wave) velocities in vertical layer models averaged over an array of linearly spaced geophones. These 1D models can be laterally stacked to provide 2D cross-sections of S-wave velocity in layers. Under most circumstances it is an indicator of material stiffness and as such the method can be used to provide quantitative results on the compaction of the subsurface material.

MASW data was acquired using a Geode (Geometrics) seismograph connected to a receiver array of 24 geophones set at 1m intervals for a total array length of 23m. The receiver array was mobilised on a land streamer whereby the geophones are mounted on base plates attached to webbing, and either towed behind a 4WD light vehicle or manually pulled by the field team. Seismic energy was generated using summed impacts from a PEG-40 (R.T. Clark) vehicle mounted accelerated weight drop or softened steel sledgehammer with source points made at a constant offset from receiver array. MASW acquisition parameters are provided in Table 3. Photographs of MASW data acquisition are shown in Figure 3.

Parameter	Value	
Number of geophones	24	
Geophone spacing	1 m	
Array length	23 m	
Geophone frequency	4.5 Hz	
Record length	1 s	
Sample interval	0.25 ms	
Source	40kg AWD or 6.35kg sledgehammer	
Source offset	4 m	
Sounding interval	8m	
Source stacks	3	





Figure 3: MASW data acquisition using a seismic streamer.

The MASW data was observed to be of high quality with the seismic records having high signal to noise ratio. The generated overtone images plotting phase velocity against frequency showed a prominent dispersion curve of the surface wave component. The MASW data was processed using SurfSeis version 6++ (Kansas Geological Survey, 2017) with the following processing routine:

- 1. Import acquired seismic data files and apply geometry including geophone spacing, source offset and sounding interval.
- 2. Generate overtone images giving the percentage intensity of phase velocity versus frequency for each seismic record (Figure 4, left image).
- 3. Pick the maximum intensity across the useful range of frequencies for each overtone image resulting in a dispersion curve.
- 4. Run the dispersion curves through a 10-layer inversion algorithm to produce 1D soundings plotting seismic S-wave velocity with depth (Figure 4, right image).

The S-wave velocity soundings were compiled with reference to distance along the transects and gridded with Surfer version 25 (Golden Software, 2023). The resulting contoured cross-sections show the variation in the modelled S-wave velocity of the subsurface material in metres per second laterally along each of the transects and with elevation.

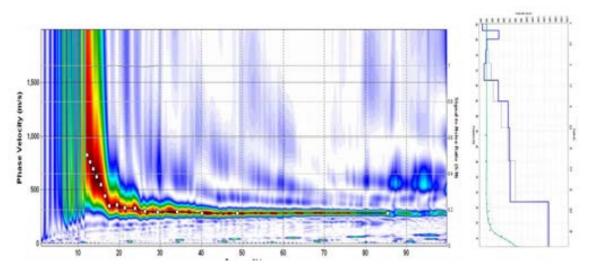


Figure 4: MASW overtone image with high signal to noise ratio and picked dispersion curve.

3.3 CONE PENETRATION TESTING

CPT is a geotechnical test method for evaluating the properties of soils and assessing subsurface stratigraphy including the sediment/rock interface at spot locations. The method involves pushing a calibrated cone and rod into the ground with a measured force with the resulting friction resistance plotted against depth to provide sediment compaction rates as well as the refusal depth indicating the depth to competent rock.

Testing was carried out using a M2 (Morooka) 11 tonne track mounted CPT Rig, specifications of which are provided in Appendix D. The test points were initially marked out at suitable locations within 2m of the intersecting geophysical transects. Dial Before You Dig enquiries and if necessary, utility locating was carried out prior to testing commencing.

CPT readings was made with sufficient ground bearing pressure to obtain a target depth of 10m or prior refusal. Where shallow refusal depths of less than 2m was encountered, when deemed necessary, an additional offset test was made to ascertain whether shallow refusal was due to a rock floater or other shallow obstruction. A photograph of CPT data acquisition is shown in Figure 5.



Figure 5: CPT data acquisition during a previous coastal investigation.

3.4 SPATIAL POSITIONING AND PHOTOGRAMMETRY

Spatial positioning of the acquired geophysical transects was achieved using Reach RS2 (Emlid) or S631 (Hemisphere) GNSS receivers with a coordinate recorded for each MASW sounding location and CPT point. Coordinates of the geophysical transects have been provided in GDA94, MGA zone 50 for horizontal component and Australian Height Datum (mAHD) for vertical component. An accuracy of +/- 0.2m is expected for both vertical and horizontal components.

To achieve precise reduced levels referenced to AHD, the positioning data was acquired with Real-Time Kinematics (RTK), using Standard Survey Markers (SSM) as known reference points for the base corrections. Details of the SSM used for this investigation are provided in Table 4.



Parameter	Value
Standard Survey Marker	GERALDTON 112
Latitude	S 28 23 05.82553
Longitude	E 114 26 14.91569
Derived GDA94 ellipsoidal height (m)	36.560
N-Value (m)	-22.960
Height (m) (AHD)	59.520

Table 4 – Details of Standard Survey Marker

A reduced level of 0.0mAHD is considered to be the Mean Sea Level (MSL) for the purpose of this investigation. This relationship for Mean Sea Level was established by the Geoscience Australia Survey in 1971 (http://www.ga.gov.au/scientific-topics/positioning-navigation/geodesy/datums-projections/australian-height-datum-ahd).

Aerial photogrammetry was carried out to obtain an up-to-date high-resolution aerial image and a surface level model of the survey area. Data was acquired with a Matrice 300 (DJI) multi-rotor drone, equipped with a L1 (Zenmuse) camera for the capture of multiple overlapping images.

The acquired photogrammetry images were processed using Metashape Professional (Agisoft) for the generation of a point cloud, surface level model and orthomosaic image of the survey area. Note: for this investigation, vegetation has not been removed during the processing stage and as such the height of existing vegetation needs to be considered when assessing surface levels.

4 RESULTS AND INTERPRETATION

4.1 **PRESENTATION OF RESULTS**

The results of the geotechnical investigation at Horrocks, Shire of Northampton are presented in Appendices B and C of this report as follows:

Appendix B – Geophysical and Interpreted Sections

- **3073L-02 and 3073L-03.** Transect 1 seismic S-wave velocity model and interpreted geological section.
- **3073L-04.** Transect 1b seismic S-wave velocity model and interpreted geological section.
- 3073L-05. Transect 2a seismic S-wave velocity model and interpreted geological section.
- **3073L-06 and 3073L-07.** Transect 2b and 2c seismic S-wave velocity model and interpreted geological section.
- **3073L-08.** Transects 2d, 2e and 3 seismic S-wave velocity model and interpreted geological section.
- **3073L-09.** Transects 4, 5, 6 and 7 seismic S-wave velocity model and interpreted geological section.

Appendix C – Modelled Level to Top of Rock and Sand Thickness

- 3073L-10 and 3073L-11. Contoured surface level model derived from aerial photogrammetry.
- 3073L-12 and 3073L-13. Contoured level to modelled top of rock.
- 3073L-14. Class post map level to modelled top of rock.
- 3073L-15 and 3073L-16. Contoured modelled sand thickness over rock.
- 3073L-17. Class post map modelled sand thickness over rock.

4.2 SEISIMC SHEAR WAVE VELOCITY SECTIONS

The seismic S-wave velocity (Vs) sections modelled from the MASW data acquired along the alongshore and cross-shore transects are presented at the top of each drawing in Appendix B. These sections show variations in the modelled Vs as per the colour scale with velocity ranging from 150m/s to 1000m/s representing a wide range of material types and conditions.

Seismic S-wave velocity is governed by the elastic properties of the medium that the wave propagates through as shown in the equation below. In particular, it is primarily a function of soil density, void ratio and effective stress. As such calculated values can provide a useful guide to the subsurface material condition with increasing velocity an indication of increasing material stiffness.

Seismic S-wave velocity

$$V_S = \sqrt{\frac{G}{\rho}}$$

where; G = Shear modulus, ρ = In-situ material density

4.3 INTERPRETED GEOLOGICAL SECTIONS

Below the seismic S-wave velocity sections are the interpreted geological sections based on detectable seismic velocity contrasts correlated with the CPT. Four classes have been defined representing different subsurface material conditions as follows:

- 1. Very low seismic S-wave velocity (Vs <250m/s). Representing the lowest seismic velocities modelled during the investigation, this class is interpreted as sediment consisting of SAND of low compaction from either the beach or dune formation.
- 2. Low seismic S-wave velocity (Vs 250-350m/s). This class is interpreted as sediment consisting of SAND of moderate compaction either due to increased depth of cover on the beach and dune formation, or due to development adjacent to the settlement.
- 3. **Moderate seismic S-wave velocity** (Vs 350-475m/s). This class is interpreted as low strength rock consisting of variably weathered CALCARENITE. Where continuous and at



base of the sections it likely represents a transitional zone to stronger, more competent underlying CALCARENITE. Where present as isolated anomalies within the interpreted SAND it is likely to represent partially lithified SAND and/or CALCARENITE lenses.

4. **Moderate to high seismic wave velocity** (Vs >475m/s). This class is interpreted as moderate strength rock consisting of slightly weathered to fresh CALCARENITE. It is typically observed at the base of the sections as competent rock underlying the variably weathered CALCARENITE.

4.4 CALIBRATION WITH GEOTECHNICAL TESTING AND ROCK MAPPING

The results of the CPTs are presented in Appendix D showing the plots of cone tip resistance in megapascals against depth in metres. The CPT plots are also shown in Appendix B and overlayed onto the interpreted geological sections with the following observations being made:

- **CPT-01 on Transect 1a** refusal of 40MPa plus inclination was at a depth of 2.9m Below Ground Level (BGL) which corresponds to the top of interpreted low strength rock.
- **CPT-02 on Transect 1b** refusal of 65MPa plus rod friction was at 2.4mBGL within interpreted moderate strength rock. Note this CPT was offset from the geophysical transect by 10m due to access difficulties for the CPT rig.
- **CPT-03 on Transect 2bc and 5** refusal of 100MPa was at 4.6mBGL which corresponds to the top of interpreted low strength rock on both intersecting transects.
- **CPT-04 on Transect 2bc** refusal of 65MPa plus rod friction was at 4mBGL which corresponds to the top of interpreted low strength rock.
- **CPT-05 on Transect 3** refusal of 70MPa plus rod friction was at 6.4mBGL within interpreted moderate strength rock. The CPT penetrated approximately 3.5m into rock before refusal suggesting a variably weathered material.
- **CPT-06 on Transect 1a** refusal was of 60MPa plus rod friction at 0.8mBGL which corresponds to the top of interpreted moderate strength rock.

The differences in the modelled level to low strength and moderate strength rock as interpreted from the MASW transects and from the CPT data can be attributed to the fact that the geophysical methods used are broad scale whilst the CPT is a point method. Geophysical methods sample a volume of subsurface material with the calculated depths at any particular point representing an average value over this volume. The CPT method samples the subsurface directly below the probe and is influenced by local variations in the subsurface such as rock floaters, highly weathered zones or lenses of partially lithified sediment. The differences in the type of subsurface sampling of the methods will not adversely affect the results as the CPT results have been used to constrain the geophysics interpretation and as such the results represent the best modelled fit between the datasets.



Surface outcropping rock was observed on the beach directly to the south of the investigation area in line with Killy Street. This corresponds to the interpreted shallow rock present at the start of Transect 1a along the beach. Rock outcrop was also visible below the water on the southern portion of the site from the orthomosaic image which corresponds to the shallow rock present along Transects 1a and 1b along the beach.

4.5 MODELLED LEVEL TO TOP OF ROCK AND SAND THICKNESS

Subsurface models for the level to top of rock substrate and overlying sand thickness within the region between the coastal foreshore and settlement are presented in Appendix C. These has been generated by digitising the interface between the interpreted sediment and underling rock profile from the interpreted geological sections along the acquired along-shore and cross-shore transects and calibrated with the CPT plots. The modelled sand thickness was then generated by subtracting this from the surface elevation. The following subsurface models have been provided:

- **Contoured Surface Level Model** (drawing 3073L-10 and 3073L-11) generated from the aerial photogrammetry, this presents the level to ground surface ranging from 0mAHD to 16mAHD. Note: vegetation height has not been removed from these models.
- Contoured Level to Top of Rock Substrate (drawing 3073L-12 and 3073L-13) this presents the level to the top of rock substrate ranging from -5mAHD to 5mAHD.
- Classed Post Map Level to Top of Rock Substrate (drawing 3073L-14) this presents the level to the top of rock substrate along the acquired transects at 2m level increments from 6mAHD to 6mAHD.
- **Contoured Sand Thickness Over Rock** (drawing 3073L-15 and 3073L-16) this presents the thickness of sand overlying the rock substrate ranging from 0mBGL to 6mBGL.
- Classed Post Map Sand Thickness Over Rock (drawing 3073L-17) this presents the thickness of sand overlying the rock substrate along the acquired transects at 1m depth increments from 1mBGL to 6mBGL.

The following limitations should be considered when assessing the subsurface models for the level to top of rock substrate and overlying sand thickness:

The expected accuracy of the top of rock substrate modelled from this investigation is +/-0.5mAHD. Similarly, an accuracy of +/-0.5m is expected for the modelled sand thickness over rock. The quoted accuracies have been based on consideration to the accuracy of the GNSS receivers using during the site work, 1D inversion of the MASW dataset using a 10-layer model, and expected undulations in the sand/rock interface. Note the quoted accuracies are only valid along the geophysical transects. Values given between transects have been interpolated in the contour maps and as such the accuracy in this case is indeterminable.



The generated contours will give the general trend of the top of rock profile however will not image local variations when the extent of these is less than transect spacing. Spatially small features such as karst sinkholes or pinnacle features may not be imaged. The significance of this limitation is considered minor for this investigation since although local geological features such as pinnacles may not be represented in the data, the generated surface of the top of rock will show the broad trends in the geology over the site which is suitable for a coastal erosion assessment.

Transition zones including between fresh and weathered rock and between sediment and lithified/partially lithified sediment may be gradational and as such the interface between these layers are not well defined.

The calculated levels to the top of rock will only be valid along the geophysical transects. Values shown on the contour maps not on the transects have been interpolated using the krigging algorithm and as such the accuracy of these levels is indeterminable. The contour surface will give the general trend of the interface however may not image local variations, it is recommended that the interpreted geological sections presented in Appendix B be used to obtain more accurate top of rock levels and overlying sand thickness.

5 PROJECT SUMMARY

A geotechnical investigation has been carried out as part of a coastal erosion assessment at Horrocks in the Shire of Northampton, Western Australia. During the investigation ground geophysical and intrusive geotechnical testing was conducted within a 900m corridor of coastal beach and dune formation adjacent to the Horrocks settlement which has been identified as an at risk site as part of Coastal Hotspot #9.

The investigation scope consisted of acquiring multi-channel analysis of surface waves data as a series of specified transects either along-shore (parallel to the coast) or cross-shore (perpendicular to the coast) and cone penetration testing at spot locations along these transects. This was supplemented with geological mapping of surface rock outcrops and topographic survey using high resolution photogrammetry for the generation of a surface level model and orthomosaic image.

The acquired MASW dataset was processed for the generation of seismic velocity sections along the transects showing variations in the seismic shear wave velocity of the subsurface material to a target depth of 10-15m below ground level. The seismic velocity sections were calibrated with the CPT plots and demarcated into velocity ranges representing different material types and conditions for the generation of interpreted geological sections consisting of loose to compacted sediment and variably weathered to fresh rock.

The interpreted geological sections have been compiled to develop subsurface models of the level to rock substrate (relative to AHD) and overlying sand thickness within the region between the foreshore and the settlement. This model will be used to assess the potential vulnerability of the site to erosion and future inundation risk, and whether there is a continuous rock barrier located below the ground surface of sufficient strength and height that may prevent the advancement of erosion to the settlement.



The methods used during the investigation are geophysical and as such the results are based on indirect measurements and the processing and interpretation of seismic wave signals calibrated with limited intrusive geotechnical testing. The findings in this report represent the professional opinions of the authors, based on experience gained during previous similar investigations.

We trust that this report and the attached drawings provide you with the information required. If you require clarification on any points arising from this geophysical investigation, please do not hesitate to contact the undersigned on 08 9354 6300.

For and on behalf of GBG GEOTECHNICS (AUSTRALIA)

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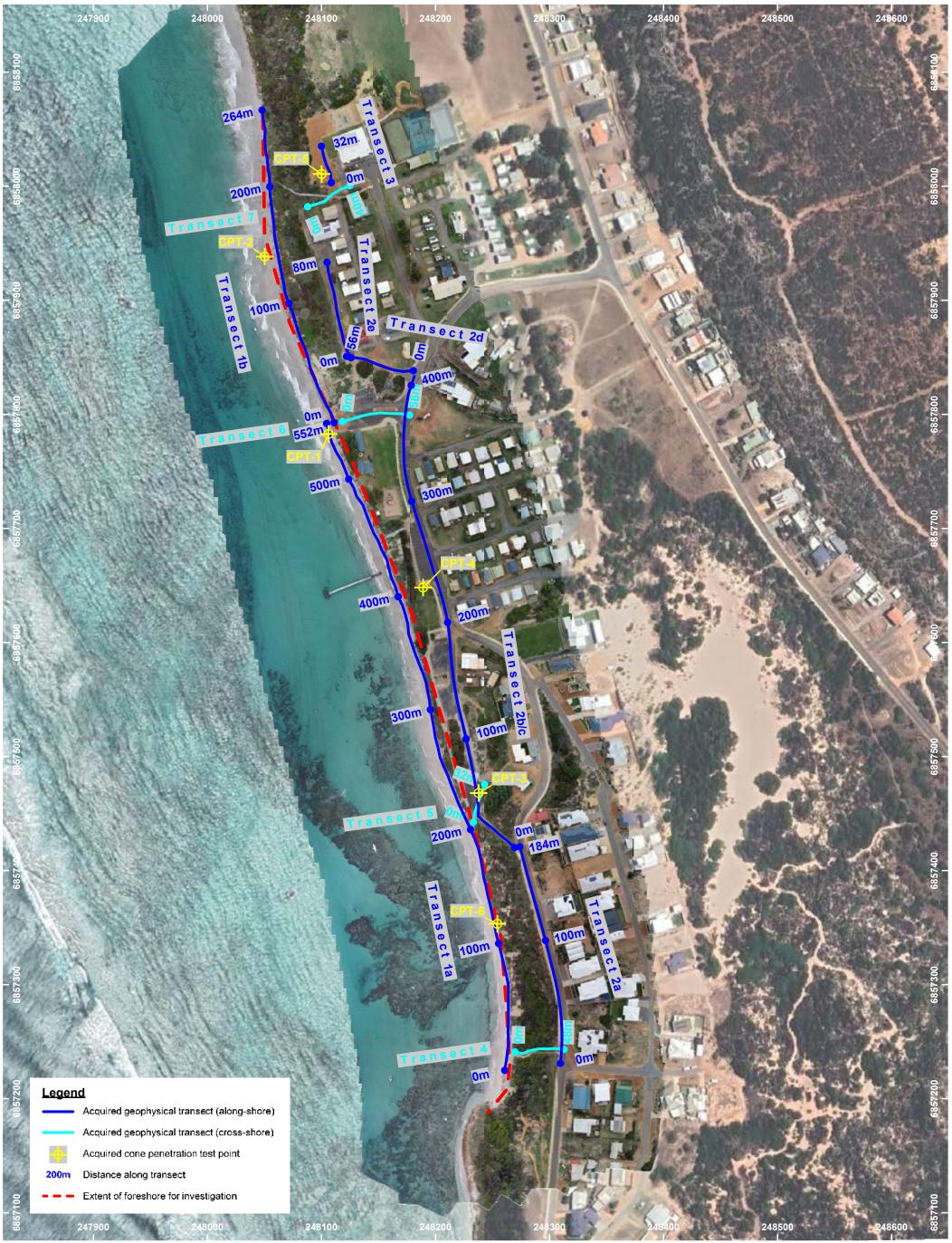
ANDREW SPYROU Operations Manager, Western Australia / Senior Geophysicist



APPENDIX A – INVESTIGATION SITE MAP



INVESTIGATION SITE MAP



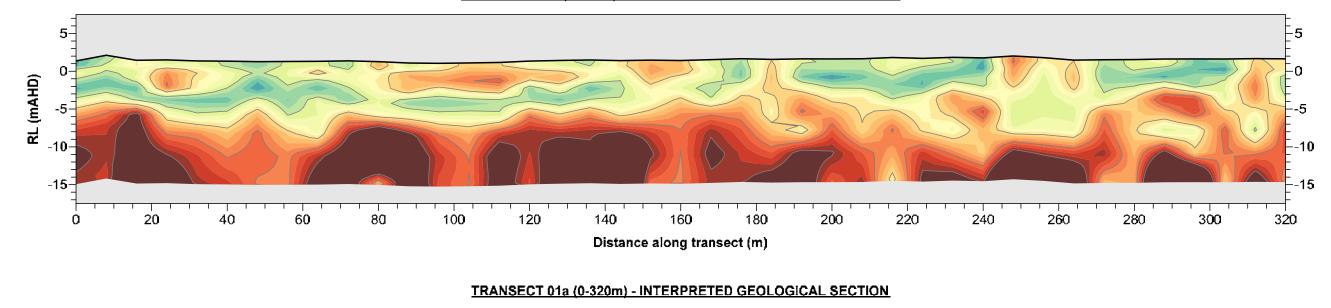
NOTES Drawing to be used in conjunction with GBG	Ņ	Date	2 May 2023	Paper Size	A3	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA		ABN: 77 009 550 869
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Aerial image from Google Earth Pro and GBG photogrammetry.	V	Drawing	3073L-01	Revision	С	HORROCKS, SHIRE OF NORTHAMPTON WA	GB Geotechnics (Australia) Pty Ltc V	Yeb: gbg-group.com.au

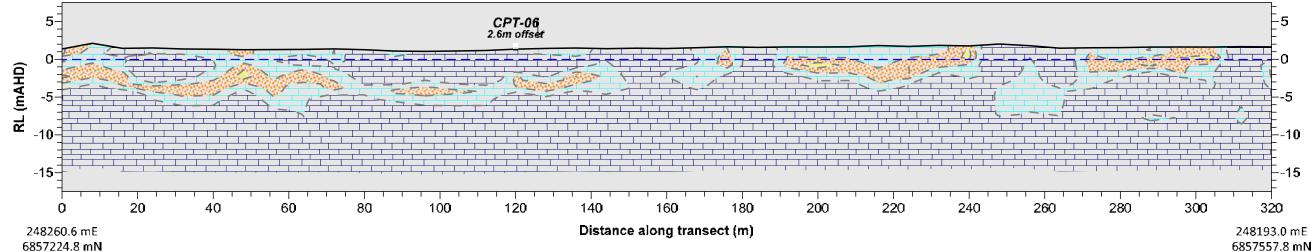


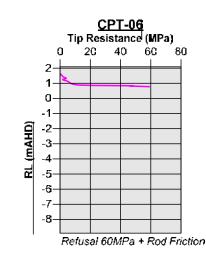
APPENDIX B – GEOPHYSICAL AND INTERPRETED SECTIONS



TRANSECT 01a (0-320m) - SEISMIC SHEAR WAVE VELOCITY MODEL



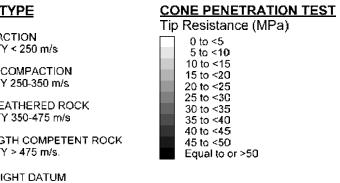




<u>1</u>	SEIS	SMIC	: S-V	VAV	<u>E VI</u>	ELO	CITY	<u>((m</u>	<u>/s)</u>	INTERPR	ETED MATERIAL TYP
											SAND - LOW COMPACTIC S-WAVE VELOCITY < 2
	200	300	400	500	600	700	800	006	1000		SAND - MODERATE COM S-WAVE VELOCITY 250
											LOW STRENGTH WEATH S-WAVE VELOCITY 350
											MODERATE STRENGTH (S-WAVE VELOCITY > 4
	I	I	I	I	I	I	I	I			0m AUSTRALIAN HEIGHT

ES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073L. Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL	Scale	1:1000 H , 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		EROSION VULNERABLITY ASSESSMENT HORROCKS, SHIRE OF NORTHAMPTON WA	Drawing	3073L-02	Revision	С

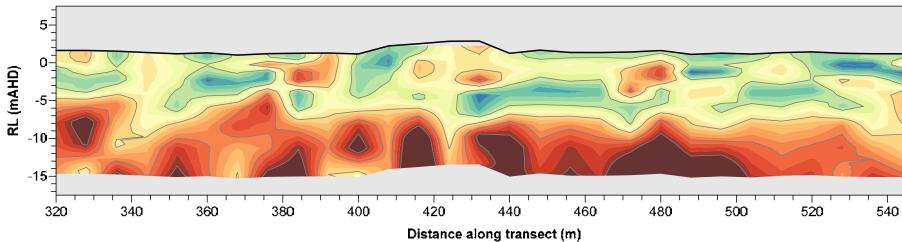
6857557.8 mN



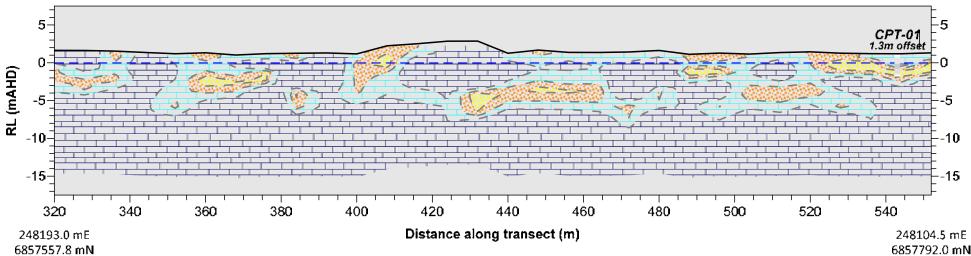


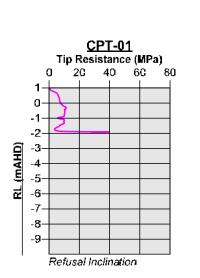


TRANSECT 01a (320-552m) - SEISMIC SHEAR WAVE VELOCITY MODEL



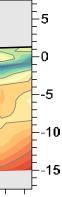
TRANSECT 01a (320-552m) - INTERPRETED GEOLOGICAL SECTION





<u>SEIS</u>	SMIC	: <u>s-I</u>	NAV	<u>E VI</u>	ELO	CITY	<u>(m</u>	<u>/s)</u>	INTERPR	ETED MATERIAL
										SAND - LOW COMP/ S-WAVE VELOCIT
200	300	400	500	600	700	800	006	1000		SAND - MODERATE S-WAVE VELOCIT
										LOW STRENGTH W S-WAVE VELOCIT
										MODERATE STREN
I	I		I	I		Į	I			0m AUSTRALIAN HE

NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073L. Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL	Scale	1:1000H. 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		EROSION VULNERABLITY ASSESSMENT HORROCKS, SHIRE OF NORTHAMPTON WA	Drawing	3073L-03	Revision	С



6857792.0 mN

TYPE

PACTION CITY < 250 m/s

E COMPACTION TY 250-350 m/s

VEATHERED ROCK ITY 350-475 m/s

NGTH COMPETENT ROCK ITY > 475 m/s.

EIGHT DATUM

CONE PENETRATION TEST

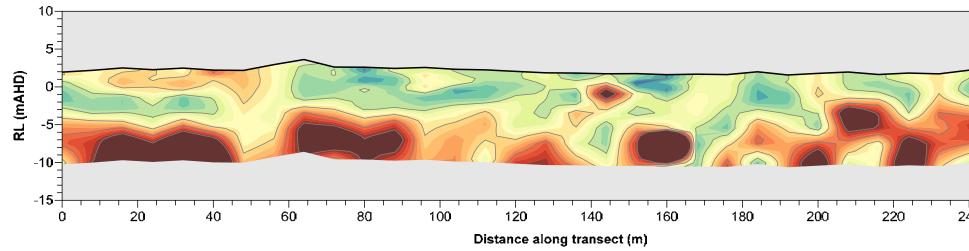
Tip Resistance (MPa)

0 to <5 5 to <10 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50

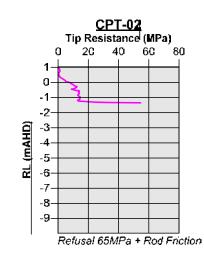
GBGGROUP





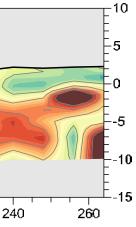


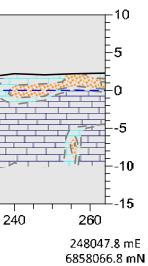
TRANSECT 01b - INTERPRETED GEOLOGICAL SECTION 10 5 CPT-02 10.0m offset RL (mAHD) (1)-10 -15-20 60 80 100 120 140 160 200 40 180 220 0 248111.1 mE Distance along transect (m) 6857792.7 mN



<u>SEI</u>	SMIC	<u>: s-v</u>	NAV	<u>e vi</u>	ELO	<u>ידו </u>	<u> (m</u>	<u>/s)</u>	INTERPR	ETED MATERIAL TYP
										SAND - LOW COMPACTI S-WAVE VELOCITY < 2
200	300	400	500	003	700	008	006	1000		SAND - MODERATE CON S-WAVE VELOCITY 25
										LOW STRENGTH WEAT S-WAVE VELOCITY 35
										MODERATE STRENGTH S-WAVE VELOCITY > 4
ļ	I	I	I	I	ļ	I				0m AUSTRALIAN HEIGH

NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073L. Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL	Scale	1:1000H. 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		EROSION VULNERABLITY ASSESSMENT HORROCKS, SHIRE OF NORTHAMPTON WA	Drawing	3073L-04	Revision	С



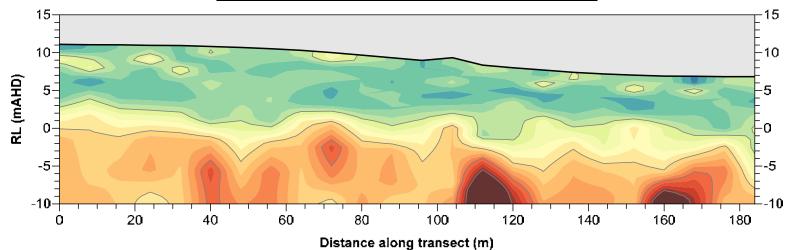


ΈE CONE PENETRATION TEST Tip Resistance (MPa) 0 to <5 5 to <10 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50 TION < 250 m/s MPACTION 250-350 m/s THERED ROCK 350-475 m/s H COMPETENT ROCK • 475 m/s. HT DATUM

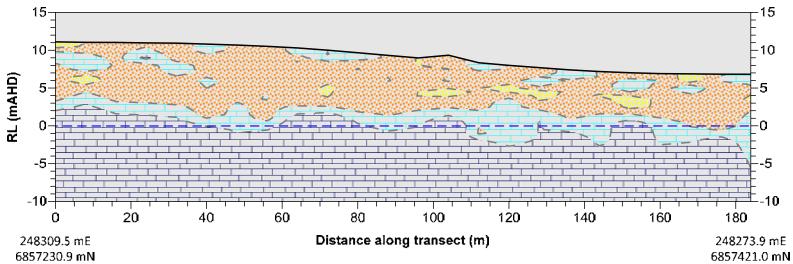


GBGGROUP

TRANSECT 02a - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 02a - INTERPRETED GEOLOGICAL SECTION



<u>\$E</u>	ISMI	CS	-WA\	/E VI	ELO	<u>CIT'</u>	<mark>/ (</mark> m	<u>/s)</u>	INTERPR	ETED MATER
										SAND - LOW C S-WAVE VE
200	300	400	500	600	700	008	900	1000		SAND - MODE S-WAVE VE
										LOW STRENG

0m AUSTRALIAN HEIGHT DATUM

NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073L. Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL	Scale	1:1000 H . 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		EROSION VULNERABLITY ASSESSMENT HORROCKS, SHIRE OF NORTHAMPTON WA	Drawing	3073L-05	Revision	С

ERIAL TYPE

/ COMPACTION /ELOCITY < 250 m/s

ERATE COMPACTION ELOCITY 250-350 m/s

OW STRENGTH WEATHERED ROCK S-WAVE VELOCITY 350-475 m/s

MODERATE STRENGTH COMPETENT ROCK S-WAVE VELOCITY > 475 m/s.

CONE PENETRATION TEST

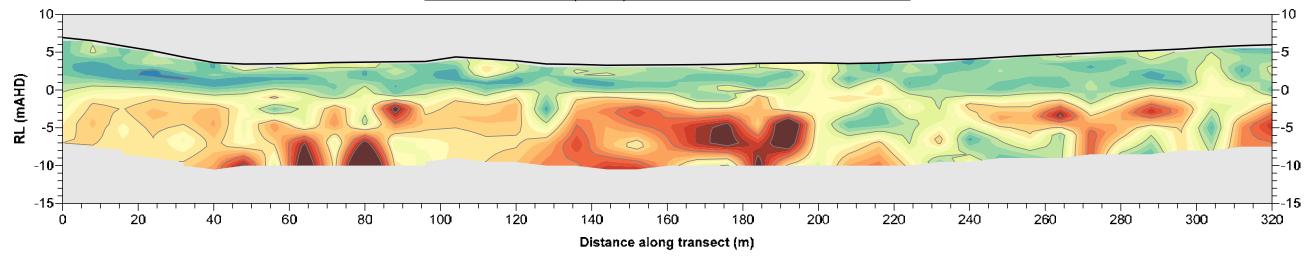
Tip Resistance (MPa)

0 to <5 5 to <10 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50

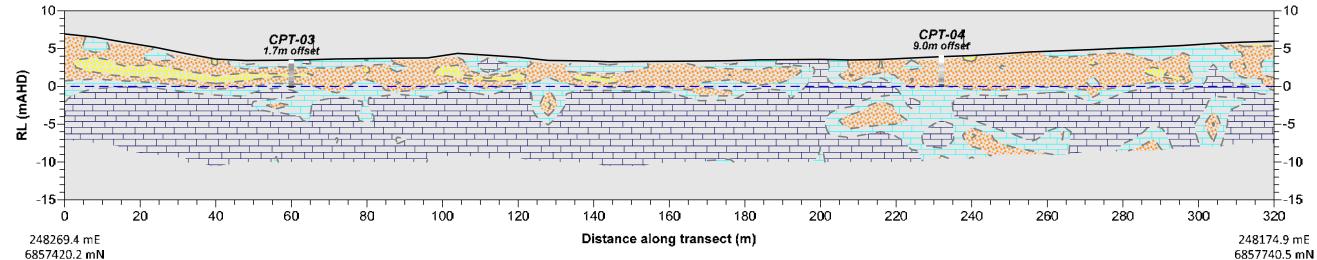
GBGGROUP

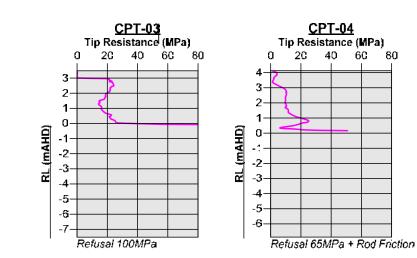


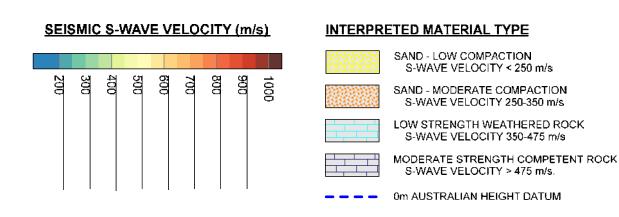
TRANSECT 02b and 2c (0-320m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 02b and 2c (0-320m) - INTERPRETED GEOLOGICAL SECTION





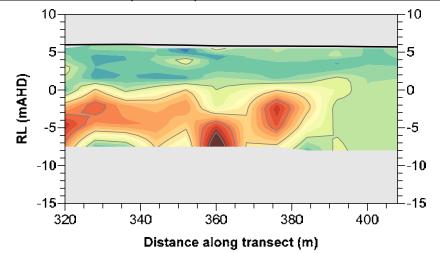


NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073L. Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT	Scale	1:1000 H , 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		HORROCKS, SHIRE OF NORTHAMPTON WA	Drawing	3073L-06	Revision	С

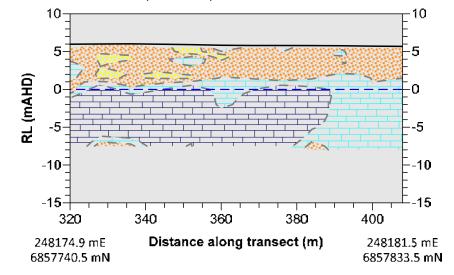
CONE PENETRATION TEST Tip Resistance (MPa) 0 to <5 5 to <10 10 to <15 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50



TRANSECT 02b and 2c (320-408m) - SEISMIC SHEAR WAVE VELOCITY MODEL



TRANSECT 02b and 2c (320-408m) - INTERPRETED GEOLOGICAL SECTION



INTERPRETED MATERIAL TYPE

SAND - LOW COMPACTIO
S-WAVE VELOCITY < 2
SAND - MODERATE COMP
S-WAVE VELOCITY 250
LOW STRENGTH WEATH
S-WAVE VELOCITY 350
MODERATE STRENGTH C
S-WAVE VELOCITY > 4

SEISMIC S-WAVE VELOCITY (m/s)

200	300	400	500	600	700	008	006	1000
		٦		1	1	1		00

NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073L. Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT	Scale	1:1000 H . 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		HORROCKS, SHIRE OF NORTHAMPTON WA	Drawing	3073L-07	Revision	С

GBGGROUP

ЛC 250 m/s

PACTION 0-350 m/s

IERED ROCK 0-475 m/s

COMPETENT ROCK 175 m/s.

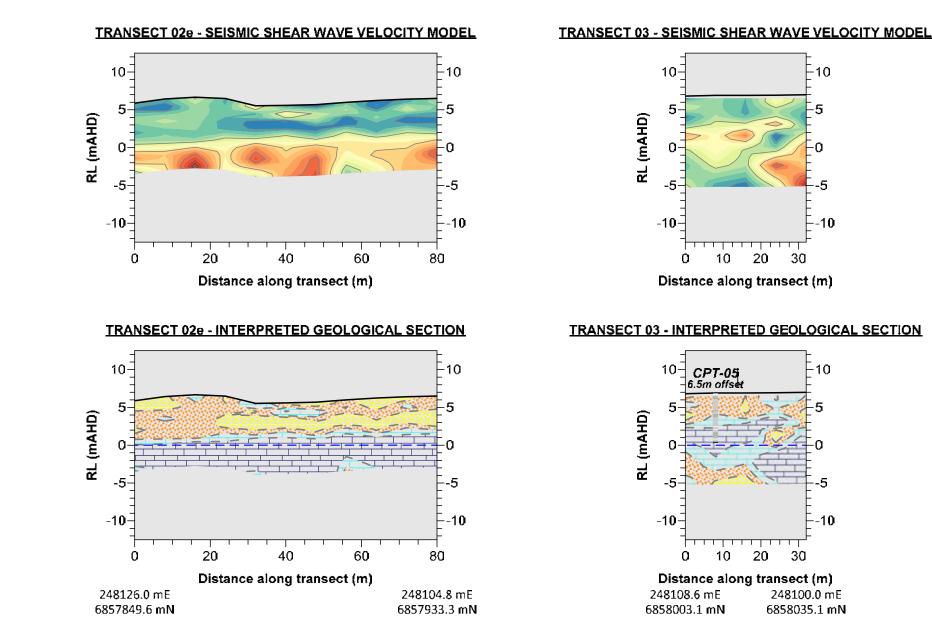
- 0m AUSTRALIAN HEIGHT DATUM

CONE PENETRATION TEST

Tip Resistance (MPa)

0 to <5 5 to <10 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50

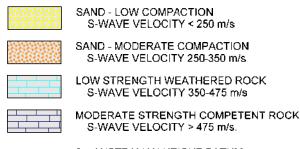
GBGGROUP



SEISMIC S-WAVE VELOCITY (m/s) .

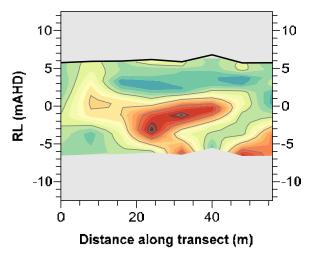
500 400 300



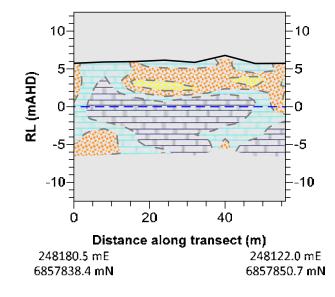


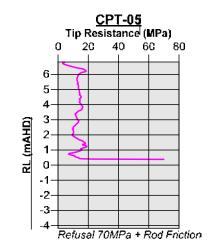
0m AUSTRALIAN HEIGHT DATUM

GBGGROUP



TRANSECT 02d - INTERPRETED GEOLOGICAL SECTION





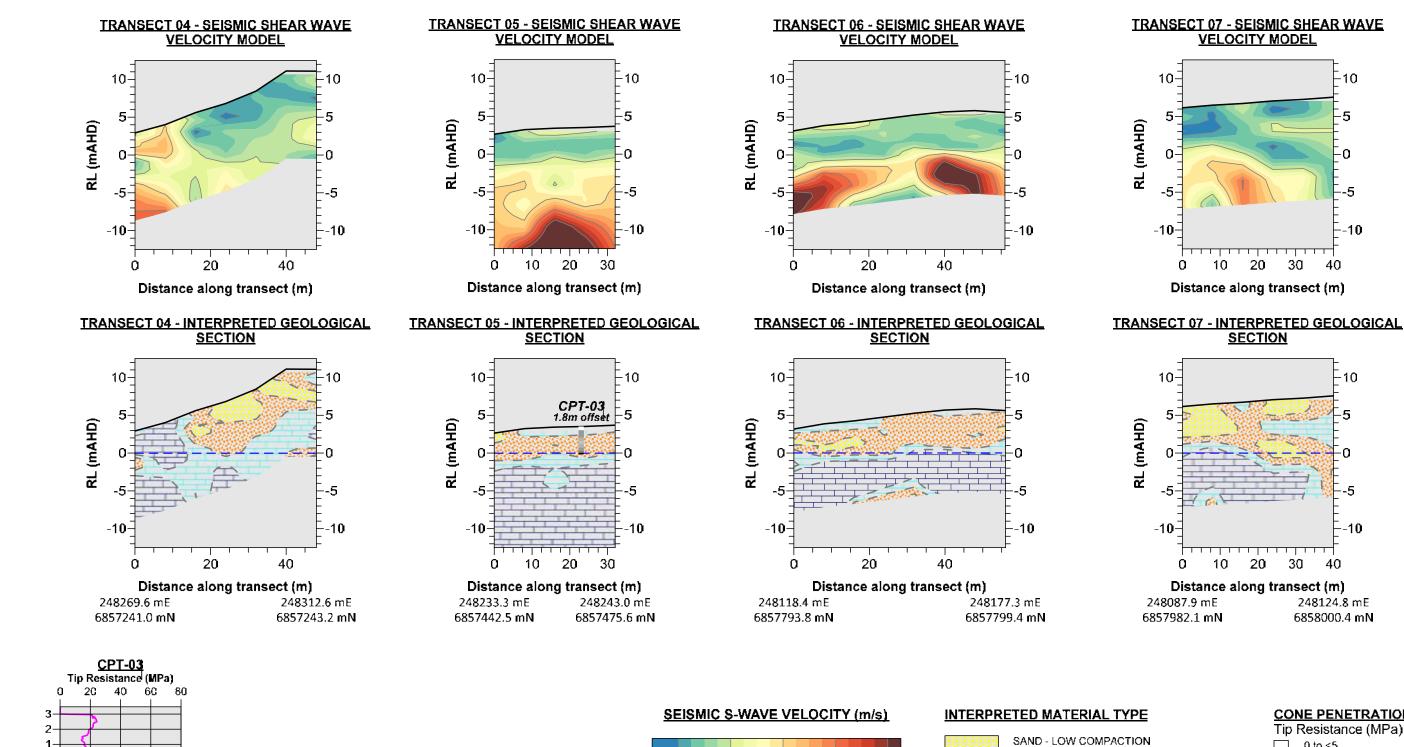
NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
Drawing to be used in conjunction with Report 3073L. Positioning is given in GDA 94 zone 50.		GEOPHYSICAL INVESTIGATION FOR COASTAL EROSION VULNERABLITY ASSESSMENT	Scale	1:1000 H , 1:500V	Drawn	PJE
Levels are given in Australian Height Datum (AHD).		HORROCKS, SHIRE OF NORTHAMPTON WA	Drawing	3073L-08	Revision	С

248100.0 mE 6858035.1 mN

CONE PENETRATION TEST Tip Resistance (MPa) 0 to <5 5 to <10 10 to <15 10 to <15 15 to <20 20 to <25 25 to <30 30 to <35 35 to <40 40 to <45 45 to <50 Equal to or >50

GBGGROUP





000

700 008 006 1000

300 400 200

200

Drawing to be used in conjunction with Report 3073L. GEOPHYSICAL INVESTIGATION FOR COASTAL Scale 1:1000H. Drawn PJE Positioning is given in GDA 94 zone 50. EROSION VULNERABLITY ASSESSMENT Drawn PJE Levels are given in Australian Height Datum (AHD). HORROCKS, SHIRE OF NORTHAMPTON WA Drawing 3073L-09 Revision C	NOTES	CLIENT	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	Date	26 June 2023	Paper Size	A3
	Positioning is given in GDA 94 zone 50.		Scale	1:1000H, 1:500V	Drawn	PJE	
	Levels are given in Australian Height Datum (AHD).			Drawing	3073L-09	Revision	С

GBGGROUP

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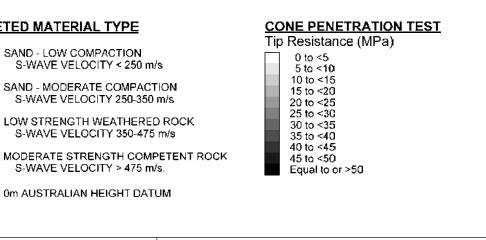
-5-

-6-

Refusal 100MPa

-7

RL (mAHD)



GBGGROUP

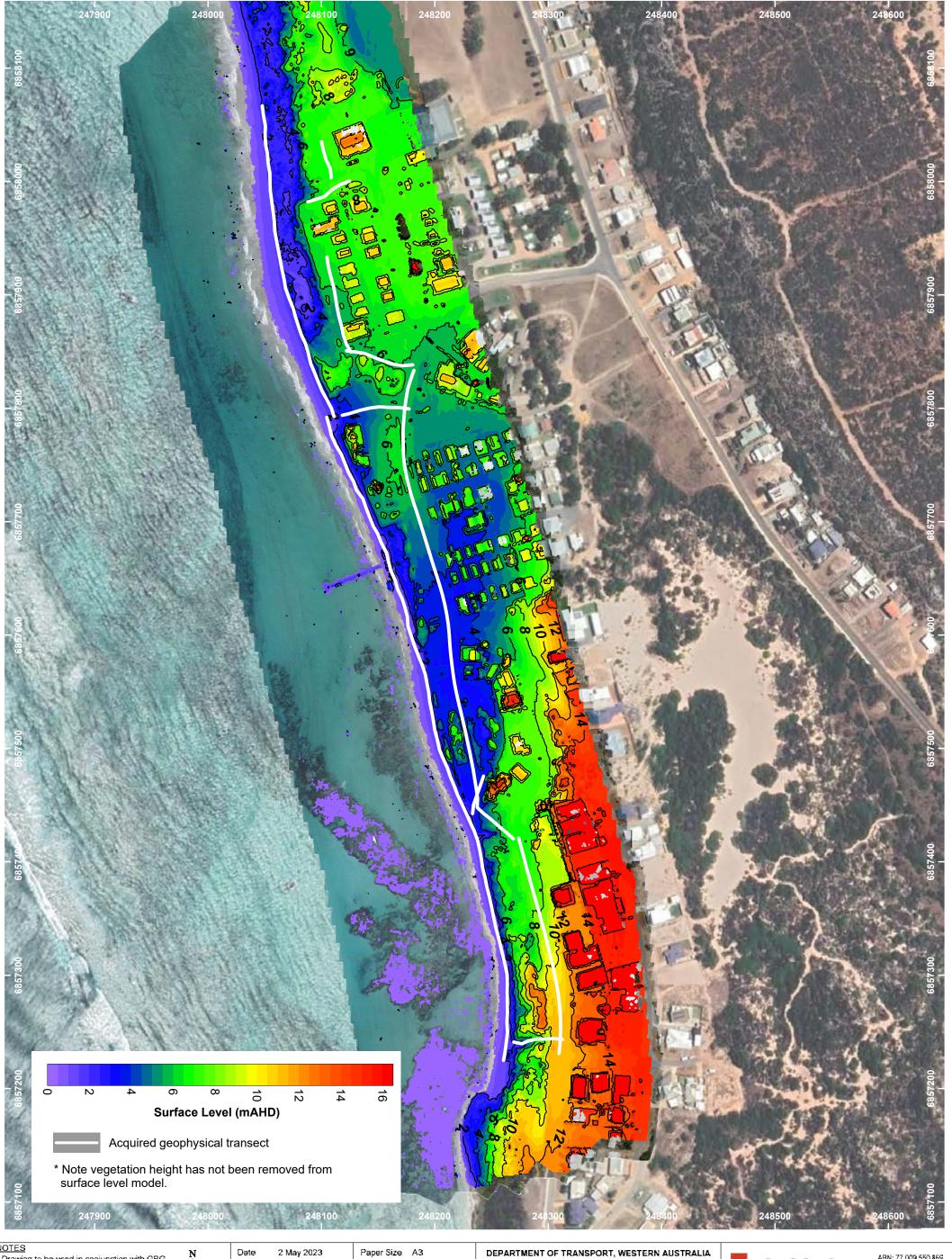




APPENDIX C – MODELLED TOP OF ROCK AND SAND THICKNESS



SURFACE LEVEL MODEL



 NOTES
 Drawing to be used in conjunction with GBG report 3073L.
 Date
 2 May 2023
 Paper Size
 A3
 DEPARTMENT OF TRANSPORT, WESTERN AUSTRAL

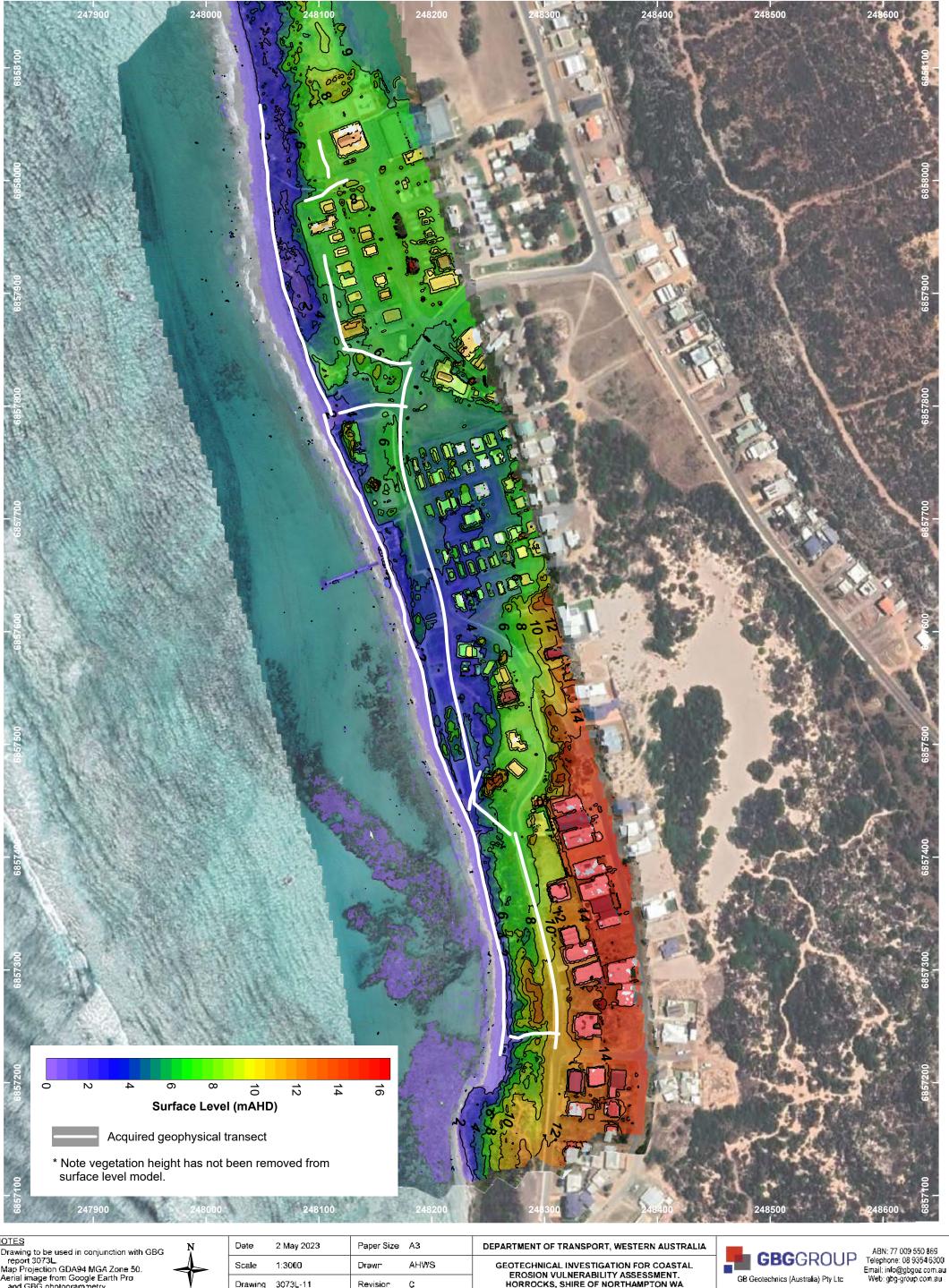
 Map Projection GDA94 MGA Zone 50.
 Aerial image from Google Earth Proand GBG photogram metry.
 Scale
 1:3000
 Drawn
 AHWS
 GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT. HORROCKS, SHIRE OF NORTHAMPTON WA



ABN: 77 009 550 869 Telephone: 08 9354 6300 Email: info@gbgoz.com.au Web: gbg-group.com.au



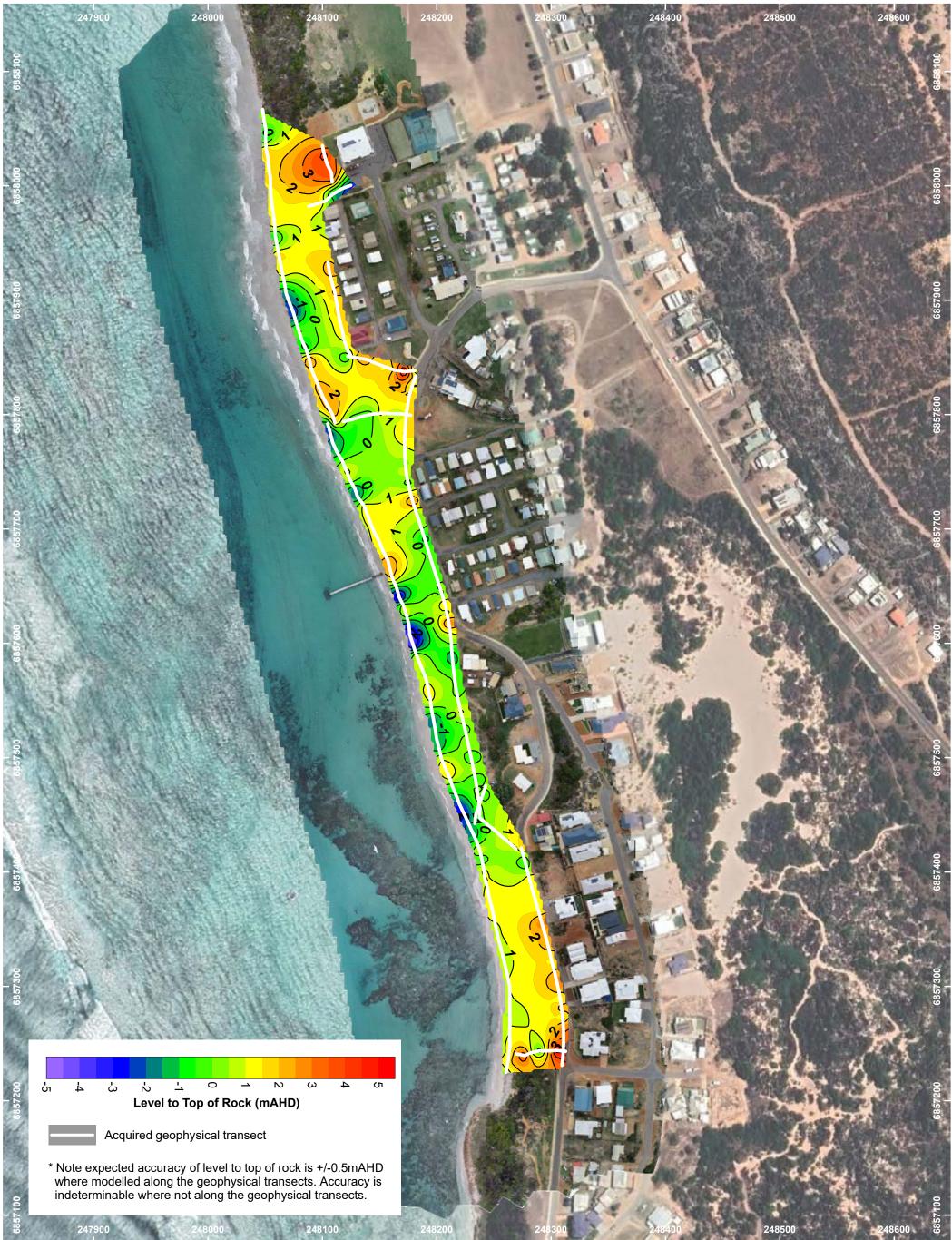
SURFACE LEVEL MODEL



NOTES Drawing to be used in conjunction with GBG	Ņ	Date	2 May 2023	Paper Size	A3	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA		ABN: 77 I
	$ \mathbf{A} $	Scale	1:3000	Drawn	AHWS	GEOTECHNICAL INVESTIGATION FOR COASTAL	GBC GROUP	Telephone: Email: info@
Aerial image from Google Earth Pro and GBG photogrammetry.	V	Drawing	3073L-11	Revision	С	EROSION VULNERABILITY ASSESSMENT. HORROCKS, SHIRE OF NORTHAMPTON WA	GB Geotechnics (Australia) Pty Ltc	Web: gbg-



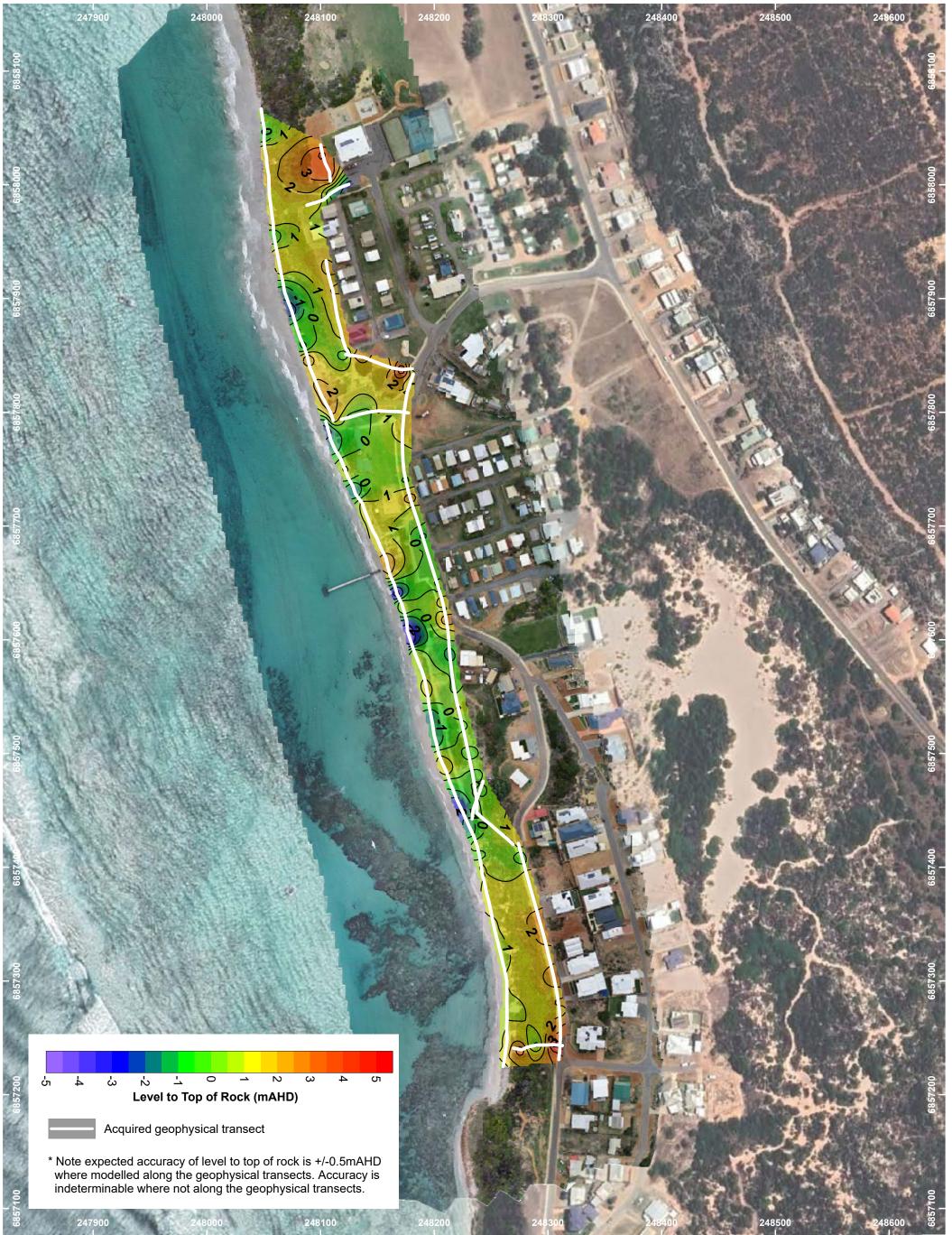
CONTOURED LEVEL TO TOP OF ROCK



NOTES Drawing to be used in conjunction with GBG	Ņ	Date	2 May 2023	Paper Size	A3	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA		ABN: 77 009 550 869
	$ \rightarrow $	Scale	1:3000	Drawn	AH₩S	GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.		Telephone: 08 9354 6300 Email: info@gbgoz.com.au
Aerial image from Google Earth Pro and GBG photogrammetry.	V	Drawing	3073L-12	Revision	С	HORROCKS, SHIRE OF NORTHAMPTON WA	GB Geotechnics (Australia) Pty Ltc	Web: gbg-group.com.au



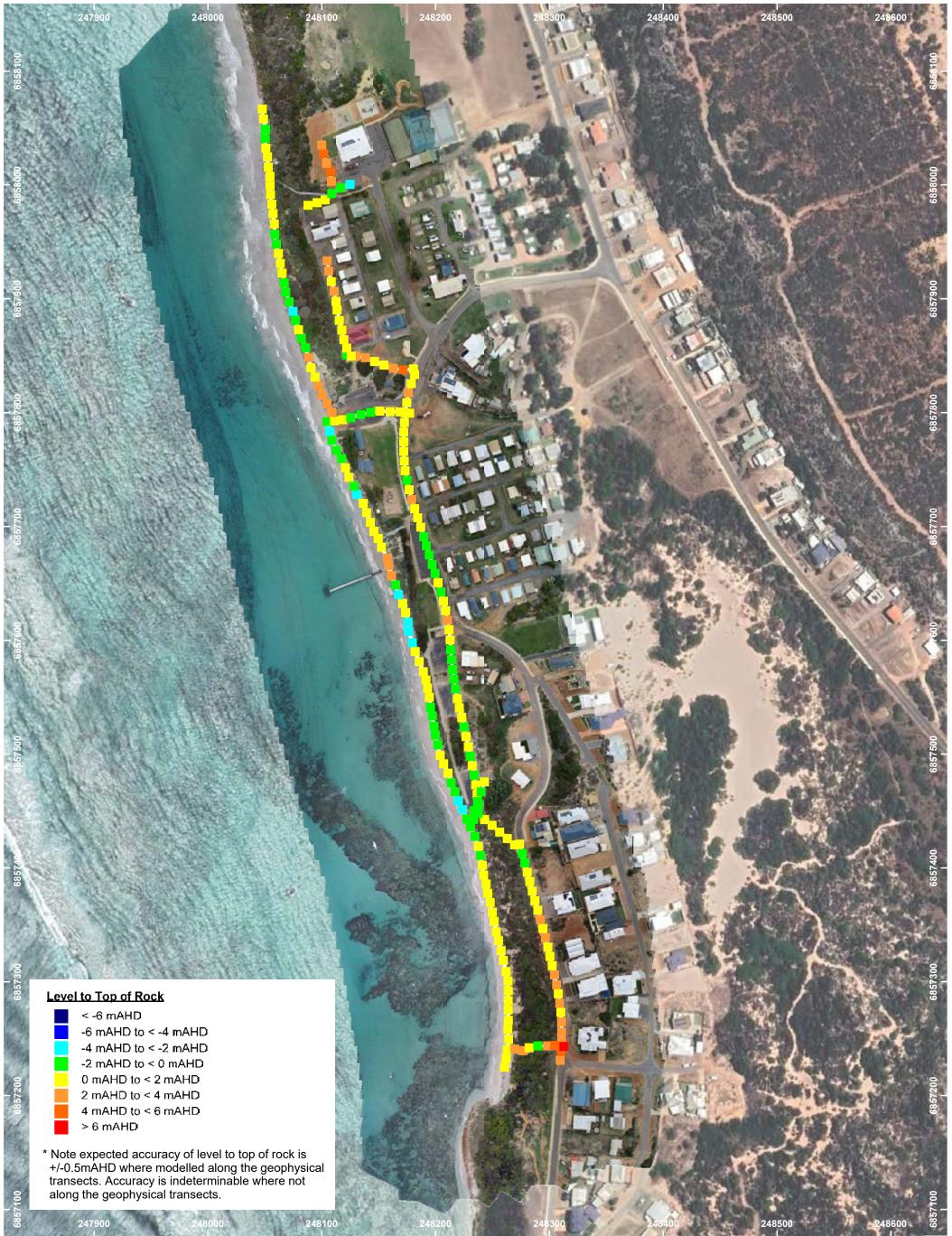
CONTOURED LEVEL TO TOP OF ROCK



NOTES Drawing to be used in conjunction with GBG	N	Date	2 May 2023	Paper Size	A3	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA		ABN: 77 009 550 869
report 3073L. Map Projection GDA94 MGA Zone 50.		Scale	1:3000	Drawn	AHWS	GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.		Telephone: 08 9354 6300 Email: info@gbgoz.com.au
Aerial image from Google Earth Pro and GBG photogrammetry.	V	Drawing	3073L-13	Revision	С	HORROCKS, SHIRE OF NORTHAMPTON WA	GB Geotechnics (Australia) Pty Ltc	Web: gbg-group.com.au



CLASSED POST MAP LEVEL TO TOP OF ROCK



NOTES Drawing to be used in conjunction with GBG	Date 2 May 2023	Paper Size A3	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	ABN: 77 009 550 869
report 3073L. Map Projection GDA94 MGA Zone 50.	Scale 1:3000	Drawn AHWS	GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.	GBGGROUP Telephone: 08 9354 6300 Email: info@gbgoz com.au
Aerial image from Google Earth Pro and GBG photogram netry.	Drawing 3073L-14	Revision C	HORROCKS, SHIRE OF NORTHAMPTON WA	GB Geotechnics (Australia) Pty Ltc Web: gbg-group.com.au



CONTOURED SAND THICKNESS OVER ROCK



NOTES Drawing to be used in conjunction with GBG	Date	2 May 2023	Paper Size	A3	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA	ABN: 77 009 550 869
report 3073L. Map Projection GDA94 MGA Zone 50.	Scale	1:3000	Drawn	AHWS	GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.	Telephone: 08 9354 630 Email: info@gbgoz.com.
Aerial image from Google Earth Pro and GBG photogram metry.	Drawing	3073L-15	Revision	С	HORROCKS, SHIRE OF NORTHAMPTON WA	GB Geotechnics (Australia) Pty Ltc Web: gbg-group.com.a



CONTOURED SAND THICKNESS OVER ROCK





NOTES Drawing to be used in conjunction with GBG	Ņ	Date	2 May 2023	Paper Size	A3	DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA		ABN: 77 009 550 869
report 3073L. Map Projection GDA94 MGA Zone 50.		Scale	1:3000	Drawn	AH₩S	GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT.		Telephone: 08 9354 6300 Email: info@gbgoz.com.au
Aerial image from Google Earth Pro and GBG photogrammetry.	V	Drawing	3073L-16	Revision	С	HORROCKS, SHIRE OF NORTHAMPTON WA	GB Geotechnics (Australia) Pty Ltc	Web: gbg-group.com.au



CLASSED POST MAP SAND THICKNESS OVER ROCK



N

NC	TES

Drawing to be used in conjunction with GBG report 3073L Map Projection GDA94 MGA Zone 50. Aerial image from Google Earth Pro and GBG photogram netry.

	Date	2 May 2023	Paper Size	A3
>	Scale	1:3000	Drawn	AH₩S
	Drawing	3073L-17	Revision	С

GEOTECHNICAL INVESTIGATION FOR COASTAL EROSION VULNERABILITY ASSESSMENT. HORROCKS, SHIRE OF NORTHAMPTON WA

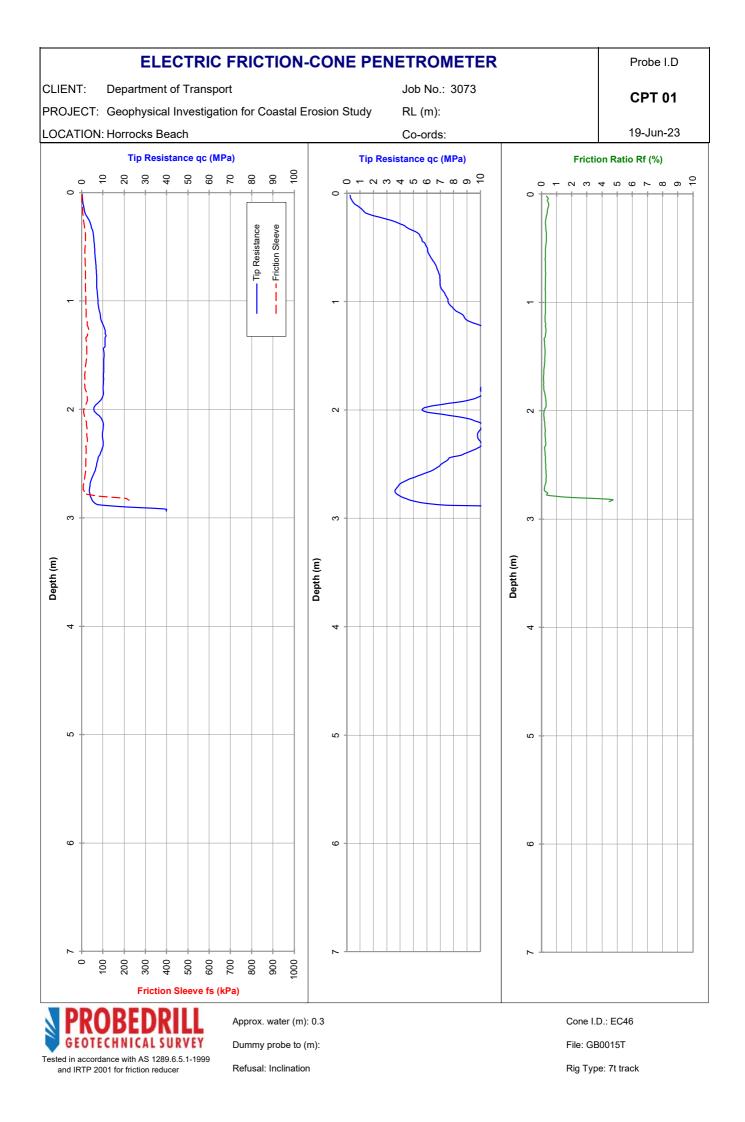
DEPARTMENT OF TRANSPORT, WESTERN AUSTRALIA

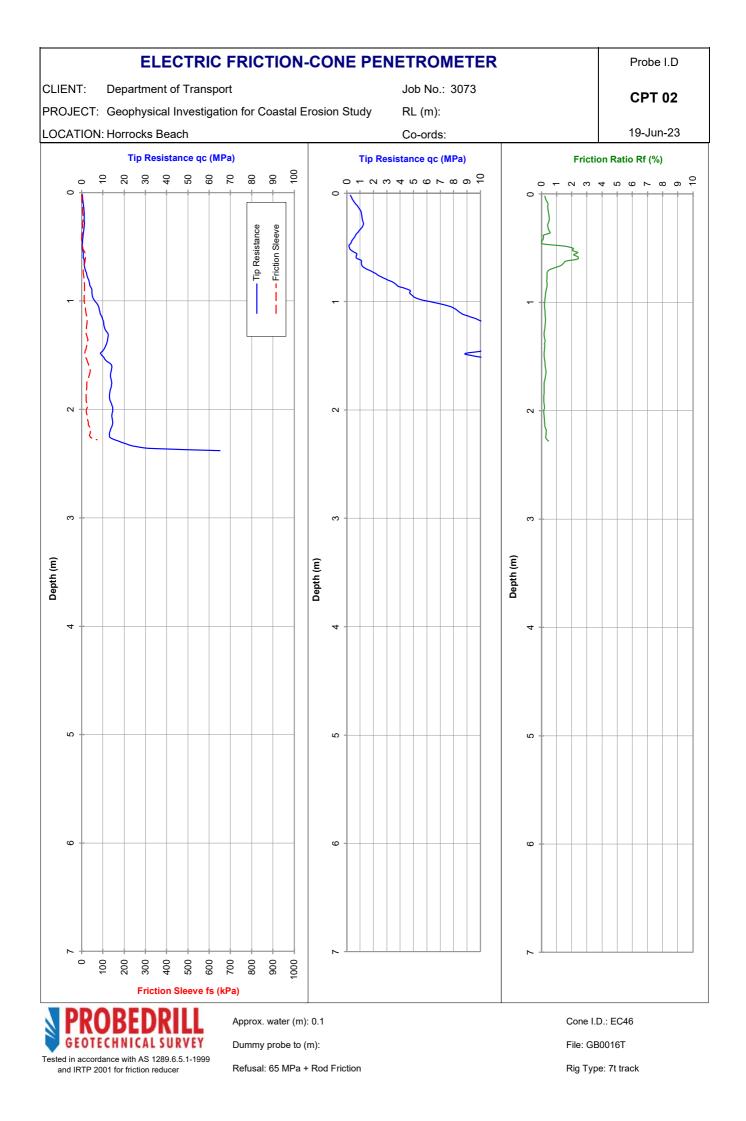


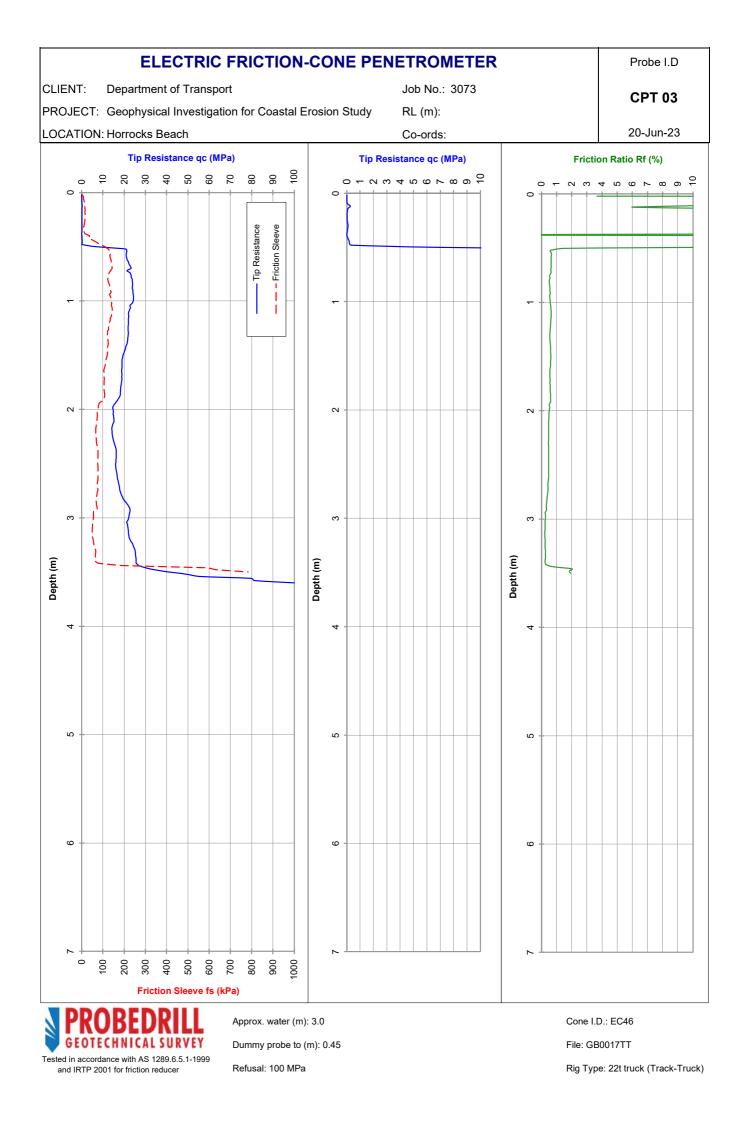
ABN: 77 009 550 869 Telephone: 08 9354 6300 Email: info@gbgoz.com.au Web: gbg-group.com.au

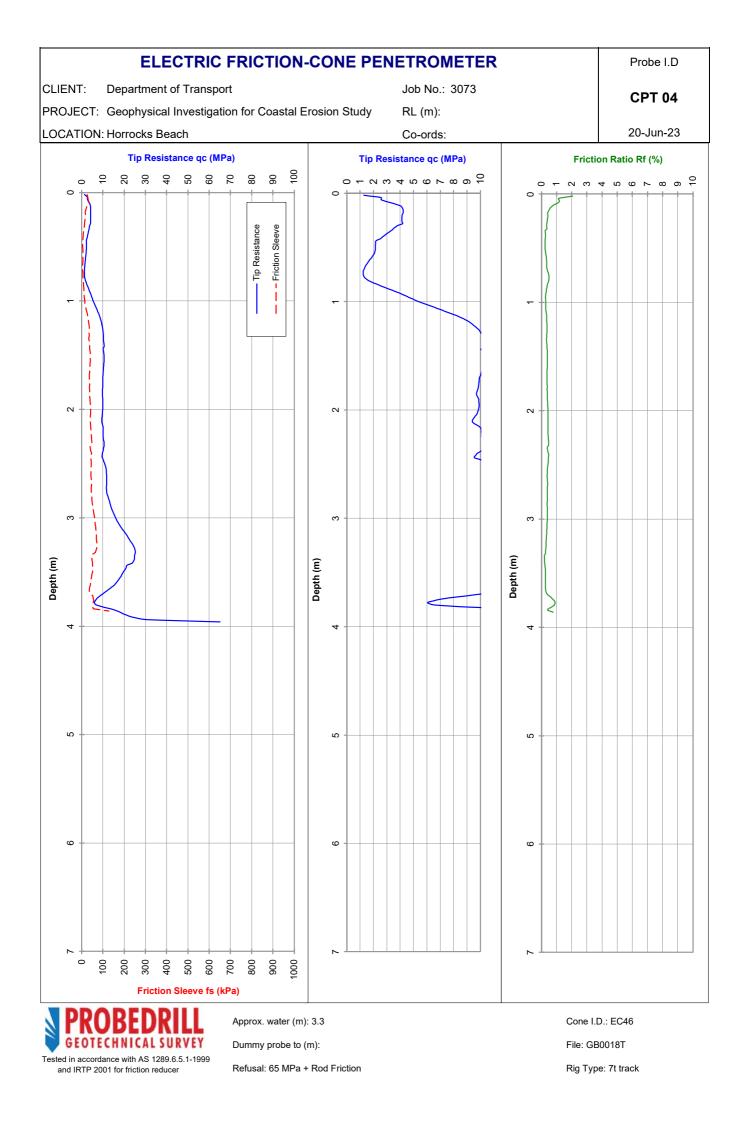


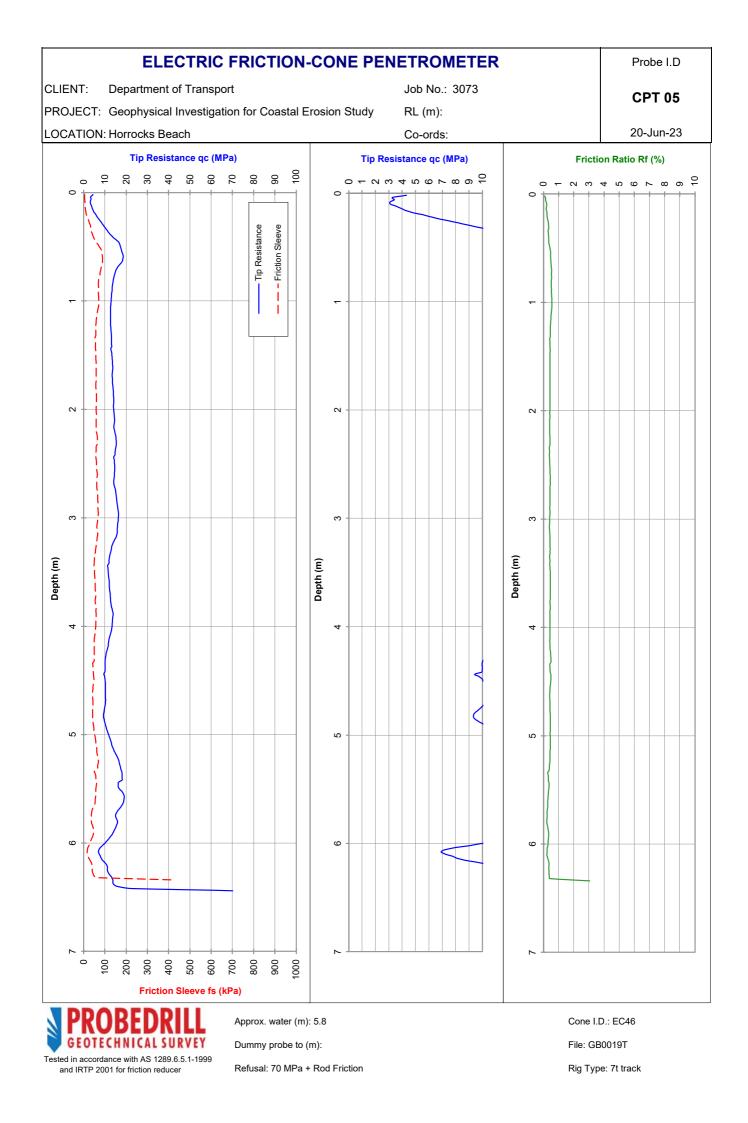
APPENDIX D – CONE PENETRATION TEST PLOTS

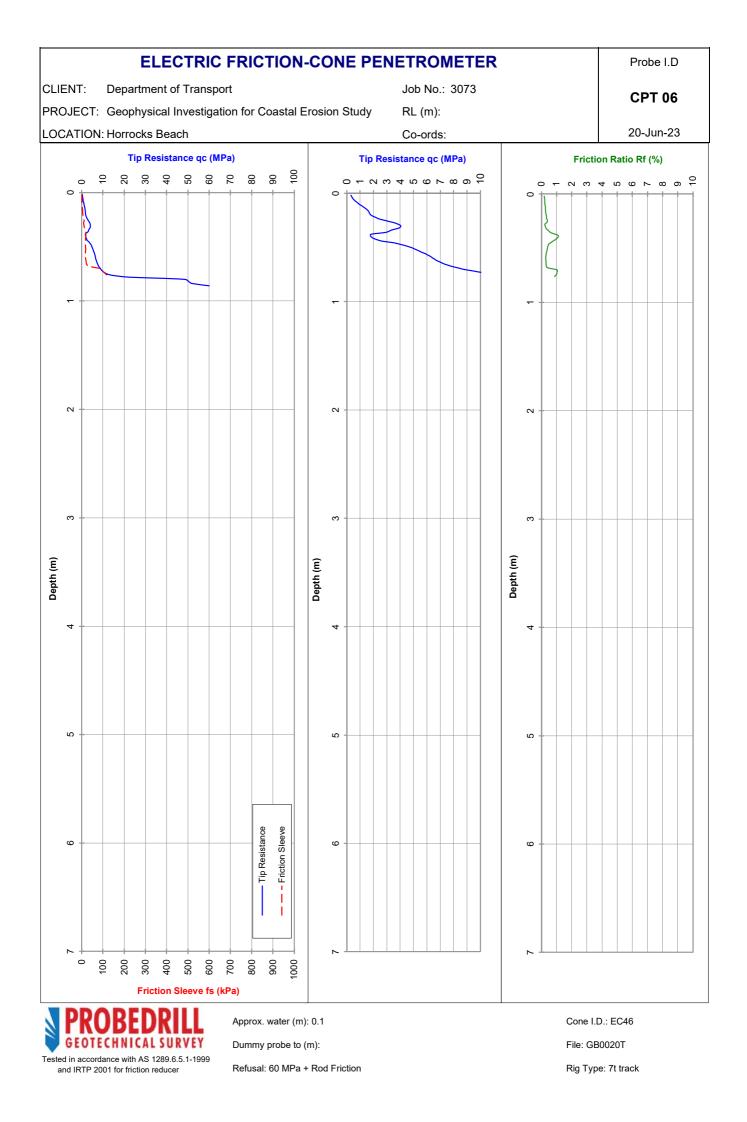














CALIBRATION CERTIFICATE

CONE ID:

Cone Type: Calibration Date (qc/fs): Calibration Date (u): Preliminary Inspection: Calibrated By: Calibration Procedure: Force Application: Reference Equipment:

EC46

Compression 9 May 2023 7 December 2022 Pass Henky Lawer ISO 22476-1:2012, IRTP 2001 Compression PT - S type 100kN Serial # 512

PT - \$ type 100kN Serial # 5126009 (Calibrated 10/03/23 - NATA approved Cert. No. 230664) Bongshin - \$ type 50kN Serial #W05345 (Calibrated 10/03/23 - NATA approved Cert. No. 230663) Digitron Panel Meter Serial #: 060213/01 (Calibrated 09/03/23 - NATA endorsed Report No. 230658, 230659, 230660) Note: In accordance with A51289 F5.1 the force calibration derived by NATA Calibration Certificates are converted to a qc reading in MPa and fs reading in kPa by dividing by 1000 mm² and 1500nm³ respectively.

Results of Calibration:

qc (tip resi		(r)	fs (sleeve f			u (pore pre		
Capacity:	100	(MPa)	Capacity:	2000) (kPa)	Capacity:	3500	(kPa)
Area	1000) (mm²)	Area	15000) (mm²)	Position	u2	
Applied	Eqv.	Mean	Applied	Eqv.	Mean	Applied	Eqv.	Mean
Load	Pressure	Observed	Force	Load	Observed	Pressure	Pressure	Observed
kN	MPa	Reading	kN	kPa	Reading	bar	kPa	Reading
		Volts			Volts			Volts
0	0	0.000	0	0	0.000	0	0	0.000
10	10	0.742	3	200	0.738	3	300	0.414
20	20	1.502	6	400	1.498	6	600	0.830
30	30	2.267	9	600	2.265	9	900	1.243
40	40	3.035	12	800	3.022	12	1200	1.656
50	50	3.800	15	1000	3.776	15	1500	2.070
60	60	4.564	18	1200	4.531	18	1800	2.483
70	70	5.324	21	1400	5.286	21	2100	2.895
80	80	6.087	24	1600	6.042	25	2500	3.444
90	90	6.852	27	1800	6.800	30	3000	4.130
100	100	7.616	30	2000	7.558	35	3500	4.816
90	90	6.860	27	1800	6.835	30	3000	4.137
80	80	6.101	24	1600	6.085	25	2500	3.455
70	70	5.343	21	1400	5.332	21	2100	2.900
60	60	4.582	18	1200	4.577	18	1800	2.489
50	50	3.820	15	1000	3.821	15	1500	2.074
40	40	3.058	12	800	3.064	12	1200	1.660
30	30	2.291	9	600	2.302	9	900	1.246
20	20	1.523	6	400	1.535	6	600	0.830
10	10	0.753	3	200	0.772	3	300	0.416
0	0	0.002	0	0	0.003	0	0	0.000
R^2 Value =	1.000		R^2 Value =	1.000		R^2 Value =	1.000	
Zero Load Erre	or	0.03%	Zero Load Err	or	0.03%	Zero Load Erro	or:	0.01%
Max. Linearity		0.31%	Max. Linearity		0.03%	Max. Linearity		0.01%
Max. Hysteris	•	0.33%	Max. Hysteris		0.62%	Max. Hysteris		0.24%
MPa/Volt:		13.109	kPa/Volt:		264.13	kPa/Volt:		726.10
wir aj volt:		13.103	κραί κοι:		204.13	•		
						Net Area (o	calibrated):	0.83

"Class 1" Application Accuracy achieved (in accordance with ISO 22476:2012 classification)

Calibration Checked & Authorised	Kylie Walker		
Job Details			
Client:	GB Geotechnics	Date of Job:	19/06/23
Rep:	Andrew Spyrou	Tip Diameter:	35.5
Location:	Horrocks Beach	Sleeve Diameter:	35.83

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MOROOKA (M2)

11 tonne track mounted CPT Rig





SPECIFICATIONS

Overall Dimensions	Width: 2.3m; Length: 5.3m; Height: 3.2m (while travelling) Height: 4.4m (while probing)
Gross Weight	11 tonne
Ground Bearing Capacity	0.38 kg/cm ² (37kPa / 5.4psi)
Speed (Low/High)	Low gear: 8.3km High gear: 12km/h on level ground
Grade ability	60%
Engine	Mitsubishi (3910cc) 110 HP @ 2,800 rpm
Fuel Tank	80 L (Diesel)
Drive System	HST
Tracks	600mm wide rubber tracks
Levelling Jacks	0.8m stroke

EQUIPMENT / FEATURES

Other Equipment / Features	2.4m x 1.2m Plastic Bog Boards
	1 x 9kg ABE Fire extinguisher
	Air conditioned work cabin and drive cabin
Transport	Prime Mover & 10m Drop-deck trailer with ramps

SERVICES

Geotechnical Services	CPT, CPTu, SCPT, SCPTu (1, 5, 10, & 15 tonne cones)
provided	DMT, SDMT
	Dissipation Testing
	Ball Penetrometer
	CPT casing for additional rod support
	Dual Tube (percussion) sampling
	Piston Sampling
	MOSTAP and PROBEDRILL soil sampling
	Vane Shear Testing (Electronically driven)
	Vibrating Wire Installation
	Water Sampling
	Standpipe Installation (20mm; 32mm & 50mm)

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